

**SOUTH WAYNE  
DRAINAGE IMPROVEMENTS  
FEASIBILITY STUDY**

**APRIL 2022**

**REVISED: MAY 31, 2022**

**PREPARED FOR:**

**RADNOR TOWNSHIP  
301 IVEN AVENUE  
WAYNE, PA 19087-5297**

**PREPARED BY:**

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## I. INTRODUCTION

Carroll Engineering Corporation (CEC) is pleased to present this report which examines the feasibility of various alternatives for improvements to the South Wayne portion of Radnor Township to improve periodic flooding which occurs after heavy rainfalls. This area is traversed by Ithan Creek which was historically a meandering stream with various ponds along Midland Avenue, Saint Davids Road, Pembroke Avenue, and Meadowbrook Avenue according to available maps dating back as far as 150 years. Since that time, there has been significant encroachment from residential development and the stream has been confined to a manmade channel which varies in geometry and composition from its headwaters in the vicinity of the Radnor Fire Company to Encke Park adjacent to the Radnor Township Building.

From the Radnor Middle School, a main storm sewer culvert is noted to run along the southern side of Midland Avenue, crossing beneath the Saint Katherine of Siena School and South Aberdeen Avenue, and continues between the rear yards of the residential properties between Midland Avenue and Saint Davids Road. These areas are noted to have limited stormwater management infrastructure in the roadways and experience continual flooding issues during heavy rainfalls. As Ithan Creek approaches Pembroke Avenue, it turns south and crosses Meadowbrook Avenue and Orchard Way before proceeding east again. The creek continues through two (2) culverts, one at Iven Avenue, and other at the entrance of the Radnor Township Building. From there, Ithan Creek proceeds along the southern side of Encke Park returning to a typical creek composition with a natural bottom and vegetated side slopes.

The purpose of this study is multi-faceted with the following being the main goals of this Phase:

1. Identify each geometrically unique portion of the stream/culvert and catalog the following:
  - Stream/culvert bed slope
  - Bottom width and/or culvert dimensions
  - Side slopes
  - Channel depth
  - Composition of the stream bottom
  - Manning's 'n' coefficient (relative roughness constant)
2. Identify the drainage area and flow rates for each design year storm for each geometrically unique portion of the stream/culvert.
3. Complete a Manning's calculation to demonstrate the theoretical capacity of each portion of the stream.
4. Identify which portions of the stream/culvert may be deficient based on the capacity calculations and provide approximate sizing required to convey the 100-yr storm.
5. Prepare a conceptual plan for storm sewer infrastructure along Midland Avenue and Saint Davids Road which shall connect to the main storm sewer culvert corridor.
6. Prepare a conceptual plan for a potential storm sewer bypass beginning in the vicinity of the Pembroke Avenue between its intersections with Midland and Saint Davids Road and running southeast to Encke Park.

## **II. UNIQUE STREAM / CUVERT SECTIONS:**

CEC performed a comprehensive topographic survey of the Ithan Creek Corridor and the adjacent right-of-way(s) to identify physical features such as stream geometry, storm sewers, culvert, retaining walls, centerline and edge of roadways, driveways, utility poles, mailboxes, fence lines, and other utilities and prominent features visible on the surface or marked by utility owners.

Following the survey, CEC prepared an existing features plan set of the entire stream corridor which is included Appendix A of this report. The existing features plan includes an index sheet to indicate where each sheet of the plans is located for ease of viewing.

The “Ithan Creek Sections – Index Plan” included in Appendix B summarizes the thirteen (13) individual stream sections along Ithan Creek which were used as the basis of our evaluation. These sections represent the approximate geometry of the stream for that particular reach. It should be noted that there are a number of minor variations in the parameters presented below (i.e., geometry, slope, etc.) for each reach. The sections are intended to represent the “best fit” which have been summarized below for reference.

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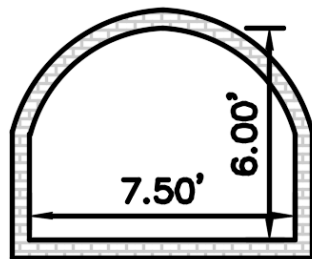
## SECTION 1

### Location:

This culvert section is located on the southern side of Midland Avenue between its intersection with Louella Lane and the Saint Katherine of Siena School.

### Section Material & Geometry:

This section is composed of a 90- x 72-inch brick arch culvert (see graphic representation and photograph from a recent Township video inspection below).



**SECTION 1**



### Section Capacity and Reach Geometry:

Length = 990 feet

Reach slope = 0.54% ±

Manning's n = 0.018

**Theoretical Capacity = 339 CFS**

Drainage Area = 192 acres

**100-year peak flow rate = 548 CFS**

50-year peak flow rate = 449 CFS

25-year peak flow rate = 358 CFS

10-year peak flow rate = 252 CFS

5-year peak flow rate = 181 CFS

2-year peak flow rate = 98.6 CFS

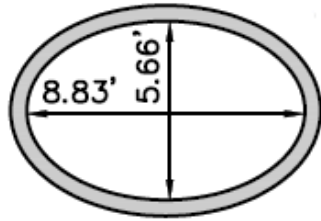
### Observations/Recommendations:

A video inspection of this closed conduit was recently commissioned by the Township which demonstrated that this reach is in relatively good condition despite its old age (installation date unknown). Additionally, the theoretical carrying capacity falls somewhere between a 10- and 25-year peak flow rate. There is a portion where the Saint Katherine of Siena School is located directly over top of the culvert which is not typically considered "good practice" since loss of property and/or life could result from a potential collapse. This conduit is recommended for consideration of eventual replacement in part to remove the conflict with Saint Katherine's, to replace aging infrastructure, incorporate stormwater inlets along Midland Avenue in accordance with Sheets C-103 & C-104 in Appendix A of this report, and provide the added capacity to convey the 100-year peak flow rate. The aforementioned design plans in Appendix presently depict the largest available concrete elliptical pipe which still falls somewhat short of the 100-year peak flow rate (437 CFS vs 545 CFS). However, alternatives to use a larger box culvert was ruled out due to space limitations of adjacent existing utilities and the significant cost addition for a box culvert as opposed to elliptical pipe. A sketch of this proposed section is included below for reference and calculations are

provided in Appendix C which demonstrate the equivalent round pipe would nearly have capacity to convey the 50-year peak flow rate.

The Township may also elect to complete the replacement of the portion overlaid by Saint Katherine's only to reduce the overall project scope.

In any case, improvements to the open channel portion of the stream at the Saint Katherine's parcel would need to be completed concurrently to remove approximately 2½ feet of the stream bottom and the pedestrian bridge to provide adequate slope for the replacement culvert. These removals are depicted on the aforementioned Sheet C-103.



PROPOSED SECTION 1

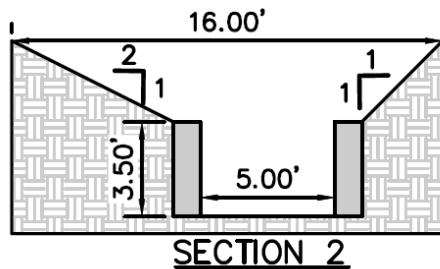
## SECTION 2

### Location:

This stream section is located on the southeastern portion of the Saint Katherine of Siena School parcel between the exit of Section 1 and an existing stone pedestrian bridge to the west of South Aberdeen Avenue.

### Section Material & Geometry:

This section is an approximately 5 feet wide rectangular open channel with stone walls on either side having an approximate height of 3.5 feet. Above the stone walls, existing grade is sloped back until it reaches the elevation of the adjacent South Aberdeen Avenue roadway (see graphic representation below).



### Section Capacity and Reach Geometry:

Length = 82 feet

Reach slope = 0.90% ±

Manning's n = 0.017

**Theoretical Capacity = 542 CFS**

Drainage Area = 237 acres

**100-year peak flow rate = 626 CFS**

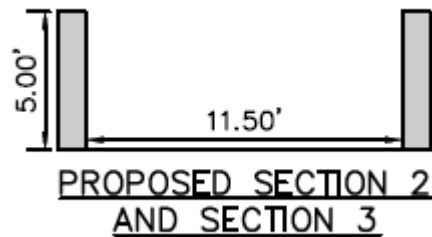
50-year peak flow rate = 513 CFS

25-year peak flow rate = 410 CFS

10-year peak flow rate = 289 CFS

5-year peak flow rate = 208 CFS

2-year peak flow rate = 114 CFS



### Observations/Recommendations:

This portion of the stream is in good condition and the theoretical carrying capacity is relatively good which falls somewhere between a 50- and 100-year peak flow rate as noted above. However, this portion of the creek may be observed to surcharge during smaller storm events due to the presence of the downstream stone pedestrian bridge which forms a "choke point" for the stream. As you will note below, this pedestrian bridge has a theoretical capacity which falls between the 2-year and 5-year peak flow rate.

Also as previously noted in the Section 1 discussion above, the Midland Avenue storm sewer replacement plans on Sheet C-103 and C-104 in Appendix A of this report requires that this portion of the stream be lowered approximately 2½ feet to allow the proposed storm sewer to "daylight" at the existing stream. The channel section could also be maximized at that time to accommodate the 100-year peak flow rate. A graphic representation of the proposed channel is included above for reference and calculations are provided in Appendix C which demonstrate this channel cross-section would have sufficient capacity to convey the 100-year peak flow rate.

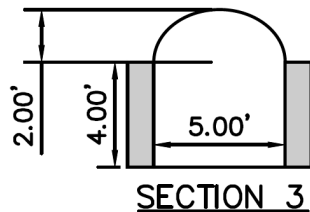
### SECTION 3

#### Location:

This section is a stone masonry pedestrian bridge over the stream located on the eastern portion of the Saint Katherine of Siena School property. This is a decorative feature leading to a garden area near the intersection of Midland Avenue and South Aberdeen Avenue.

#### Section Material & Geometry:

This creek section is a 5 feet wide culvert with a 2 feet stone arch above 4 feet stacked stone walls (see graphic representation and photograph below).



#### Section Capacity and Reach Geometry:

Length = 9 feet

Reach slope = 0.35% ±

Manning's n = 0.017

**Theoretical Capacity = 165 CFS**

Drainage Area = 256 acres

**100-year peak flow rate = 657 CFS**

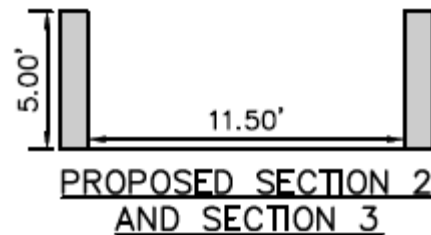
50-year peak flow rate = 539 CFS

25-year peak flow rate = 431 CFS

10-year peak flow rate = 305 CFS

5-year peak flow rate = 220 CFS

2-year peak flow rate = 121 CFS



#### Observations/Recommendations:

The pedestrian bridge has a theoretical capacity which falls between the 5-yr and 10-yr peak flow rate and is considered vastly undersized based on the tributary flows. As previously noted, this likely serves as a "choke point" for the flow which is tributary to this bridge. It is recommended that this bridge, which is assumed to have been installed for aesthetics rather than serving a particular function, be removed along with the abrupt drop in the channel just downstream to improve flow characteristics by removing this constriction.

Also as previously noted in the Section 1 & 2 discussion(s) above, the Midland Avenue storm sewer replacement plans on Sheet C-103 and C-104 in Appendix A of this report requires that that this structure be removed, and the stream be lowered approximately 2 ½ feet to allow the proposed storm sewer to "daylight" at the existing stream. The channel section could also be maximized at that time to accommodate the 100-year peak flow rate. A graphic representation of the proposed channel is included above for reference and calculations are provided in Appendix C which demonstrate this channel cross-section would have sufficient capacity to convey the 100-year peak flow rate.



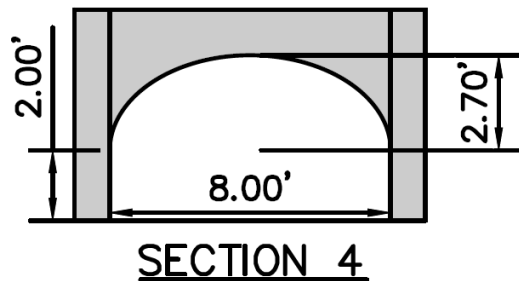
## SECTION 4

### Location:

This stream section is the culvert underneath South Aberdeen Avenue to the east of the Saint Katherine of Siena School.

### Section Material & Geometry:

This section is an 8 feet wide culvert with a 2.7 feet stone arch above 2 feet stacked stone walls (see graphic representation and photograph below).



### Section Capacity and Reach Geometry:

Length = 63 feet

Reach slope = 1.52% ±

Manning's n = 0.017

**Theoretical Capacity = 426 CFS**

Drainage Area = 256 acres

**100-year peak flow rate = 657 CFS**

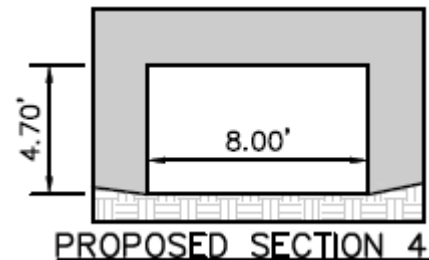
50-year peak flow rate = 539 CFS

25-yr peak flow rate = 431 CFS

10-yr peak flow rate = 305 CFS

5-yr peak flow rate = 220 CFS

2-yr peak flow rate = 121 CFS



### Observations/Recommendations:

The theoretical capacity of the stone culvert is nearly equivalent to the 25-year peak flow rate. Additionally, no operational issues are known to exist. As such, it is recommended that the Township continue to conduct periodic inspections to verify the integrity of the culvert is intact as is good practice.

This culvert may be subject to replacement in the future largely due to its assumed advanced age as part of the Township's general infrastructure replacement programs. The relative opening could be maximized at that time to adequately pass the 100-year peak flow rate. This culvert would be well suited for a CON/SPAN bridge or a box culvert. The graphic representation of the proposed box culvert is included above for reference and calculations are provided in Appendix C which demonstrate this culvert would have sufficient capacity to convey the 100-year peak flow rate.

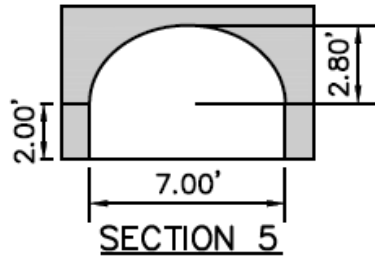
## SECTION 5

### Location:

This closed conduit is located below existing grade between South Aberdeen Avenue and Pembroke Avenue. It runs along the rear yards of residences having frontage on Midland Avenue and Saint David's Road.

### Section Material & Geometry:

This creek section is a 7 feet wide culvert with a 4.8 feet brick arch (see graphic representation and photograph below).



### Section Capacity and Reach Geometry:

Length = 548 feet

Reach slope = 0.295% ±

Manning's n = 0.017

**Theoretical Capacity = 164 CFS**

Drainage Area = 262 acres

**100-year peak flow rate = 668 CFS**

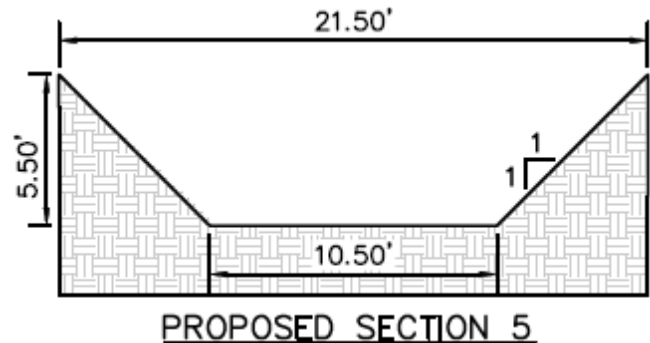
50-year peak flow rate = 547 CFS

25-yr peak flow rate = 438 CFS

10-yr peak flow rate = 310 CFS

5-yr peak flow rate = 223 CFS

2-yr peak flow rate = 123 CFS



### Observations/Recommendations:

The theoretical capacity of this closed conduit falls below the 5-year peak flow rate and is considered vastly undersized based on the tributary flows. This closed conduit likely serves as a substantial "choke point" due to its low theoretical capacity and the hydraulic losses of stormwater entering a closed conduit from an open channel. Furthermore, the existing grade above the conduit is somewhat higher than adjacent areas which is likely due to a coverage issue. This results in stormwater runoff entering the rear yards of residents along Midland and Saint Davids Avenue which cannot be conveyed by the conduit. There are also no intermediate inlets to accept additional runoff along this entire reach. Rather, stormwater flow must run to the east along the rear yards of residences until it meets the open channel portion of the stream.

Our recommendation would be to remove this closed conduit and replace it with an open channel having a bottom width of approximately 10½ feet, with 1:1 side slopes, and an approximate top width of 21½ feet. Calculations are provided in Appendix C which demonstrate this channel cross-section would have sufficient capacity to convey the 100-year

peak flow rate. Alternatives for smaller channels were not examined since it is not advisable to complete a replacement project for a channel not having sufficient capacity for the 100-year peak flow rate.

Typically, new channels would be designed to have 3:1 side slopes or less to minimize any bank erosion and allow for ease of maintenance. However, there are a number of existing features which are in close proximity to the stream which preclude the channel from having more gradual side slopes and some that require modifications to accommodate the proposed channel. These existing features and/or impacts are as follows:

- **Garage at 313 Saint Davids Road (Parcel ID 36030190800)**  
The existing garage in the rear yard of this parcel is located within 10.3 feet of the existing closed conduit. The proposed open channel option would effectively move the edge of the stream 7.5 feet closer to this garage leaving approximately 3 feet of separation between the top of bank and northern side of the garage.
- **Garage / SWM Facility at 321 Saint Davids Road (Parcel ID 36030190600)**  
The existing garage in the rear yard of this parcel is located within 12 feet of the existing closed conduit. The proposed open channel option would effectively move the edge of the stream 7.5 feet closer to this garage leaving approximately 4½ feet of separation between the top of bank and northern side of the garage. Additionally, the private stormwater facility on this parcel would need to be modified to move the berm to the south by approximately 6 feet.
- **Fence at 301 Saint Davids Road (Parcel ID 36030191000)**  
An existing fence line at the rear of this parcel would need to be moved to the south approximately 6½ feet.
- **Fence at 305 Saint Davids Road (Parcel ID 36030190900)**  
An existing fence line at the rear of this parcel would need to be moved to the south approximately 4 feet.
- **Fence at 319 Saint Davids Road (Parcel ID 36030190700)**  
An existing fence line at the rear of this parcel would need to be moved to the south approximately 4 feet.
- **Shed & Fence at 318 Midland Avenue (Parcel ID 36030179600)**  
An existing fence line at the rear of this parcel would need to be moved to the north approximately 6 feet. Additionally, an existing shed at the southwestern corner of the parcel would need to be moved north by approximately 6 feet.
- **Utility Poles at the rear yards of residences along Saint Davids Road**  
A line of four (4) existing utility poles along the rear yards of the residences along Saint Davids Road would be located at the top of the southern bank of the proposed open channel stream section. These limit the overall width of the proposed stream which would be feasible at this location.

As a result of steeper side slopes being required, the proposed open channel would need to be installed with a robust bank liner which may consist of a variety of options including grouted riprap, reno mattress, green gabions, etc.

Additionally, the option to replace the closed conduit with open channel would require that each homeowner along Midland Avenue and Saint Davids Avenue (between South Aberdeen and Pembroke Avenue) grant a permanent drainage easement to facilitate the work and allow the Township to maintain this reach of the stream in perpetuity. The acquisition of these easements will likely pose as a significant challenge to the Township.

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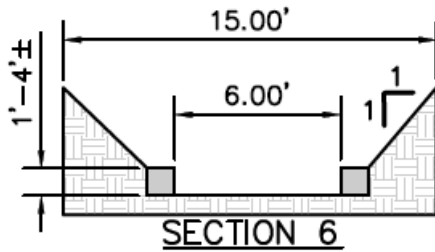
## SECTION 6

### Location:

This section of stream is located between the endwall of Section 5 southwest of the intersection of Midland Avenue and Pembroke Avenue and the headwall of the closed conduit running to the south along Pembroke Avenue.

### Section Material & Geometry:

This creek section is a 6 feet wide trapezoidal open channel with 3:1 slopes on the sides atop a stone wall ranging in height from 1- to 4 feet (see graphic representation below).



### Section Capacity and Reach Geometry:

Length = 130 feet

Reach slope = 1.100% ±

Manning's n = 0.017

**Theoretical Capacity = 659 CFS**

Drainage Area = 269 acres

**100-year peak flow rate = 678 CFS**

50-year peak flow rate = 556 CFS

25-yr peak flow rate = 445 CFS

10-yr peak flow rate = 315 CFS

5-yr peak flow rate = 227 CFS

2-yr peak flow rate = 125 CFS

### Observations/Recommendations:

This portion of the stream is in relatively good condition and the theoretical carrying capacity falls just below the 100-year peak flow rate as noted above. As such, no major modifications are recommended to this portion of the stream at this time. However, this portion of the creek may be observed to surcharge during smaller storm events due to the presence of the downstream closed conduit running to the south along Pembroke Avenue which forms a "choke point" for the stream. As you will note below, this Pembroke conduit has a theoretical capacity just above the 5-year peak flow rate.

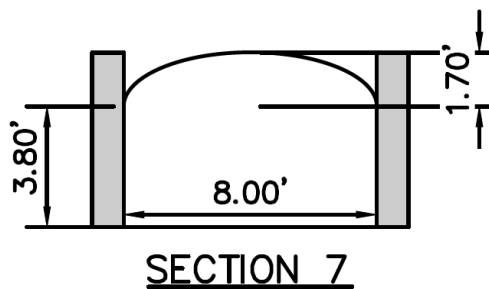
## SECTION 7

### Location:

This closed conduit is located beneath Pembroke Avenue which runs from its headwall to the southeast of the intersection of Midland Avenue and Pembroke Avenue and exits at approximately 200 feet southeast of the intersection of Pembroke Avenue and Saint Davids Road.

### Section Material & Geometry:

This section is an 8 feet wide rectangular channel with 3.8 feet stone walls and a 1.7 feet stone arch (see graphic representation and photographs below).



### Section Capacity and Reach Geometry:

Length = 422 feet

Reach slope = 0.260% ±

Manning's n = 0.017

**Theoretical Capacity = 234 CFS**

Drainage Area = 359 acres

**100-year peak flow rate = 813 CFS**

50-year peak flow rate = 556 CFS

25-yr peak flow rate = 445 CFS

10-yr peak flow rate = 315 CFS

5-yr peak flow rate = 227 CFS

2-yr peak flow rate = 125 CFS

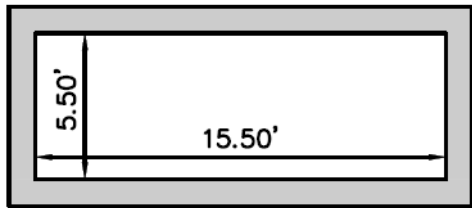


### Observations/Recommendations:

As noted above, this closed conduit has a theoretical capacity just above 5-year peak flow rate and likely serves as a “choke point” for flow along the stream. This is also exacerbated by deposition in the stream at the exit of this closed conduit. This deposition of sediment and debris from years of erosion has effectively reduced the overall carrying capacity of the Pembroke Avenue closed conduit by about 1½ feet. This is further described under Section 8 below. A video inspection of this closed conduit was recently commissioned by the Township which demonstrated that this reach is in relatively good condition despite its old age (installation date unknown).

We recommend that this closed conduit be ultimately replaced with a larger concrete box culvert beneath Pembroke Avenue. Since the alignment of the stream is such that it runs along Pembroke Avenue, options for open channel flow are not feasible. The proposed box culvert would need to be approximately 15½ feet wide by 5½ feet in height to accommodate the 100-year peak flow rate. A graphic representation of the proposed culvert is included below for reference and calculations are provided in Appendix C which demonstrate this channel cross-section would have sufficient capacity to convey the 100-year peak flow rate.

A parallel bypass pipe for this alternative would also not be hydraulically feasible since the largest elliptical concrete pipe available would still not provide adequate carrying capacity to convey the 100-year peak flow, less the capacity of the existing conduit. Additionally, there would be limited space to accommodate this alternative without the acquisition of private property.



PROPOSED SECTION 7

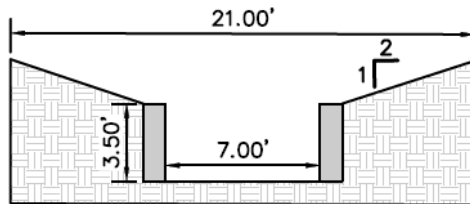
## SECTION 8

### Location:

This section of stream located between the endwall of the Pembroke Avenue conduit and the point where the stream crosses Meadowbrook Avenue.

### Section Material & Geometry:

This section is a 7 feet wide rectangular open channel with 3.5 feet stone walls on the sides with 2:1 vegetated slopes above the walls (see graphic representation below).



SECTION 8

### Section Capacity and Reach Geometry:

Length = 321 feet

Reach slope = 0.270% ±

Manning's n = 0.017

**Theoretical Capacity = 441 CFS**

Drainage Area = 359 acres

**100-year peak flow rate = 813 CFS**

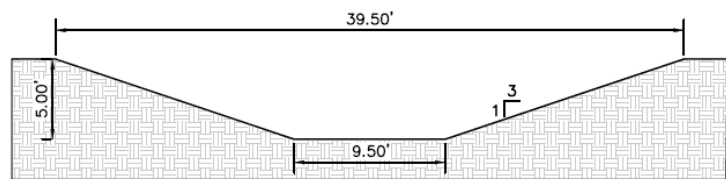
50-year peak flow rate = 668 CFS

25-yr peak flow rate = 536 CFS

10-yr peak flow rate = 380 CFS

5-yr peak flow rate = 275 CFS

2-yr peak flow rate = 153 CFS



PROPOSED SECTION 8

### Observations/Recommendations:

As noted above, this open channel has a theoretical capacity which falls between the 10-year and 25-year peak flow rate. It was also noted that there is some deposition of sediment in the stream which effectively reduces the overall carrying capacity of the Pembroke Avenue closed conduit by about 1½ feet. As such, we recommend a short-term project to remove the sediment deposition along approximately 320 feet of the stream to allow the Pembroke Conduit to freely outfall and utilize its full carrying capacity.

Long term improvements to the stream may include removal of the stone walls to incorporate gradually sloped banks to increase overall capacity. However, these improvements may not be completely warranted since this area is encompassed by the 100-year floodplain as identified by FEMA. As such, these areas are likely to be inundated during the 100-year peak flow rate anyway. A graphic representation of the proposed channel is included above for reference and calculations are provided in Appendix C which demonstrate this channel cross-section would have sufficient capacity to convey the 100-year peak flow rate.



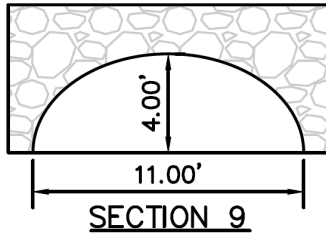
## SECTION 9

### Location:

This culvert is located beneath Meadowbrook Avenue.

### Section Material & Geometry:

This culvert section is an 11 feet wide 4 feet tall stone arch culvert (see graphic representation and photograph below).



### Section Capacity and Reach Geometry:

Length = 33 feet

Measured Reach Slope: -0.1%

Mean Reach slope = 0.27% ±

Manning's n = 0.017

**Theoretical Capacity = 165 CFS**

Drainage Area = 390 acres

**100-year peak flow rate = 858 CFS**

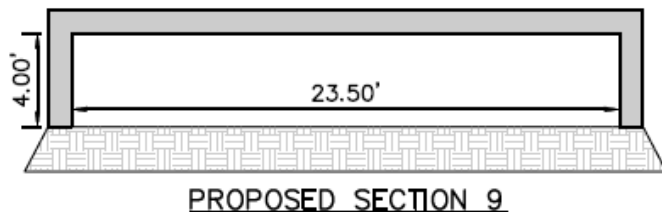
50-year peak flow rate = 705 CFS

25-yr peak flow rate = 566 CFS

10-yr peak flow rate = 402 CFS

5-yr peak flow rate = 292 CFS

2-yr peak flow rate = 162 CFS



### Observations/Recommendations:

The theoretical capacity of this culvert is nearly equivalent to the 2-year peak flow rate and is considered vastly undersized based on the tributary flows. This culvert likely serves as a substantial "choke point" due to its low theoretical capacity and the hydraulic losses of stormwater entering a closed conduit from an open channel.

It is recommended that the Township continue to conduct periodic inspections to verify the integrity of the culvert is intact as is good practice. The Township should also plan to replace culvert in the future largely due to its assumed advanced age as part of the Township's general infrastructure replacement programs. The relative opening of the culvert could be maximized at that time to adequately pass the 100-year peak flow rate. This would result in the culvert being wider (approximately 23 to 24 feet) while maintaining its somewhat limited height at 4 feet. A graphic representation is included above for the proposed box culvert option and calculations are provided in Appendix C of this report which demonstrate the proposed section has sufficient capacity to convey the 100-year peak flow rate. This culvert would be well suited for a CON/SPAN bridge system or twin box culverts.

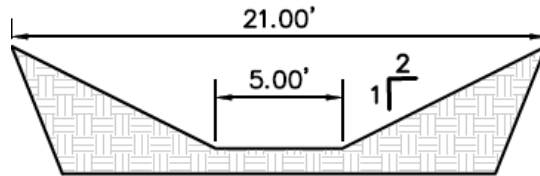
## SECTION 10

### Location:

This section of stream located between Meadowbrook Avenue and Orchard Way.

### Section Material & Geometry:

This section is a 5 feet wide trapezoidal open channel with 2:1 vegetated slopes on the sides (see graphic representation below).



SECTION 10

### Section Capacity and Reach Geometry:

Length = 250 feet

Reach slope = 0.99% ±

Manning's n = 0.024

**Theoretical Capacity = 554 CFS**

Drainage Area = 397 acres

**100-year peak flow rate = 867 CFS**

50-year peak flow rate = 712 CFS

25-yr peak flow rate = 572 CFS

10-yr peak flow rate = 406 CFS

5-yr peak flow rate = 295 CFS

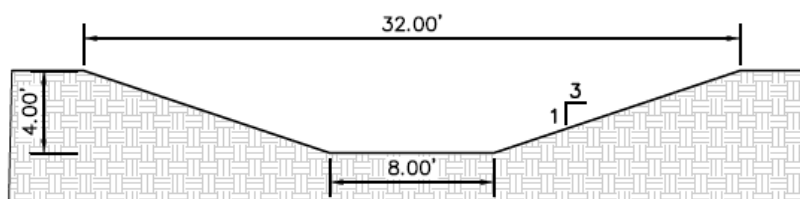
2-yr peak flow rate = 164 CFS

### Observations/Recommendations:

The theoretical capacity of this section falls between the 10-year and 25-year peak flow rate. This only considers flow to the approximate top of bank. In situ, excess flow would inundate the areas surrounding the open channel.

The Township could complete a project to increase the dimensions of the stream to have a bottom width of 8 feet, 3:1 side slopes, and approximately 32 feet top width to accommodate the 100-year peak flow rate and better confine flow to the channel only. However, these improvements may not be completely warranted since this area is encompassed by the 100-year floodplain as identified by FEMA. As such, the stream is likely to be inundated during the 100-year peak flow rate anyway. As such, no improvements are recommended at this time.

In any case, a graphic representation of the proposed channel is included below for reference and calculations are provided in Appendix C which demonstrate this channel cross-section would have sufficient capacity to convey the 100-year peak flow rate.



PROPOSED SECTION 10 AND 11

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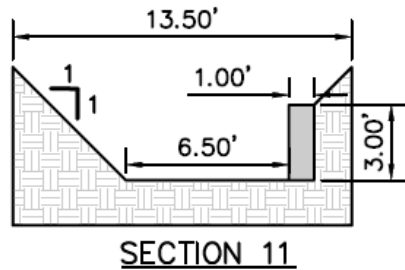
## SECTION 11

### Location:

This section of stream located between Meadowbrook Avenue and Orchard Way.

### Section Material & Geometry:

This section is a 6.5 feet wide trapezoidal open channel with a 1:1 vegetated slopes on the western side and a 3 feet stone wall on the eastern side (see graphic representation below).



### Section Capacity and Reach Geometry:

Length = 210 feet

Reach slope = 0.99% ±

Manning's n = 0.024

**Theoretical Capacity = 429 CFS**

Drainage Area = 403 acres

**100-year peak flow rate = 875 CFS**

50-year peak flow rate = 720 CFS

25-yr peak flow rate = 578 CFS

10-yr peak flow rate = 411 CFS

5-yr peak flow rate = 298 CFS

2-yr peak flow rate = 166 CFS

### Observations/Recommendations:

The theoretical capacity of this section falls between the 10-year and 25-year peak flow rate. This only considers flow to the approximate top of bank. In situ, excess flow would inundate the areas surrounding the open channel.

The Township could complete a project to increase the dimensions of the stream to accommodate the 100-year peak flow rate and better confine flow to the channel only. However, these improvements may not be completely warranted since this area is encompassed by the 100-year floodplain as identified by FEMA. As such, the stream is likely to be inundated during the 100-year peak flow rate anyway. As such, no improvements are recommended at this time.

In any case, a graphic representation of the proposed channel is included above in the Section 10 description for reference and calculations are provided in Appendix C which demonstrate this channel cross-section would have sufficient capacity to convey the 100-year peak flow rate.

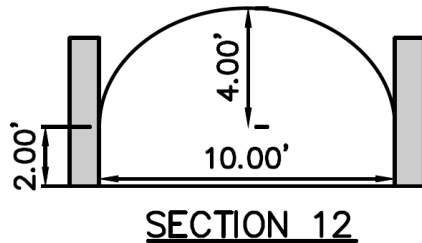
## SECTION 12

### Location:

This section is a brick and stone arch culvert beneath Orchard Way.

### Section Material & Geometry:

This section is a 10 feet wide culvert with 2 feet walls and a 4 feet brick and stone arch (see graphic representation and photograph below).



### Section Capacity and Reach Geometry:

Length = 32 feet

Reach mean slope = 0.92% (mean slope of channel before and after)

Reach measured slope = -2.469%

Manning's n = 0.017

**Theoretical Capacity = 579 CFS**

Drainage Area = 409 acres

**100-year peak flow rate = 884 CFS**

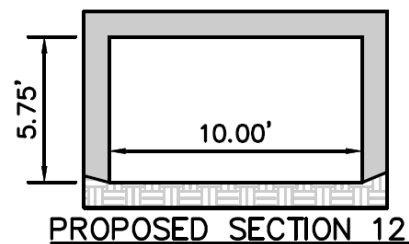
50-year peak flow rate = 727 CFS

25-yr peak flow rate = 584 CFS

10-yr peak flow rate = 415 CFS

5-yr peak flow rate = 301 CFS

2-yr peak flow rate = 168 CFS



### Observations/Recommendations:

The theoretical capacity of the stone culvert falls between the 10-year and 25-year peak flow rate. It is recommended that the Township continue to conduct periodic inspections to verify the integrity of the culvert is intact, as is good practice. The Township should also plan to replace culvert in the future largely due to its assumed advanced age as part of the Township's general infrastructure replacement programs. The relative opening could be maximized at that time to adequately pass the 100-year peak flow rate. The profile of Meadowbrook Drive may also require modifications to eliminate the hump at the culvert. This culvert would be well suited for a CON/SPAN bridge or similar system. The graphic representation of the proposed box culvert is included above for reference and calculations are provided in Appendix C which demonstrate this culvert would have sufficient capacity to convey the 100-year peak flow rate.

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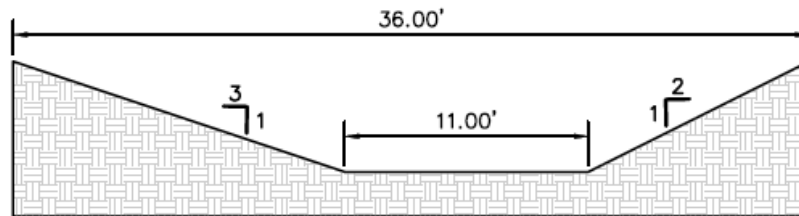
## SECTION 13

### Location:

This section of stream located between Orchard Way and Iven Avenue.

### Section Material & Geometry:

This section is an approximately 10' wide trapezoidal open channel with 1:1 vegetated slopes on the sides (see graphic representation below).



SECTION 13

### Section Capacity and Reach Geometry:

Length = 1,323 feet

Reach slope = 0.62% ±

Manning's n = 0.024

**Theoretical Capacity = 1,216 CFS**

Drainage Area = 524 acres

**100-year peak flow rate = 1,040 CFS**

50-year peak flow rate = 858 CFS

25-yr peak flow rate = 691 CFS

10-yr peak flow rate = 493 CFS

5-yr peak flow rate = 359 CFS

2-yr peak flow rate = 201 CFS

### Observations/Recommendations:

The theoretical capacity of this section appears to be adequate for the 100-year peak flow rate. However, the surrounding areas may still be observed to periodically flood since this reach is encompassed by the 100-year floodplain as identified by FEMA. As such, no major modifications are recommended to this portion of the stream at this time.

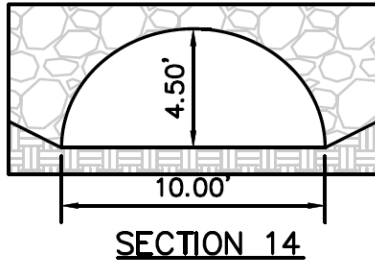
## SECTION 14

### Location:

This section is a stone arch culvert beneath Iven Avenue.

### Section Material & Geometry:

This section is a 10 feet wide culvert with 4½ feet stone arch (see graphic representation and photograph below).



### Section Capacity and Reach Geometry:

Length = 25 feet

Measured Reach Slope = -0.8%

Mean Reach slope = 1.1% ±

Manning's n = 0.017

**Theoretical Capacity = 352 CFS**

Drainage Area = 531 acres

**100-year peak flow rate = 1,040 CFS**

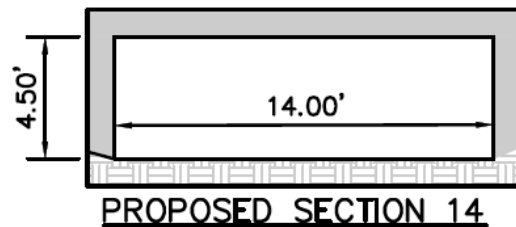
50-year peak flow rate = 858 CFS

25-yr peak flow rate = 691 CFS

10-yr peak flow rate = 493 CFS

5-yr peak flow rate = 359 CFS

2-yr peak flow rate = 201 CFS



### Observations/Recommendations:

The theoretical capacity of this culvert is nearly equivalent to the 5-year peak flow rate and is considered vastly undersized based on the tributary flows. This culvert likely serves as a substantial "choke point" due to its low theoretical capacity and the hydraulic losses of stormwater entering a closed conduit from an open channel. It was also noted that there is some deposition of sediment in the stream which effectively reduces the overall carrying capacity of the Iven Avenue closed conduit by about 1 foot. As such, we recommend a short-term project to remove the sediment deposition along approximately 60 feet of the stream to allow the Iven Avenue culvert to freely outfall and utilize its full carrying capacity. This would be an advantageous time to also to remove any sediment in the adjacent corrugated metal pipe beneath the Township Building entrance drive (Section 15).

It is recommended the Township replace this culvert in the future to increase the opening size to adequately pass the 100-year peak flow rate and reduce any flooding upstream due to this constriction. This would result in the culvert being wider (approximately 14 feet) while maintaining its somewhat limited height at 4½ feet. A graphic representation is included above for the proposed box culvert option and calculations are provided in Appendix C of this

report which demonstrate the proposed section has sufficient capacity to convey the 100-year peak flow rate. This culvert would be well suited for a CON/SPAN bridge or similar system.

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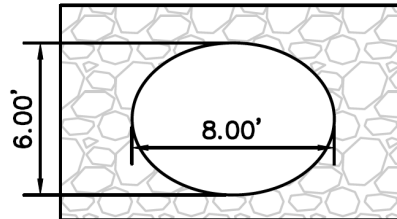
## SECTION 15

### Location:

This section is a corrugated metal culvert beneath the Township Building Entrance Drive.

### Section Material & Geometry:

This section is an 8 feet by 6 feet corrugated metal pipe (see graphic representation and photograph below).



SECTION 15



### Section Capacity and Reach Geometry:

Length = 33 feet

Mean Reach slope = 1.0% ±

Manning's n = 0.019

**Theoretical Capacity = 393 CFS**

Drainage Area = 531 acres

**100-year peak flow rate = 1,040 CFS**

50-year peak flow rate = 858 CFS

25-yr peak flow rate = 691 CFS

10-yr peak flow rate = 493 CFS

5-yr peak flow rate = 359 CFS

2-yr peak flow rate = 201 CFS

### Observations/Recommendations:

The theoretical capacity of this culvert is nearly equivalent to the 5-year peak flow rate and is considered vastly undersized based on the tributary flows. This culvert likely serves as a substantial "choke point" due to its low theoretical capacity and the hydraulic losses of stormwater entering a closed conduit from an open channel.

It is recommended the Township replace this culvert in the future to increase the opening size to adequately pass the 100-year peak flow rate and reduce any flooding upstream due to this constriction. This would result in the culvert being wider (approximately 14 feet) which is similar to what would be required at the culvert crossing Iven Avenue directly upstream. A graphic representation is included under Section 14 above for the proposed box culvert option and calculations are provided in Appendix C of this report which demonstrate the proposed section has sufficient capacity to convey the 100-year peak flow rate. This culvert would be well suited for a CON/SPAN bridge or similar system.



### **III. CONCEPTUAL STORM SEWER IMPROVEMENTS:**

CEC performed an evaluation of Midland Avenue between its intersection with Louella Avenue and Pembroke Avenue and provided plans for conceptual storm sewer improvements in Appendix A of this report. This was also completed for Saint Davids Road between its intersection with South Aberdeen Avenue and Pembroke Avenue. These two (2) roadways were previously identified by municipal personnel as being susceptible to flooding as there was little to no storm sewer present on either roadway.

Stormwater improvements along Midland Avenue were broken into two (2) separate portions. The first of which is located between the intersection of Midland Avenue and South Aberdeen Avenue and the intersection of Midland Avenue and Pembroke Avenue. Sheets C-101 and C-102 in Appendix A depict the improvements along this portion of Midland Avenue which proposes a series of stormwater inlets on the north and south side of the roadway which ultimately discharge to the open channel portion of the stream before it enters the Pembroke Avenue closed conduit. Inlets were spaced at approximately 100 feet and two (2) existing city inlets as well as one (1) stormwater manhole are proposed to be replaced at the intersection of Midland Avenue and Pembroke Avenue. This stormwater system provides a means for conveying runoff from the roadway to the receiving watercourse and does not result in any additional impervious surfaces.

The second portion of Midland Avenue considered is located between its intersections with Louella Avenue and South Aberdeen Avenue. Sheets C-103 and C-104 of Appendix A depict the existing brick culvert along Midland Avenue being replaced with the largest elliptical concrete pipe available which is equivalent to an 84-inch diameter round pipe. This is likely the largest size pipe that can be accommodated in this area due to existing cover available and the adjacent existing utilities. This alternative proposes to modify the existing alignment to remove the portion beneath the Saint Katherines of Sienna School and outfall to the existing open channel on the eastern portion of this parcel. This requires that the existing pedestrian bridge be removed, and the stream lowered by approximately 2½ feet. Inlets were spaced at approximately 100 feet on the north and south side of Midland Avenue with three (3) existing city inlets being replaced.

The conceptual stormwater for Saint Davids Road is included on Sheet C-105 in the Appendix A of this report. The alignment runs west to east with inlets spaced at approximately 100 feet on the north and south side of the roadway and ultimately discharges into the Pembroke conduit where a tie-in will be required.

#### **IV. EVALUATION OF STORM SEWER BYPASS:**

CEC performed an evaluation of a potential storm sewer bypass beginning in the vicinity of the Pembroke Avenue between its intersections with Midland and Saint Davids Road and running east to Encke Park. Survey data was obtained in various areas in Encke Park which was used to determine if there was sufficient slope to accommodate a gravity bypass line. Multiple alignments were examined which the bypass could follow as well as two (2) separate locations for the intake. The alternatives considered were as follows:

1. **Primary Stormwater Bypass Route** – This alignment begins southwest of the intersection of Midland Avenue and Pembroke Avenue where the stream enters the Pembroke closed conduit. From there the bypass would follow the Pembroke Avenue roadway south, proceed east along Saint Davids Road, and continue south along Orchard Way / Meadowbrook Circle. An easement would be required from the resident adjacent from the Township Building Entrance to accommodate the bypass between Meadowbrook Circle and Iven Avenue. Lastly the pipe would proceed to the area designated for a potential future basin in the “Driving Range” portion of Encke Park.
2. **Alternate 1: Stormwater Bypass Route** – This alignment begins southwest of the intersection of Midland Avenue and Pembroke Avenue where the stream enters the Pembroke closed conduit. From there the bypass would follow the Pembroke Avenue roadway south, proceed east along Saint Davids Road, and continue south along Saint Davids Court. An easement would be required from the Radnor Crossing Apartment accommodate the bypass between Saint Davids Court and Iven Avenue. Lastly the pipe would proceed to the area designated for a potential future basin in the “Driving Range” portion of Encke Park.
3. **Alternate 2: Stormwater Bypass Route** – This alignment follows largely the same alignment as the Primary Stormwater Bypass Route noted above with the exception that the location of the intake is moved to an alternate location at Saint Katherines of Sienna School Property.
4. **Alternate 3: Stormwater Bypass Route** – This alignment is directly parallel to the existing stream alignment.

Each alternate was determined to **not be feasible** due to a variety of reasons listed below.

1. The Pembroke closed conduit has capacity for approximately 234 CFS which is deficient by approximately 579 CFS. As such, the proposed gravity bypass would need to exceed the largest elliptical concrete pipe available. For purposes of simplicity, the various bypass profiles in Appendix F depict an 84-inch pipe.
2. Coverage is an insurmountable issue for each bypass alternative. This ranges from coverage being far too great with the deepest excavations ranging from 92 feet and 26 feet for the primary bypass and alternate 1 respectively. Additionally, the gravity bypass has insufficient cover for each alternative as you approach Encke Park leaving large swaths of the pipe exposed. Incorporating additional fill to provide coverage over the pipe would be prohibited since it would result in the placement of fill in the 100-year flood plain areas as identified by FEMA.

3. Although there is technically sufficient fall for the gravity bypass, the receiving regional detention basin would presumably fill with stormwater and create submerged outfall for the gravity bypass. This would limit the hydraulic capacity of the gravity bypass therefore negating its ability to sufficiently bypass flow.
4. Appendix F: also depicts a pressure pipe alternative for each alignment as well. However, this was simply provided for anecdotal reasons as the flow required to be pumped (579 CFS or **260,000 gallons per minute**) would result in a pump station **Six-Times larger** than the largest regional wastewater Pumping Station known to this office (Totem Road Pump Station) having an approximate capacity of 42,000 gallons per minute. A pump station of this size with associated force main would be on the order of \$30 million.
5. A joint permit for the installation of a stormwater gravity bypass would not be able to be obtained due to regulations governing improvement to Waters of the Commonwealth. These DEP regulations typically discourage confining streams to closed conduits, and rather, encourage improvements to existing watercourses which provide added capacity/cross-sectional area and return them to their natural state (i.e., open channels, gradual vegetated banks, etc.).
6. Costs would also be prohibitively expensive for a parallel gravity bypass of the stream with the 3,600 linear feet of 84-inch diameter gravity estimated at approximately \$3.6 million to construct.

**APPENDIX A: EXISTING FEATURES AND CONCEPTUAL STORM SEWER PLANS**

# SOUTH WAYNE DRAINAGE IMPROVEMENTS FEASIBILITY STUDY

SITUATED IN:  
RADNOR TOWNSHIP  
DELAWARE COUNTY, PENNSYLVANIA

PREPARED FOR:  
RADNOR TOWNSHIP  
301 IVEN AVENUE  
WAYNE, PENNSYLVANIA 19087-5297

PREPARED BY:  
*Carroll Engineering Corporation*



949 Easton Road  
Warrington, PA 18976  
Phone: 215-343-5700  
Fax: 215-343-0875

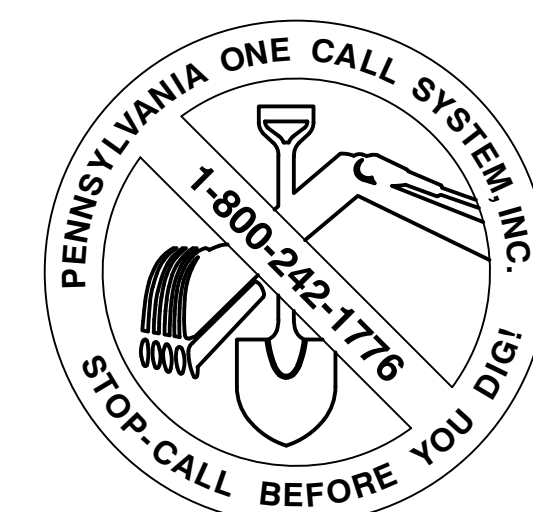
630 Freedom Business Center,  
Third Floor  
King of Prussia, PA 19406  
Phone: 610-572-7093

105 Raider Boulevard, Suite 206  
Hillsborough, NJ 08844  
Phone: 908-874-7500  
Fax: 908-874-5762

433 Lancaster Avenue,  
Suite 200  
Malvern, PA 19355  
Phone: 610-489-5100

[www.carrollengineering.com](http://www.carrollengineering.com)

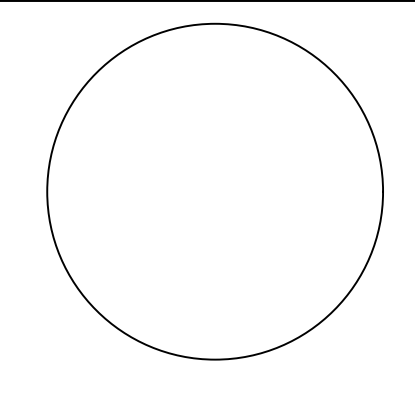
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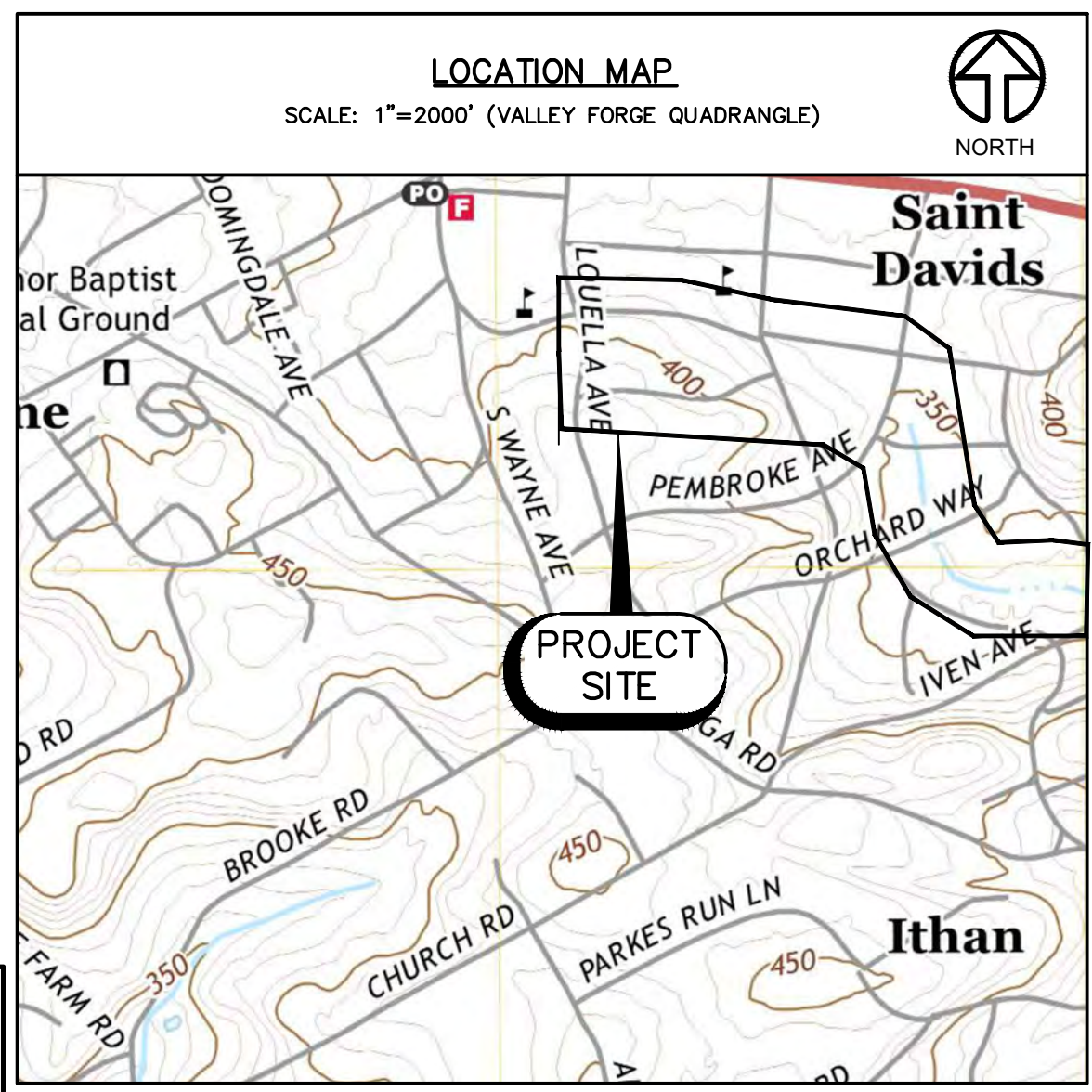
**Carroll Engineering Corporation**  
 CORPORATE OFFICE  
 949 EASTON ROAD  
 WARRINGTON, PA 18976  
 PHONE: 215.343.5700  
 FAX: 215.343.0875  
 630 Freedom Business Ctr., 3rd Fl. 105 Rader Boulevard, Suite 206  
 King of Prussia, PA 19386 Hillborough, NJ 08044  
 Phone: 610.572.7093 Phone: 908.874.7500  
 433 Lancaster Avenue, Suite 200  
 Malvern, PA 19355  
 Phone: 610.489.5100 Fax: 908.874.5102  
 www.carrollengineering.com



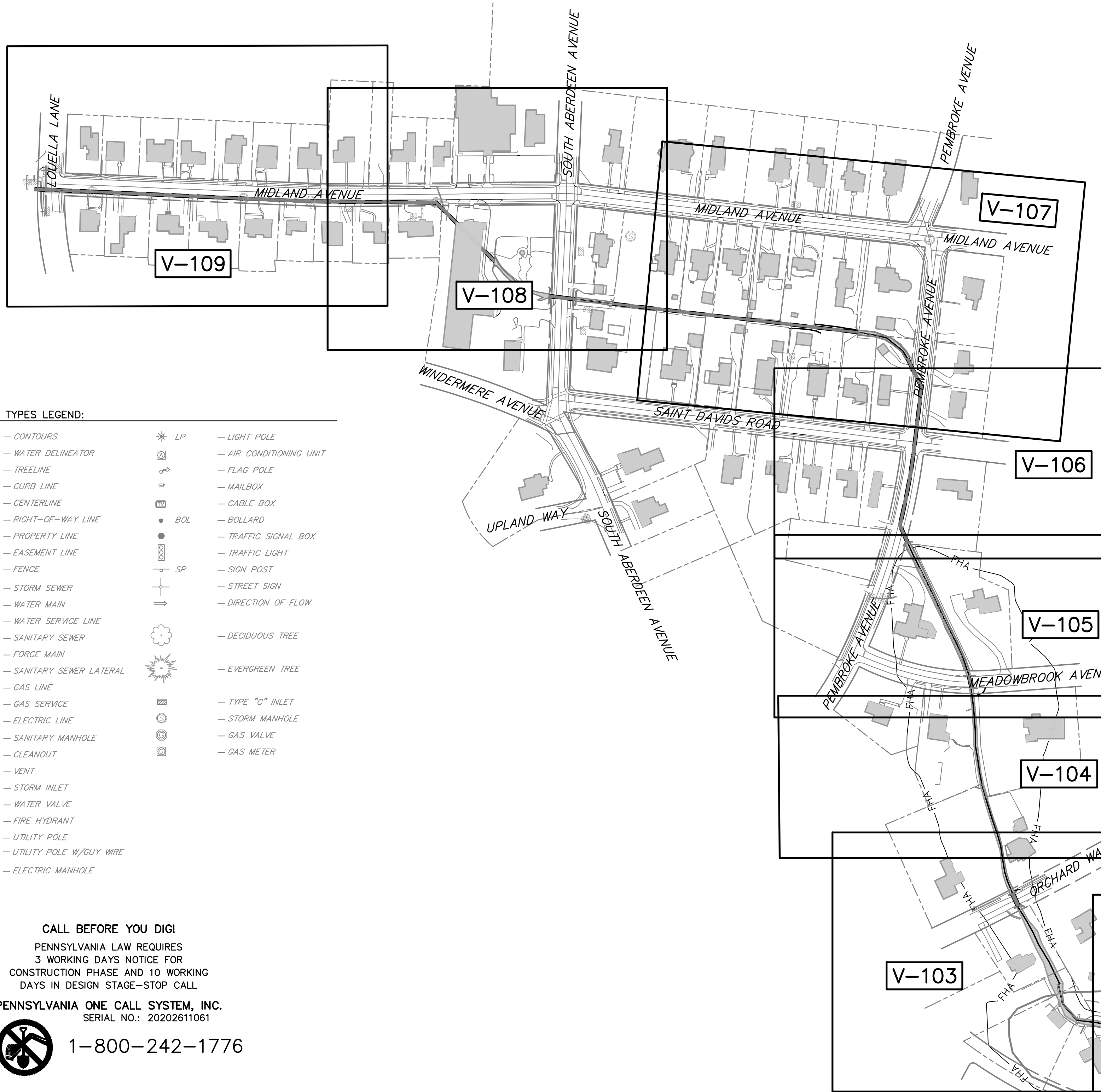
**EXISTING FEATURES INDEX PLAN**  
 SOUTH WAYNE DRAINAGE IMPROVEMENTS  
 FEASIBILITY STUDY  
 SITUATED IN  
 RADNOR TOWNSHIP  
 PREPARED FOR  
 RADNOR TOWNSHIP  
 301 IVEN AVENUE  
 WAYNE, PENNSYLVANIA, 19087-5297

NO.	DATE	DESCRIPTION	INITIALS

DATE: 4-1-2022  
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 JOB NO: 21-1990  
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 DWN BY: TSB  
 CKD BY: CAP  
 SCALE: 1"=150'  
 DRAWER NUMBER: -  
 SHEET 2 OF 17 SHEETS  
 DRAWING NUMBER: G-001



DRAWING INDEX		
SHT. NO.	DWG. NO.	DESCRIPTION
1	-	COVER
2	G-001	EXISTING FEATURES INDEX PLAN
3	V-101	EXISTING FEATURES IVEN AVENUE
4	V-102	EXISTING FEATURES BROOKSIDE AVENUE
5	V-103	EXISTING FEATURES ORCHARD WAY
6	V-104	EXISTING FEATURES PEMBROKE AVENUE & ORCHARD WAY
7	V-105	EXISTING FEATURES PEMBROKE AVENUE & MEADOWBROOK AVENUE
8	V-106	EXISTING FEATURES PLAN PEMBROKE AVENUE & SAINT DAVIDS ROAD
9	V-107	EXISTING FEATURES PLAN PEMBROKE AVENUE & MIDLAND AVENUE
10	V-108	EXISTING FEATURES PLAN SOUTH ABERDEEN & MIDLAND AVENUE
11	V-109	EXISTING FEATURES PLAN MIDLAND AVENUE (WEST)
12	G-002	CONCEPTUAL STORM SEWER INDEX PLAN
13	C-101	CONCEPTUAL STORM SEWER MIDLAND AVENUE BTW PEMBROKE & S. ABERDEEN
14	C-102	CONCEPTUAL STORM SEWER MIDLAND AVENUE BTW PEMBROKE & S. ABERDEEN
15	C-103	CONCEPTUAL STORM SEWER MIDLAND AVENUE BTW LOUELLA & S. ABERDEEN
16	C-104	CONCEPTUAL STORM SEWER MIDLAND AVENUE BTW LOUELLA & S. ABERDEEN
17	C-105	CONCEPTUAL STORM SEWER SAINT DAVIDS BTW PEMBROKE & S. ABERDEEN

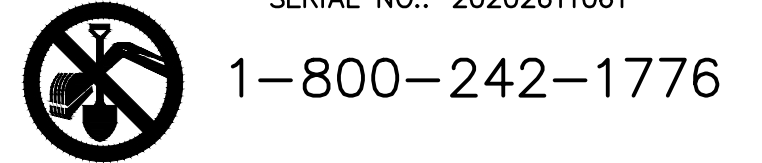


**SYMBOLS / LINE TYPES LEGEND:**

320 - - - - -	CONTOURS	LP	LIGHT POLE
- - - - -	WATER DELINEATOR	ACU	AIR CONDITIONING UNIT
- - - - -	TREELINE	FP	FLAG POLE
- - - - -	CURB LINE	M	MAILBOX
- - - - -	CENTERLINE	CB	CABLE BOX
- - - - -	RIGHT-OF-WAY LINE	BOL	BOLLARD
- - - - -	PROPERTY LINE	TSB	TRAFFIC SIGNAL BOX
- - - - -	EASEMENT LINE	TL	TRAFFIC LIGHT
- - - - -	FENCE	SP	SIGN POST
- - - - -	STORM SEWER	SS	STREET SIGN
W	WATER MAIN	DF	DIRECTION OF FLOW
WS	WATER SERVICE LINE	DT	DECIDUOUS TREE
SS	SANITARY SEWER	ET	EVERGREEN TREE
FM	FORCE MAIN	CI	TYPE "C" INLET
SLAT	SANITARY SEWER LATERAL	SM	STORM MANHOLE
G	GAS LINE	GV	GAS VALVE
GS	GAS SERVICE	GM	GAS METER
E	ELECTRIC LINE		
	SANITARY MANHOLE		
C/O	CLEANOUT		
V	VENT		
SI	STORM INLET		
WV	WATER VALVE		
FH	FIRE HYDRANT		
UP	UTILITY POLE		
	UTILITY POLE W/GUY WIRE		
EM	ELECTRIC MANHOLE		

**CALL BEFORE YOU DIG!**  
 PENNSYLVANIA LAW REQUIRES  
 3 WORKING DAYS NOTICE FOR  
 CONSTRUCTION PHASE AND 10 WORKING  
 DAYS IN DESIGN STAGE--STOP CALL

**PENNSYLVANIA ONE CALL SYSTEM, INC.**  
 SERIAL NO.: 20202611061



**ACT 287 UNDERGROUND USERS LIST**

DESIGN ONE CALL SERIAL NO(S): 20220170662,  
 20220170688, 20220170712, 20220170654, 20220170712,  
 20220171008, 20220271331, 20220272100, 20220201654,

USER	ADDRESS	TELEPHONE/EMAIL
AQUA PENNSYLVANIA, INC.	762 LANCASTER AVENUE BRYN MAWR, PA 19010	SBPZZI@AQUAAMERICA.COM
COMCAST	100 SPRINGBROOKE BLVD ASTON, PA 19014	RICHARD_KAIN@CABLE.COMCAST.COM
PECO ENERGY	450 S. HENDERSON ROAD, SUITE B. KING OF PRUSSIA, PA 19406	484-681-5720
VERIZON PA, INC.	15 MONTGOMERY AVENUE, FLOOR 2 PITTSBURGH, PA 15212	412-359-2000
RADNOR TOWNSHIP	301 IVEN AVENUE WAYNE, PA 19087	SMCNELIS@RADNOR.ORG

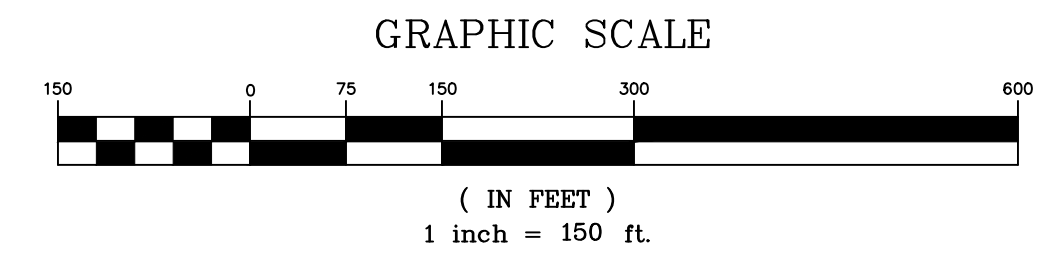
**PA ONE CALL SYSTEM 1-800-242-1776**

LOCATIONS OF EXISTING UTILITIES SHOWN HEREON HAVE BEEN DEVELOPED FROM EXISTING RECORDS AND/OR ABOVE-GROUND OBSERVATIONS AT THE SITE. COMPLETENESS OR ACCURACY OF LOCATION CANNOT BE GUARANTEED. ALL CONTRACTORS AND OTHER PERSONS UTILIZING THIS PLAN AND THE INFORMATION CONTAINED HEREON ARE CAUTIONED TO COMPLY WITH THE REQUIREMENTS OF PENNSYLVANIA ACT 287, AS AMENDED, TITLED "EXCAVATION AND DEMOLITION WORK PROTECTION OF UNDERGROUND UTILITIES." EACH INDIVIDUAL USING THIS PLAN MUST VERIFY THE DEPTH AND LOCATION OF ALL UNDERGROUND FACILITIES BEFORE STARTING WORK.

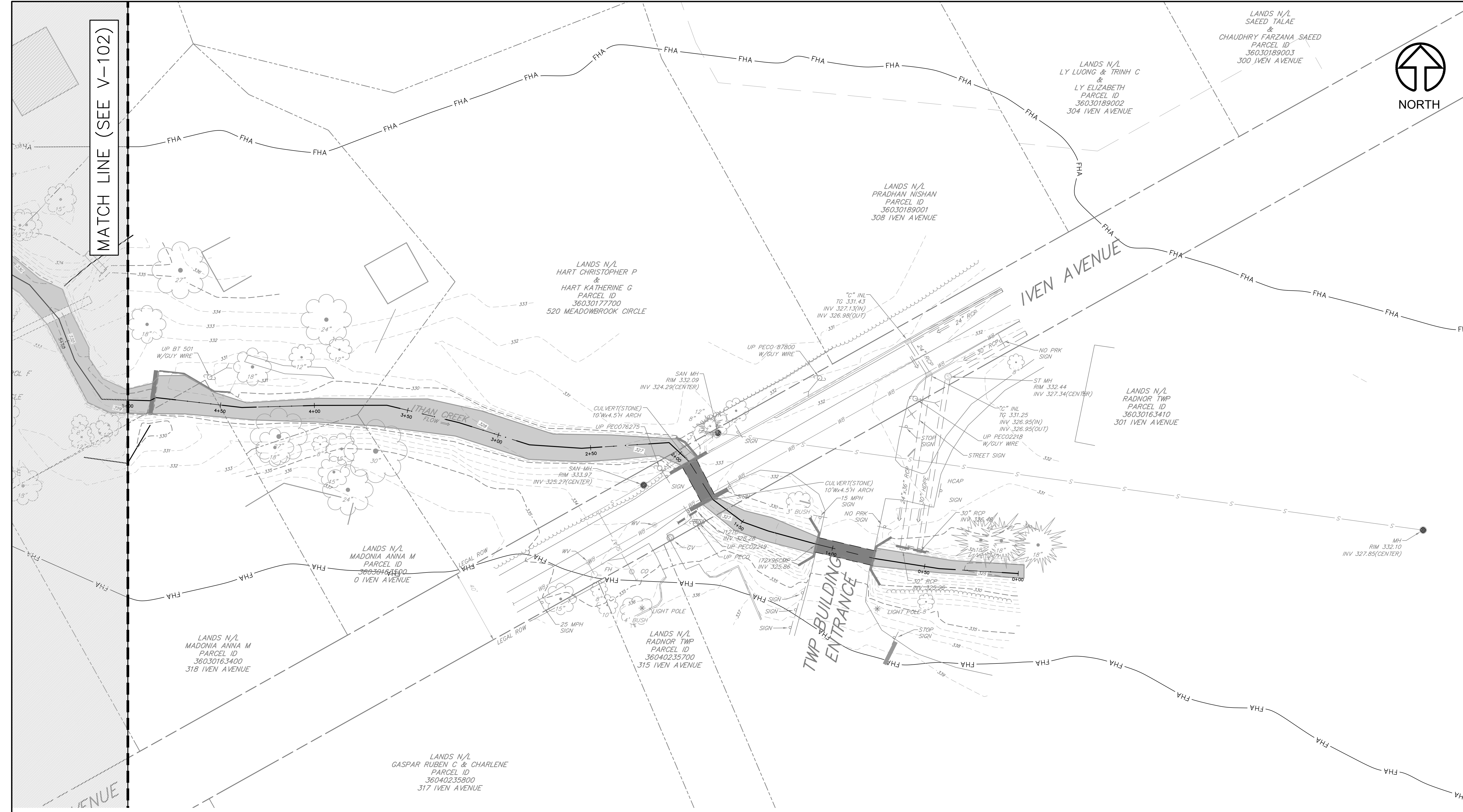
**CALL BEFORE YOU DIG**

"CALL BEFORE YOU DIG" PA ONE CALL AT 1-800-242-1776 IN ACCORDANCE WITH ACT 187 CARROLL ENGINEERING CORPORATION HAS CONTACTED THE PENNSYLVANIA "ONE CALL" SYSTEM. THE SITE SERIAL NUMBERS ARE LISTED NEXT TO THE ONE CALL LOGO THE UTILITIES LISTED ON THIS SHEET HAVE UNDERGROUND FACILITIES LOCATED AT THIS SITE. IT SHALL BE THE DUTY OF EACH CONTRACTOR WHO INTENDS TO PERFORM EXCAVATION OR DEMOLITION WORK AT A SITE WITHIN THIS COMMONWEALTH:

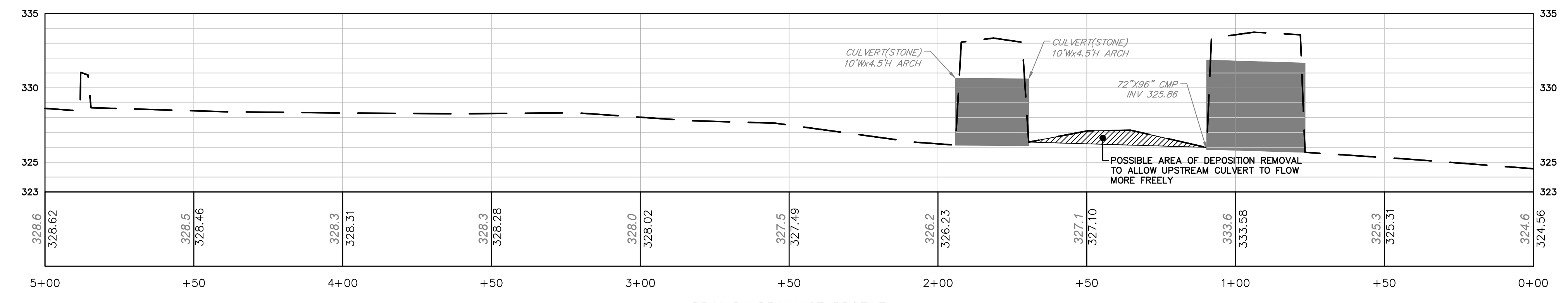
- TO ASCERTAIN THE LOCATIONS AND TYPE OF USERS LINES BY INSPECTION OR DRAWINGS.
- TO SECURE ALL NECESSARY MUNICIPAL PERMITS RELATED TO ROAD OCCUPANCY PRIOR TO COMMENCING EXCAVATION.
- TO NOTIFY EACH USER OF CONTRACTOR'S INTENT TO PERFORM SUCH WORK AT SITE NOT LESS THAN 3 OR MORE THAN 10 WORKING DAYS PRIOR TO THE BEGINNING OF WORK FOR THE PURPOSE OF:
  - REQUEST THE UTILITY TO FIELD LOCATE ITS LINES.
  - INITIATE COOPERATION WHICH WILL AVOID DAMAGE.
  - REQUEST PROCEDURES WHICH WILL AVOID DAMAGE.
- TO INFORM EACH OPERATOR EMPLOYED BY THE CONTRACTOR AT THE SITE OF SUCH WORK OF THE INFORMATION OBTAINED.
- TO REPORT IMMEDIATELY TO THE OCCUPANTS OF THE PREMISES AS TO ANY EMERGENCY THAT THE CONTRACTOR MAY CREATE OR DISCOVER AT OR NEAR SUCH PREMISES.
- TO REPORT IMMEDIATELY TO THE USER ANY BREAK OR LEAK ON ITS LINES OR ANY DENT, GOUGE, GROOVE OR OTHER DAMAGE TO SUCH LINES OR TO THEIR COATING OR CATHODIC PROTECTION, MADE OR DISCOVERED IN THE COURSE OF THE EXCAVATION OR DEMOLITION WORK.
- TO TAKE ALL REASONABLE STEPS NECESSARY TO AVOID INJURY OR OTHERWISE INTERFERE WITH ALL LINES WHERE POSITIONS HAVE BEEN PROVIDED TO THE CONTRACTOR BY USERS.
- TO EMPLOY PRUDENT TECHNIQUES, WHICH MAY INCLUDE HAND-DUG TEST HOLES, TO ASCERTAIN THE PRECISE POSITION OF SUCH FACILITIES.



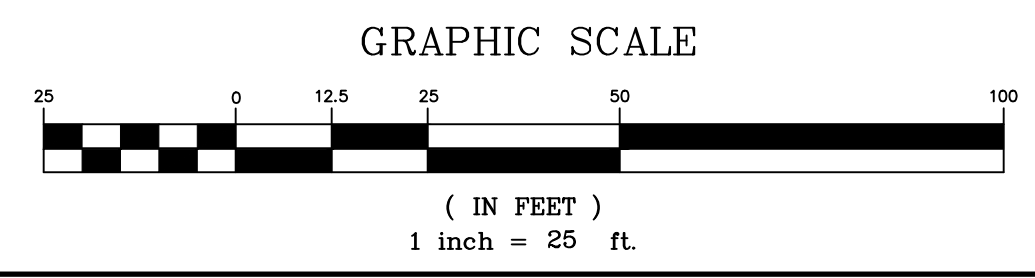
MATCH LINE (SEE V-102)



PLAN  
SCALE: 1"=25'



PRIMARY DRAINAGE PROFILE  
SCALE: HORIZ 1"=25'  
VERT 1"=5'

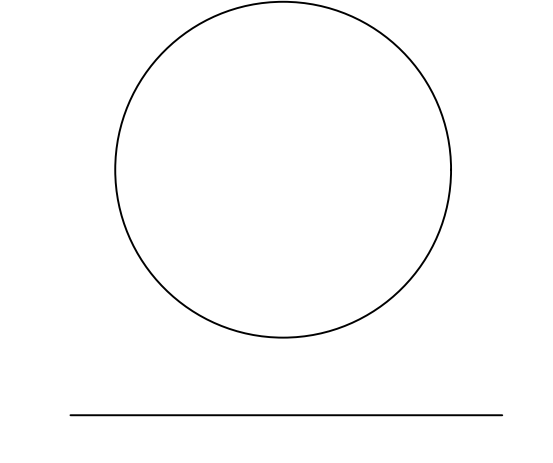


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**EXISTING FEATURES PLAN**  
**IVEN AVENUE**  
**SOUTH WAYNE DRAINAGE IMPROVEMENTS**  
**FEASIBILITY STUDY**  
 SITUATED IN  
 RADNOR TOWNSHIP  
 PREPARED FOR  
**RADNOR TOWNSHIP**  
**301 IVEN AVENUE**  
**WAYNE, PENNSYLVANIA, 19087-5297**

NO.	DATE	DESCRIPTION	INITIALS

DATE: 4-1-2022  
 CADD FILE: 2119900002  
 JOB NO: 21-1990

DSG BY: CAP  
 DWN BY: TSB  
 CKD BY: CAP  
 SCALE: 1"=25'  
 DRAWER NUMBER: -

SHEET 3 OF 17 SHEETS  
 DRAWING NUMBER: V-101

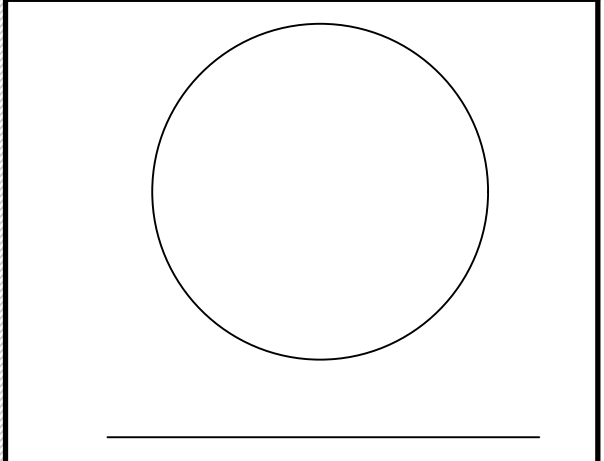
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 Phone: 610.572.7093 Fax: 908.874.7500

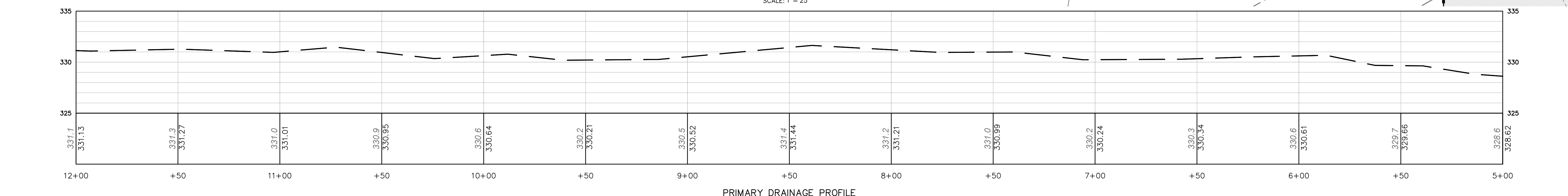
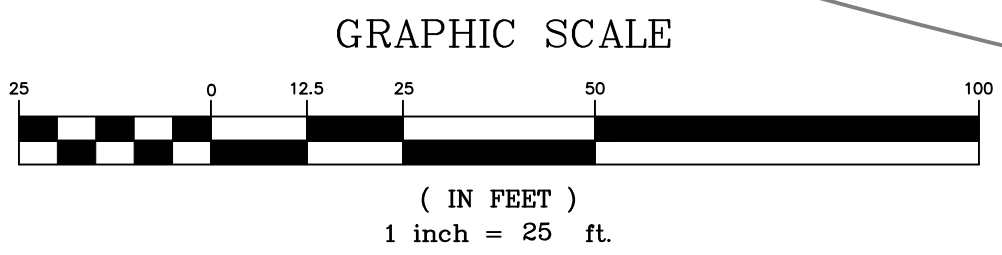
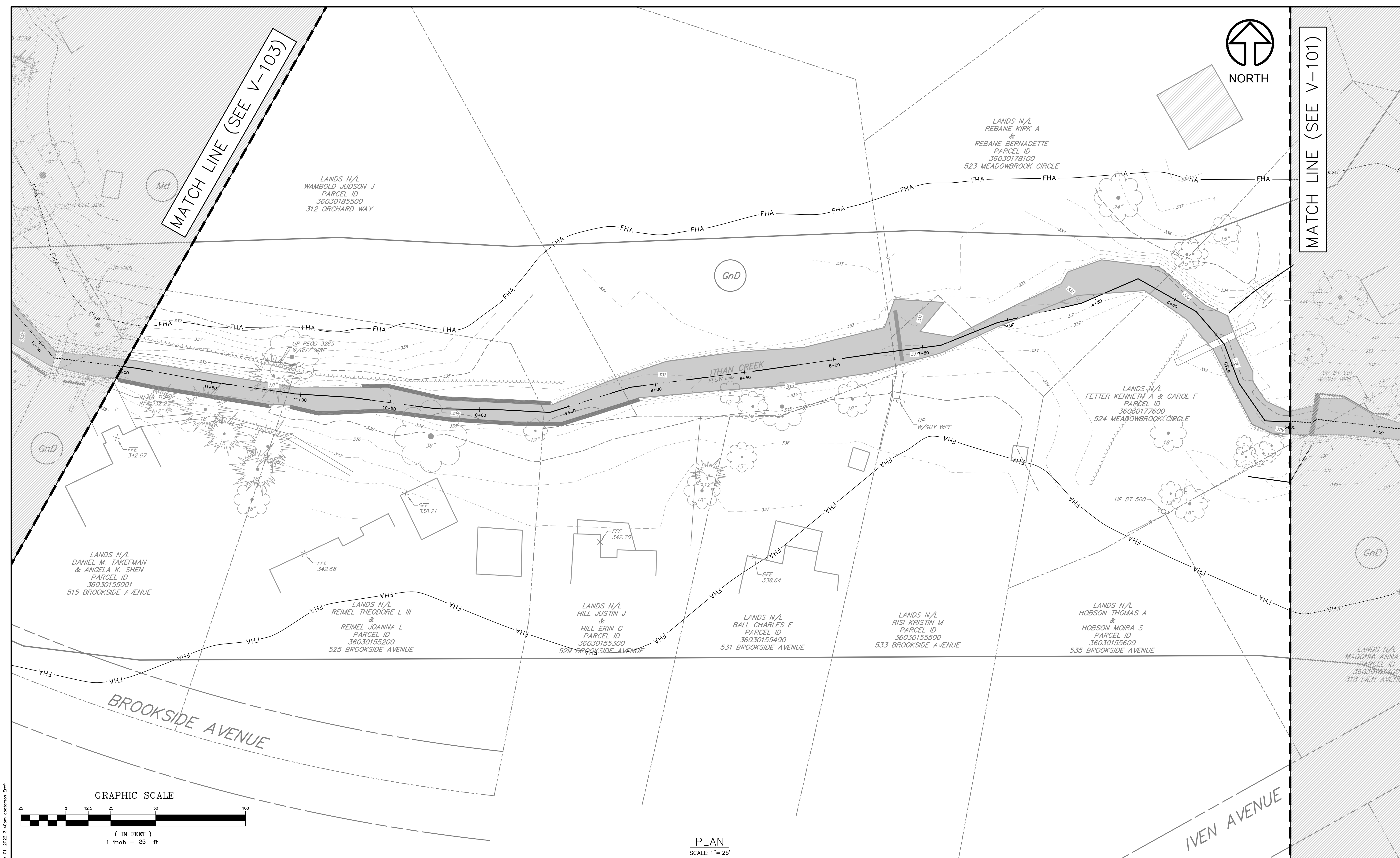
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 Malvern, PA 19355  
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**EXISTING FEATURES PLAN**  
**BROOKSIDE AVENUE**  
**SOUTH WAYNE DRAINAGE IMPROVEMENTS**  
**FEASIBILITY STUDY**  
 SITUATED IN  
 RADNOR TOWNSHIP  
 PREPARED FOR  
**RADNOR TOWNSHIP**  
**301 IVEN AVENUE**  
**WAYNE, PENNSYLVANIA, 19087-5297**

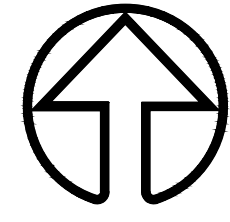
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 JOB NO 21-1990  
 DSG BY CAP  
 DWN BY TSB  
 CKD BY CAP  
 SCALE 1"=25'  
 DRAWER NUMBER -  
 SHEET 4 OF 17 SHEETS  
 DRAWING NUMBER V-102

NO.	DATE	DESCRIPTION	INITIALS



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NORTH

MATCH LINE (SEE V-104)

LANDS N/L  
VULTAGGIO JOSEPH B  
&  
VULTAGGIO LAUREN M  
PARCEL ID  
36030184300  
309 ORCHARD WAY

LANDS N/L  
LEE MAURICE III  
&  
RATH MELINDA G  
PARCEL ID  
36030185700  
320 ORCHARD WAY

LANDS N/L  
HANNUM THOMAS B III  
&  
HANNUM KIMBERLY  
PARCEL ID  
36030185600  
316 ORCHARD WAY

LANDS N/L  
ARNOLD KARA HANLON  
PARCEL ID  
36030185400  
310 ORCHARD WAY

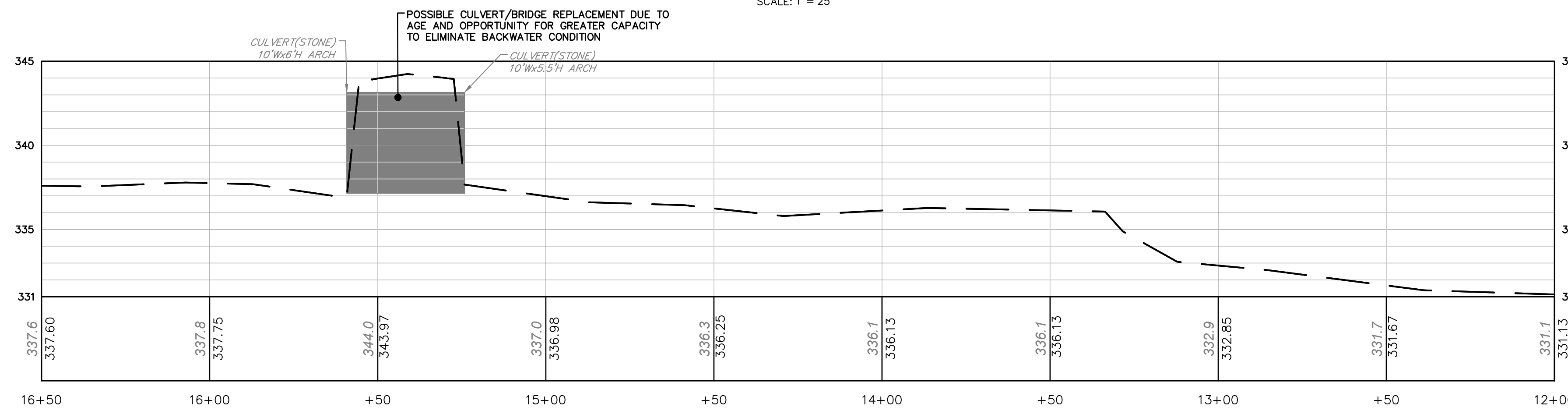
LANDS N/L  
WHITAKER BRANDON  
&  
WHITAKER RORY  
PARCEL ID  
36030155100  
306 ORCHARD WAY

LANDS N/L  
WHITAKER BRANDON  
&  
WHITAKER RORY  
PARCEL ID  
36030155100  
306 ORCHARD WAY

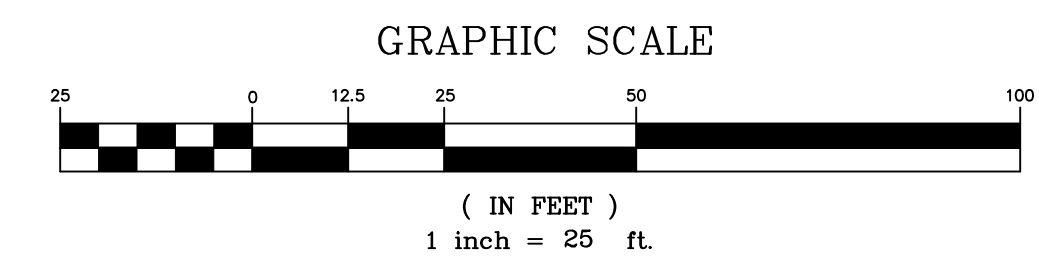
LANDS N/L  
TAKEFMAN DANIEL M  
&  
SHEN ANGELA K  
PARCEL ID  
36030155001  
515 BROOKSIDE AVENUE

LANDS N/L  
WAMBOLD JUDSON J  
PARCEL ID  
36030185500  
312 ORCHARD WAY

PLAN  
SCALE: 1"=25'



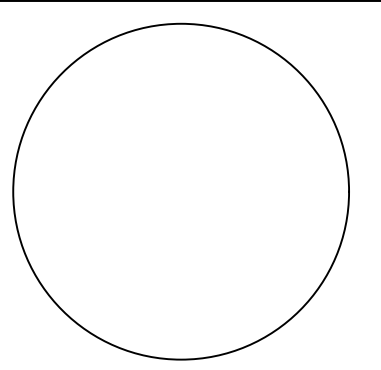
PRIMARY DRAINAGE PROFILE  
SCALE: HORIZ 1"=25'  
VERT 1"=5'



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EXISTING FEATURES PLAN  
ORCHARD WAY  
SOUTH WAYNE DRAINAGE IMPROVEMENTS  
FEASIBILITY STUDY  
SITUATED IN  
RADNOR TOWNSHIP  
PREPARED FOR  
RADNOR TOWNSHIP  
301 IVEN AVENUE  
WAYNE, PENNSYLVANIA, 19087-5297

NO.	DATE	DESCRIPTION	INITIALS

DATE 4-1-2022  
 CADD FILE 2119900002  
 JOB NO 21-1990  
 DSG BY CAP  
 DWN BY TSB  
 CKD BY CAP  
 SCALE 1"=25'  
 DRAWER NUMBER -  
 SHEET 5 OF 17 SHEETS  
 DRAWING NUMBER  
**V-103**



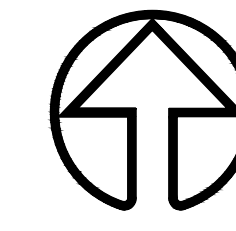
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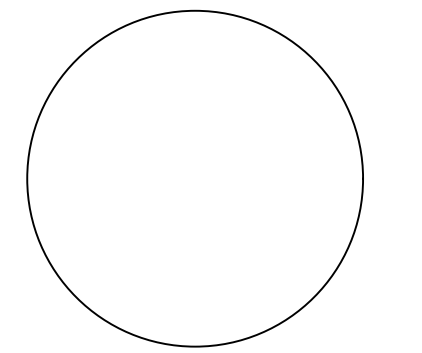
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NORTH



EXISTING FEATURES PLAN  
MEADOWBROOK AVENUE & ORCHARD WAY  
SOUTH WAYNE DRAINAGE IMPROVEMENTS  
FEASIBILITY STUDY

SITUATED IN  
RADNOR TOWNSHIP  
PREPARED FOR  
RADNOR TOWNSHIP  
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WAYNE, PENNSYLVANIA, 19087-5297

NO.	DATE	DESCRIPTION	INITIALS

DATE 4-1-2022  
CADD FILE 2119900002  
JOB NO 21-1990

DSG BY CAP  
DWN BY TSB  
CKD BY CAP  
SCALE 1"=25'

DRAWER NUMBER -  
SHEET 6 OF 17 SHEETS

DRAWING NUMBER  
V-104

MATCH LINE (SEE V-104)

MATCH LINE (SEE V-103)

PEMBROKE AVENUE

MEADOWBROOK AVENUE

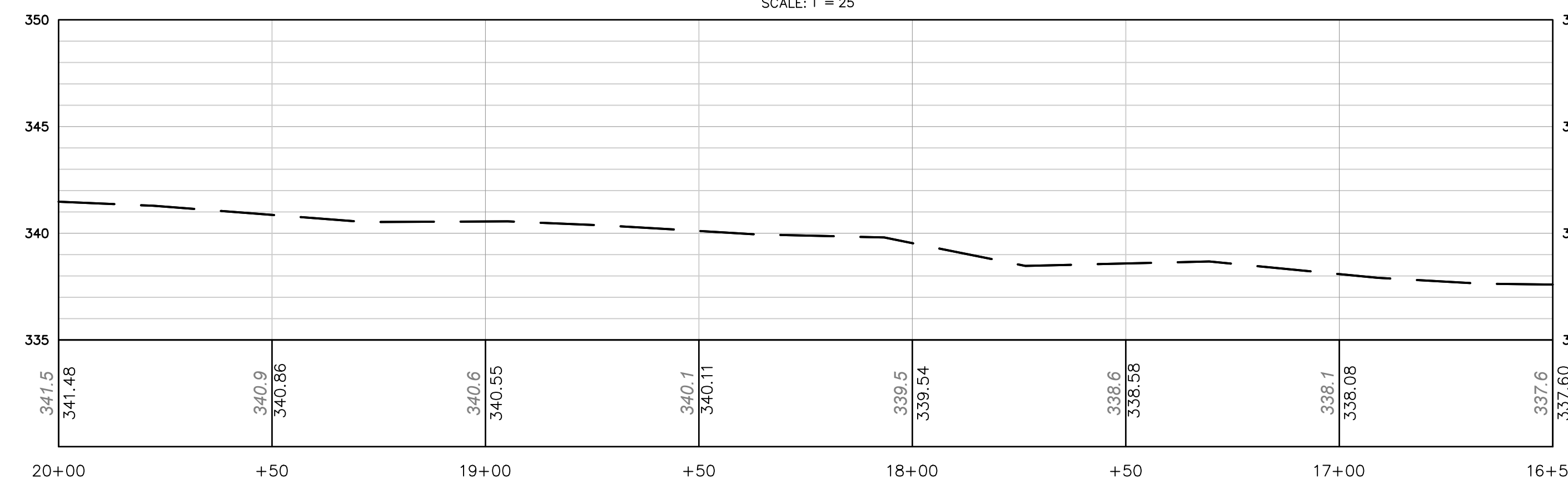
LANDS N/L  
RENEHAN JOHN B JR & PATRICIA  
PARCEL ID  
36030176901  
400 MEADOWBROOK AVENUE

LANDS N/L  
HAUCK KHAREN  
&  
HAUCK CHRISTOPHER  
PARCEL ID  
36030177000  
410 MEADOWBROOK AVENUE

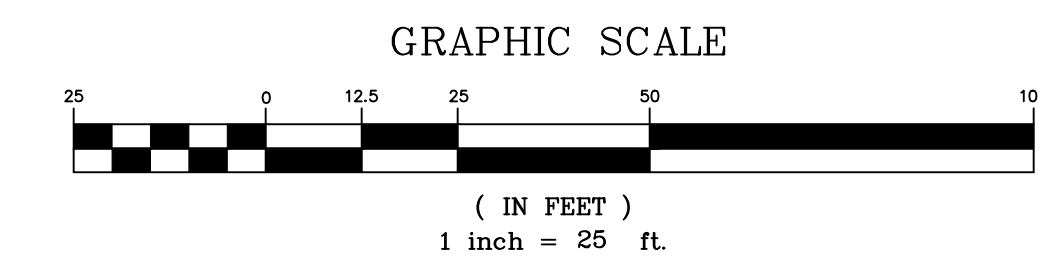
LANDS N/L  
BUCKLEY MORTIMER J III  
&  
NORRIS ELIZABETH A  
PARCEL ID  
36030176400  
420 MEADOWBROOK AVENUE

LANDS N/L  
ZISMAN MICHAEL D  
&  
GAMBLE LINDA J  
PARCEL ID  
36030184400  
311 ORCHARD WAY

PLAN  
SCALE: 1"=25'



PRIMARY DRAINAGE PROFILE  
SCALE: HORIZ 1"=25'  
VERT 1"=5'



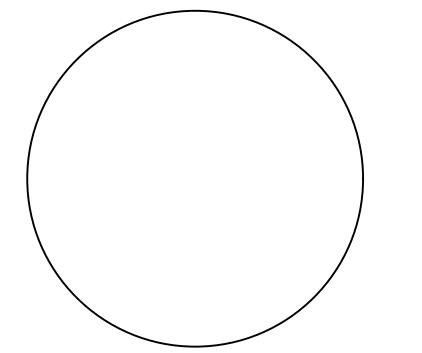


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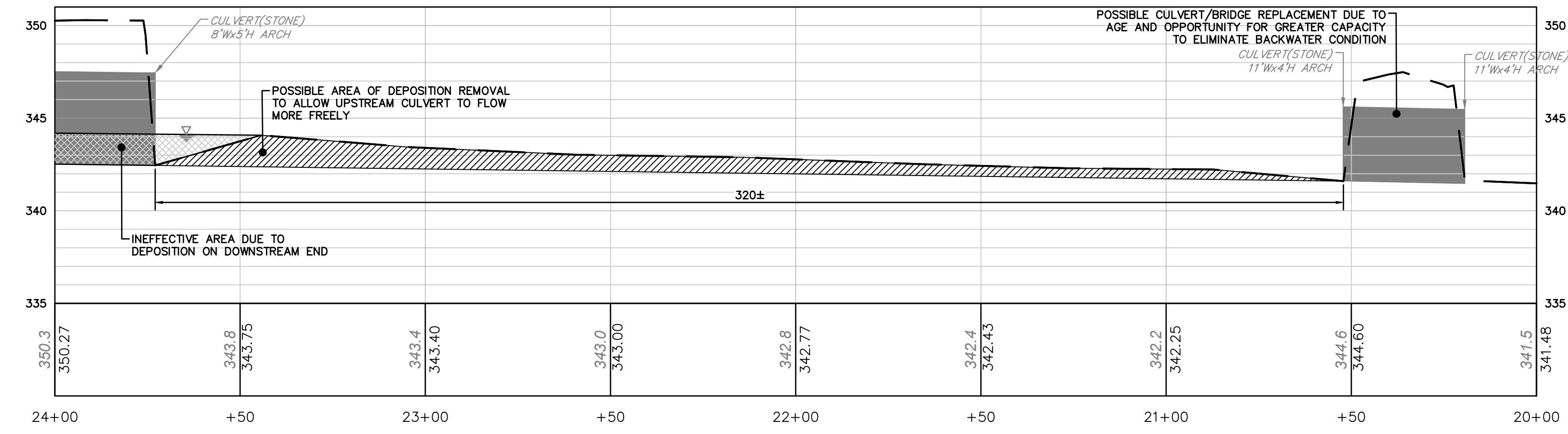


MATCH LINE (SEE V-106)

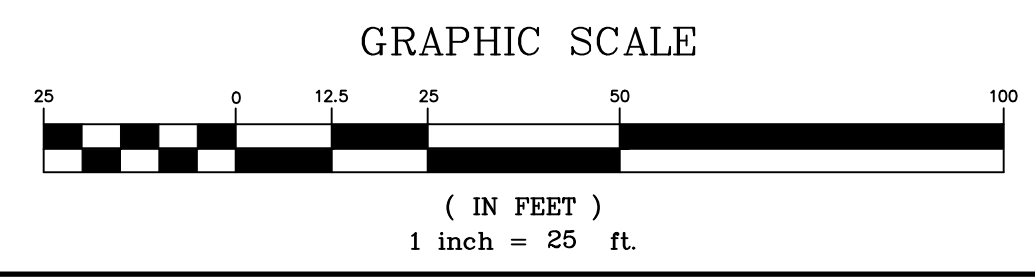
MATCH LINE (SEE V-104)



PLAN  
 SCALE: 1"=25'



PRIMARY DRAINAGE PROFILE  
 SCALE: HORIZ 1"=25'  
 VERT 1"=5'



EXISTING FEATURES PLAN  
 PEMBROKE AVENUE & MEADOWBROOK AVENUE  
 SOUTH WAYNE DRAINAGE IMPROVEMENTS  
 FEASIBILITY STUDY  
 SITUATED IN  
 RADNOR TOWNSHIP  
 PREPARED FOR  
 RADNOR TOWNSHIP  
 301 IVEN AVENUE  
 WAYNE, PENNSYLVANIA, 19087-5297

NO.	DATE	DESCRIPTION	INITIALS

DATE 4-1-2022  
 CADD FILE 2119900002  
 JOB NO 21-1990  
 DSG BY CAP  
 DWN BY TSB  
 CKD BY CAP  
 SCALE 1"=25'  
 DRAWER NUMBER -  
 SHEET 7 OF 17 SHEETS  
 DRAWING NUMBER V-105

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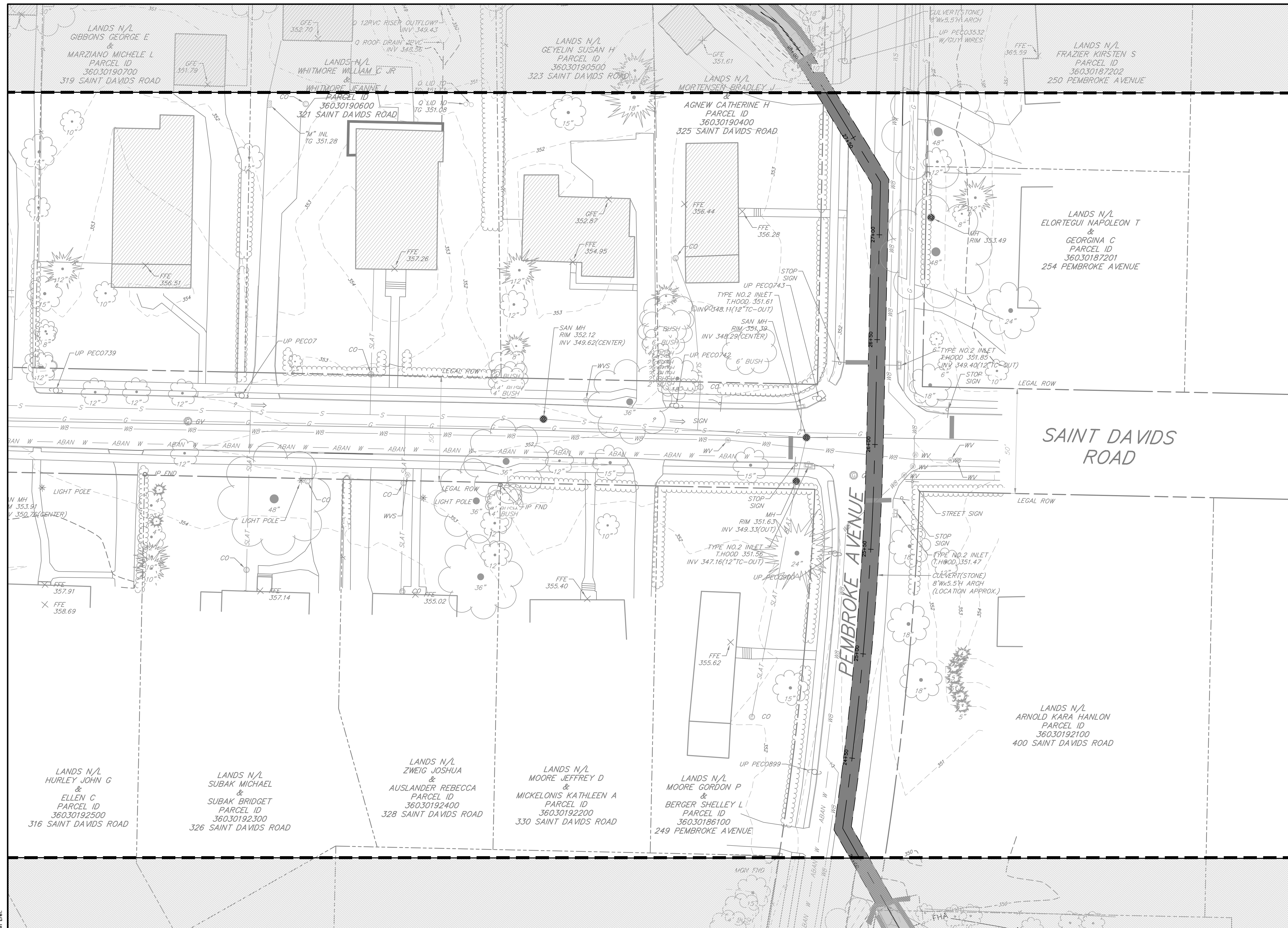
630 Freedom Business Ctr., 3rd Fl. 105 Rader Boulevard, Suite 206  
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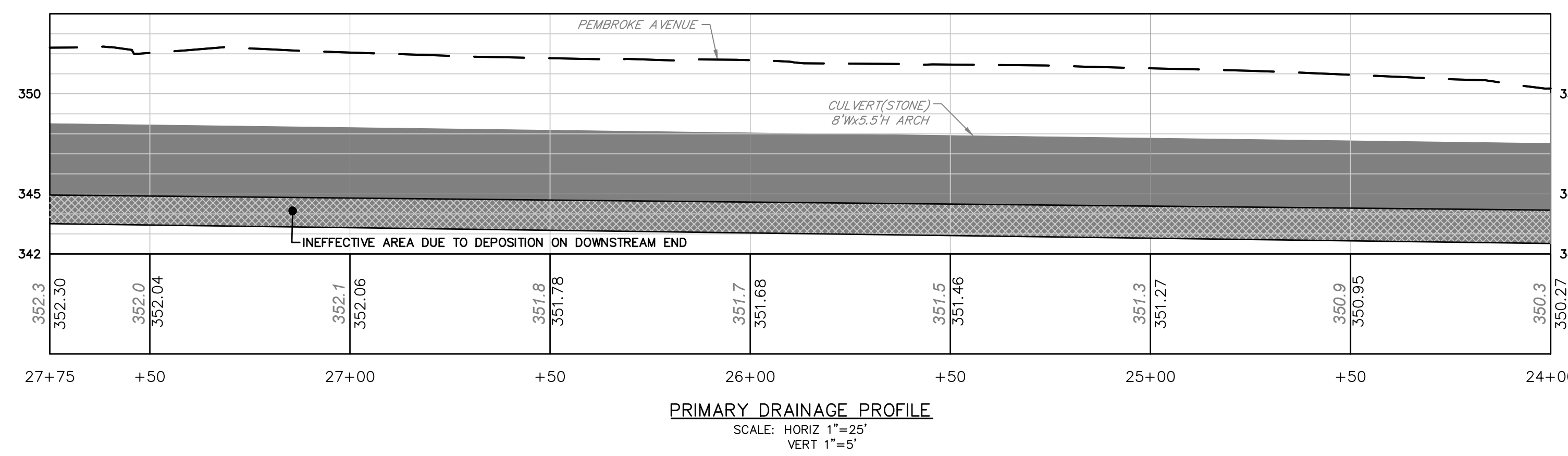
NORTH

MATCH LINE (SEE V-107)

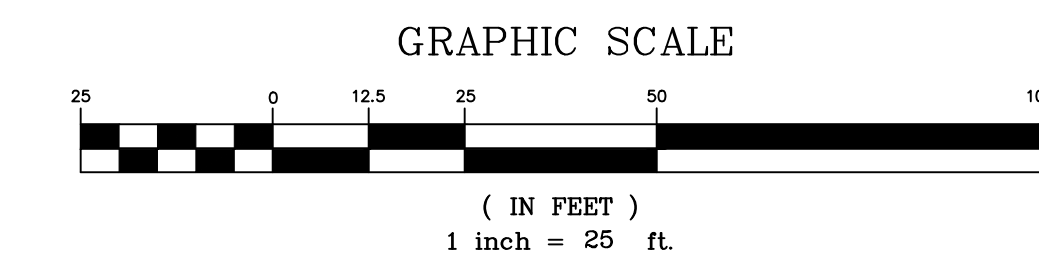


PLAN  
 SCALE: 1"=25'

MATCH LINE (SEE V-105)



PRIMARY DRAINAGE PROFILE  
 SCALE: HORIZ 1"=25'  
 VERT 1"=5'



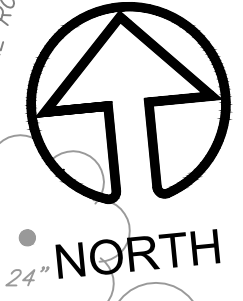
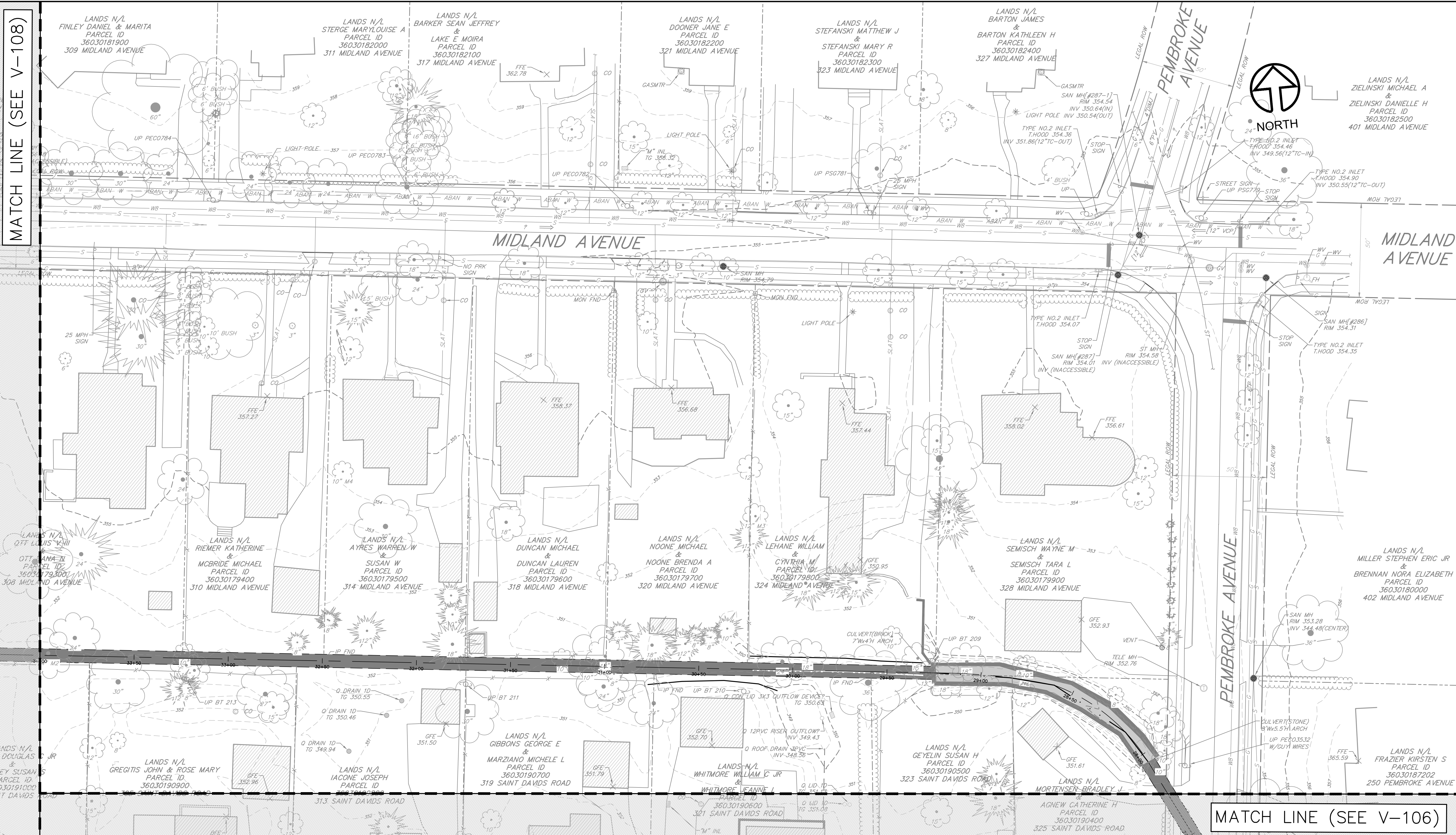
EXISTING FEATURES PLAN  
 PEMBROKE AVENUE & SAINT DAVIDS ROAD  
 SOUTH WAYNE DRAINAGE IMPROVEMENTS  
 FEASIBILITY STUDY  
 SITUATED IN  
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NO.	DATE	DESCRIPTION	INITIALS

DATE 4-1-2022  
 CADD FILE 2119900002  
 JOB NO 21-1990  
 DSG BY CAP  
 DWN BY TSB  
 CKD BY CAP  
 SCALE 1"=25'  
 DRAWER NUMBER -  
 SHEET 8 OF 17 SHEETS  
 DRAWING NUMBER  
 V-106

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MATCH LINE (SEE V-108)

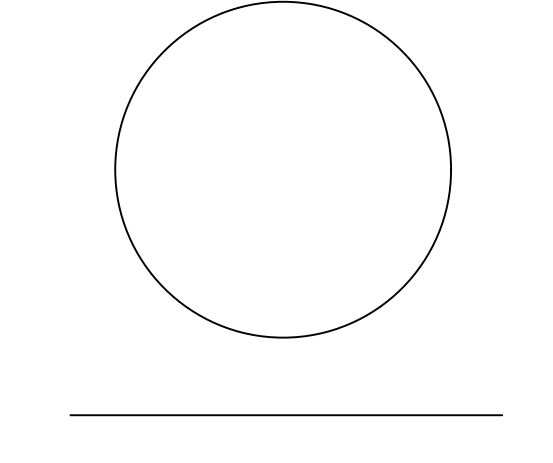


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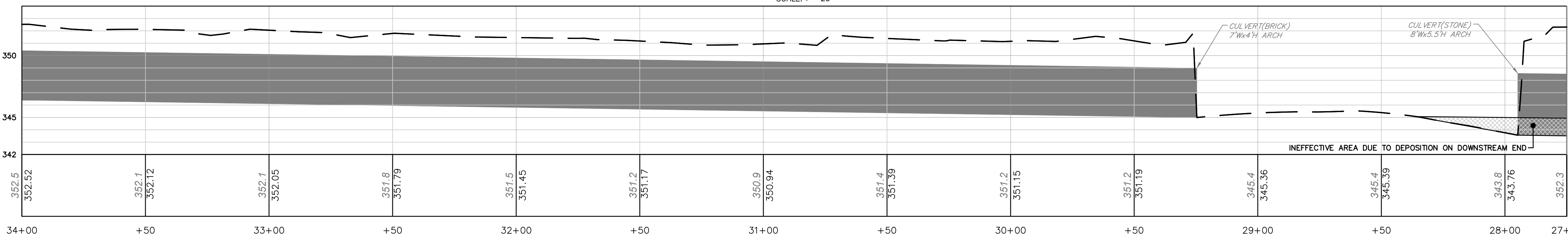


**EXISTING FEATURES PLAN**  
**PEMBROKE AVENUE & MIDLAND AVENUE**  
**SOUTH WAYNE DRAINAGE IMPROVEMENTS**  
**FEASIBILITY STUDY**

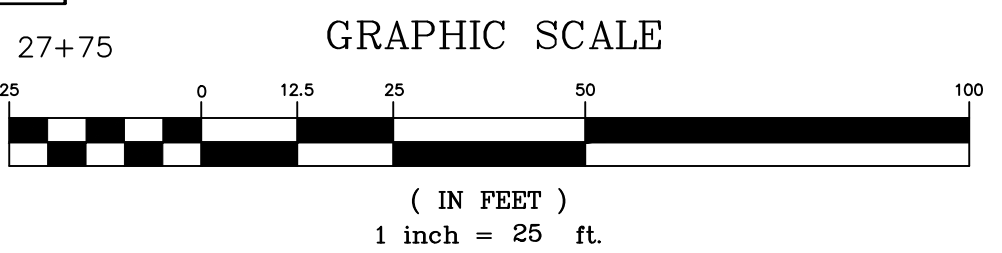
SITUATED IN  
 RADNOR TOWNSHIP  
 PREPARED FOR  
**RADNOR TOWNSHIP**  
 301 IVEN AVENUE  
 WAYNE, PENNSYLVANIA, 19087-5297

PLAN  
 SCALE: 1" = 25'

MATCH LINE (SEE V-106)



PRIMARY DRAINAGE PROFILE  
 SCALE: HORIZ 1" = 25'  
 VERT 1" = 5'



NO.	DATE	DESCRIPTION	INITIALS

DATE	4-1-2022
CADD FILE	211990002
JOB NO	21-1990
DSG BY	CAP
DWN BY	TSB
CKD BY	CAP
SCALE	1"=25'
DRAWER NUMBER	-
SHEET	9 OF 17 SHEETS
DRAWING NUMBER	V-107

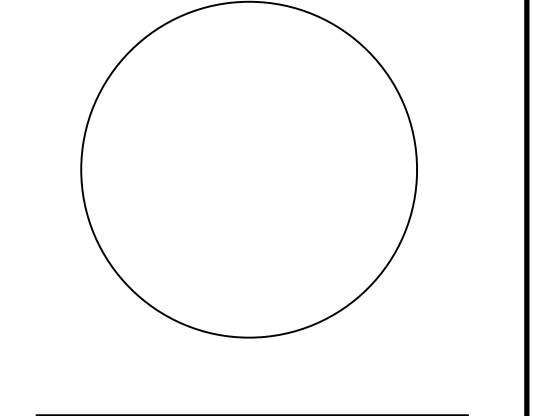
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**EXISTING FEATURES PLAN**  
**SOUTH ABERDEEN AVENUE & MIDLAND AVENUE**  
**SOUTH WAYNE DRAINAGE IMPROVEMENTS**  
**FEASIBILITY STUDY**  
 SITUATED IN  
 RADNOR TOWNSHIP  
 PREPARED FOR  
**RADNOR TOWNSHIP**  
**301 IVEN AVENUE**  
**WAYNE, PENNSYLVANIA, 19087-5297**

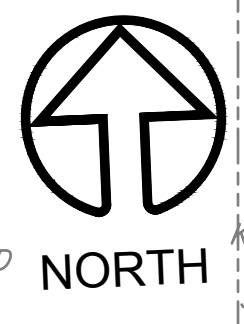
NO.	DATE	DESCRIPTION

DATE	4-1-2022
CADD FILE	2119900002
JOB NO	21-1990
DSG BY	CAP
DWN BY	TSB
CKD BY	CAP
SCALE	1"=25'
DRAWER NUMBER	-
SHEET	10 OF 17 SHEETS

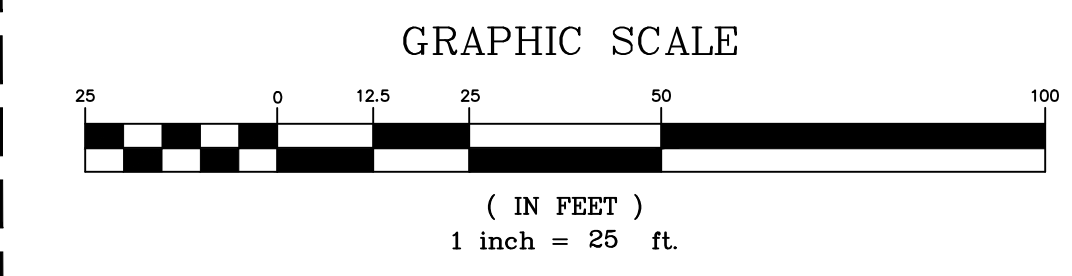
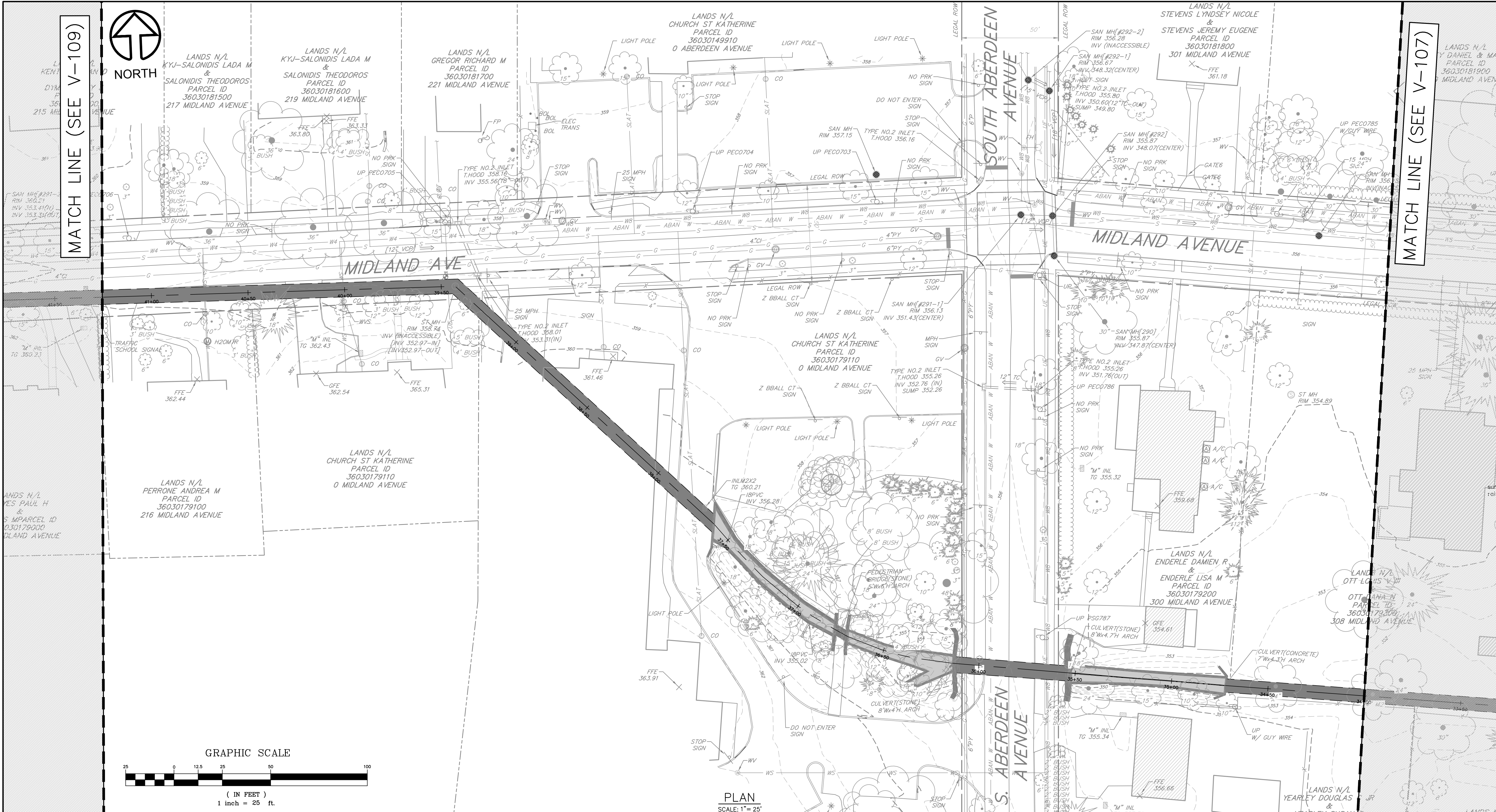
DRAWING NUMBER  
**V-108**

MATCH LINE (SEE V-109)

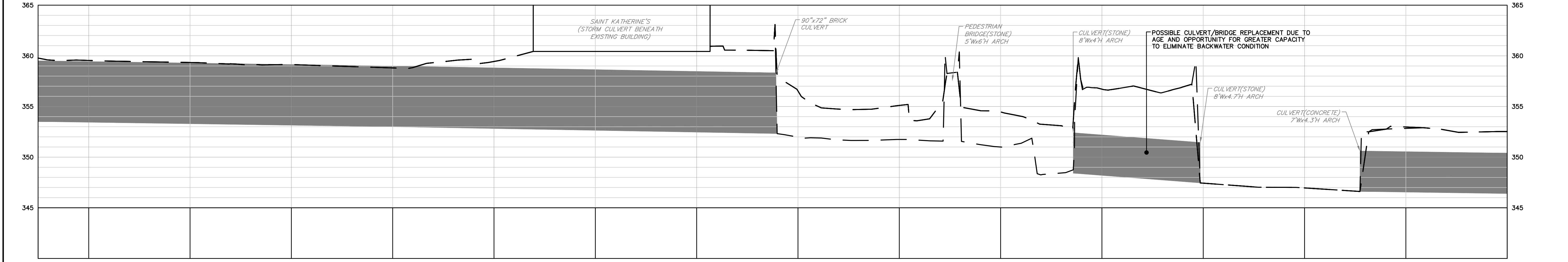
MATCH LINE (SEE V-107)



**NORTH**

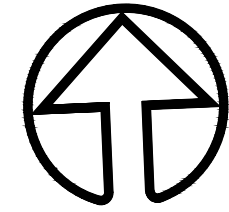


**PLAN**  
 SCALE: 1"=25'



**PRIMARY DRAINAGE PROFILE**  
 SCALE: HORIZ 1"=25'  
 VERT 1"=5'

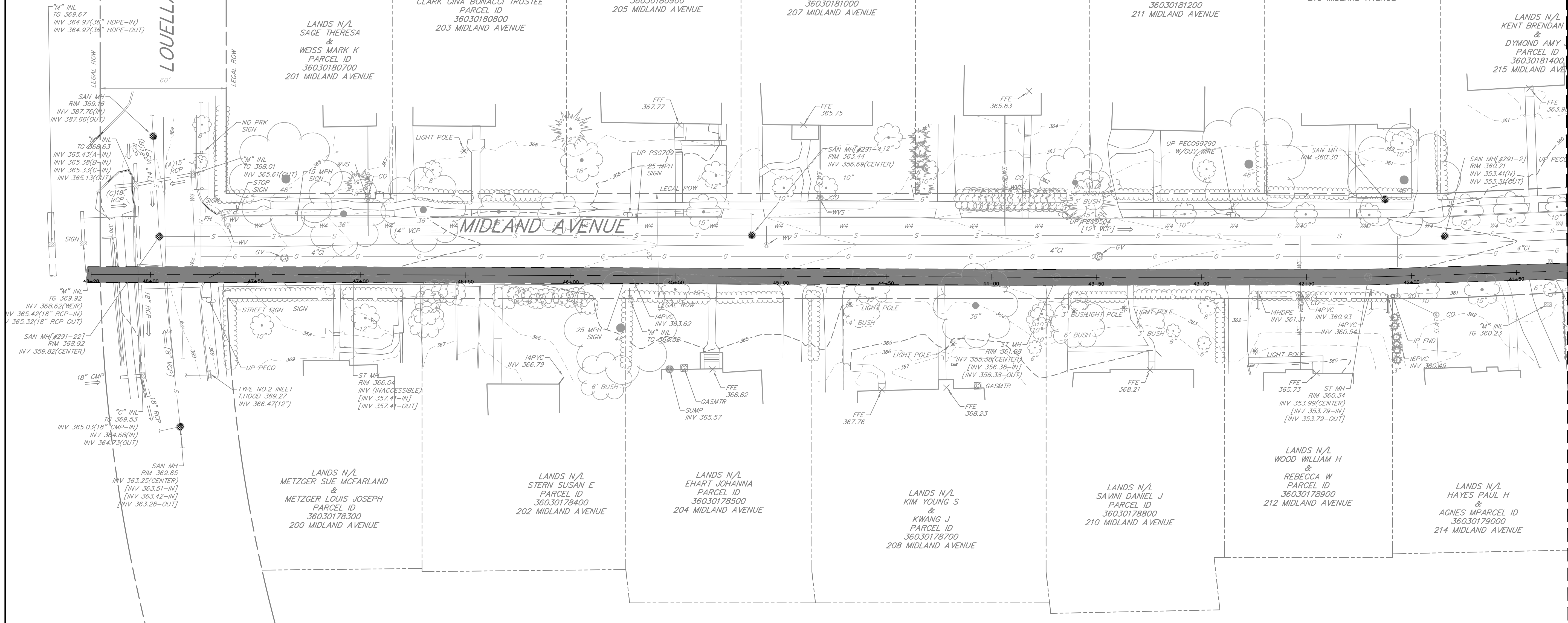
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NORTH

LOUELLA LANE

60'



PLAN  
SCALE: 1" = 25'

MATCH LINE (SEE V-108)

EXISTING FEATURES PLAN  
MIDLAND AVENUE (WEST)

SOUTH WAYNE DRAINAGE IMPROVEMENTS  
FEASIBILITY STUDY

SITUATED IN  
RADNOR TOWNSHIP  
PREPARED FOR  
RADNOR TOWNSHIP  
301 IVEN AVENUE  
WAYNE, PENNSYLVANIA, 19087-5297

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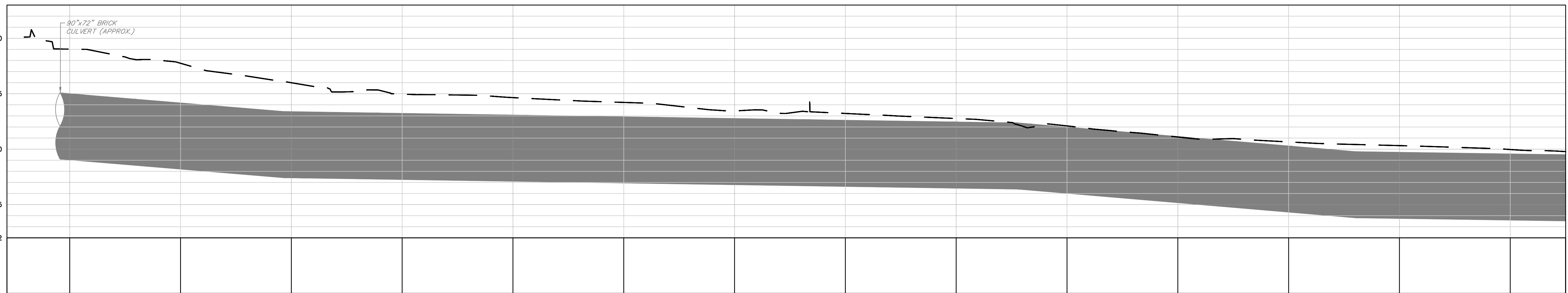
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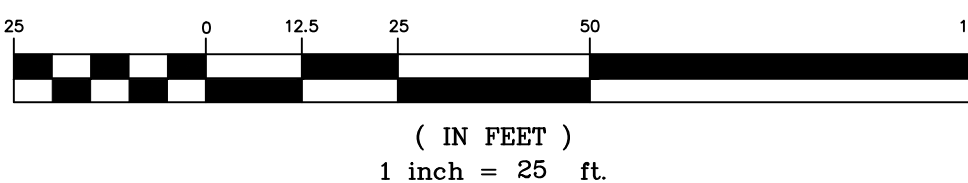
NO.	DATE	DESCRIPTION	INITIALS

DATE	4-1-2022
CADD FILE	2119900002
JOB NO	21-1990
DSG BY	CAP
DWN BY	TSB
CKD BY	CAP
SCALE	1"=25'
DRAWER NUMBER	-
SHEET	11 OF 17 SHEETS
DRAWING NUMBER	V-109



PRIMARY DRAINAGE PROFILE  
SCALE: HORIZ 1"=25'  
VERT 1"=5'

GRAPHIC SCALE



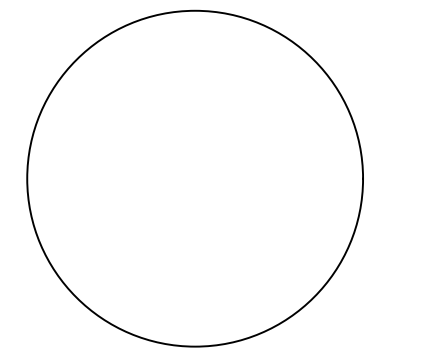
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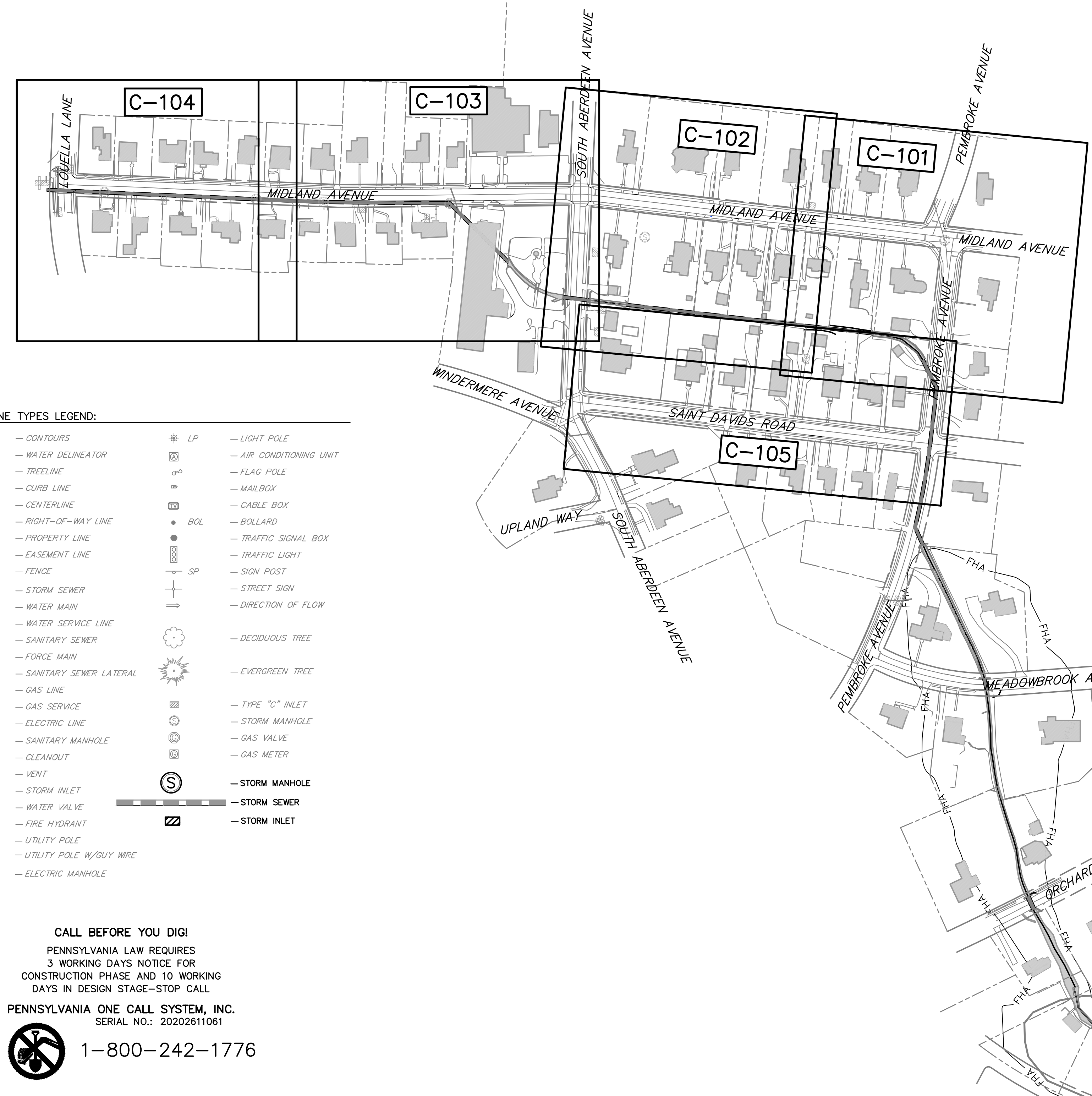
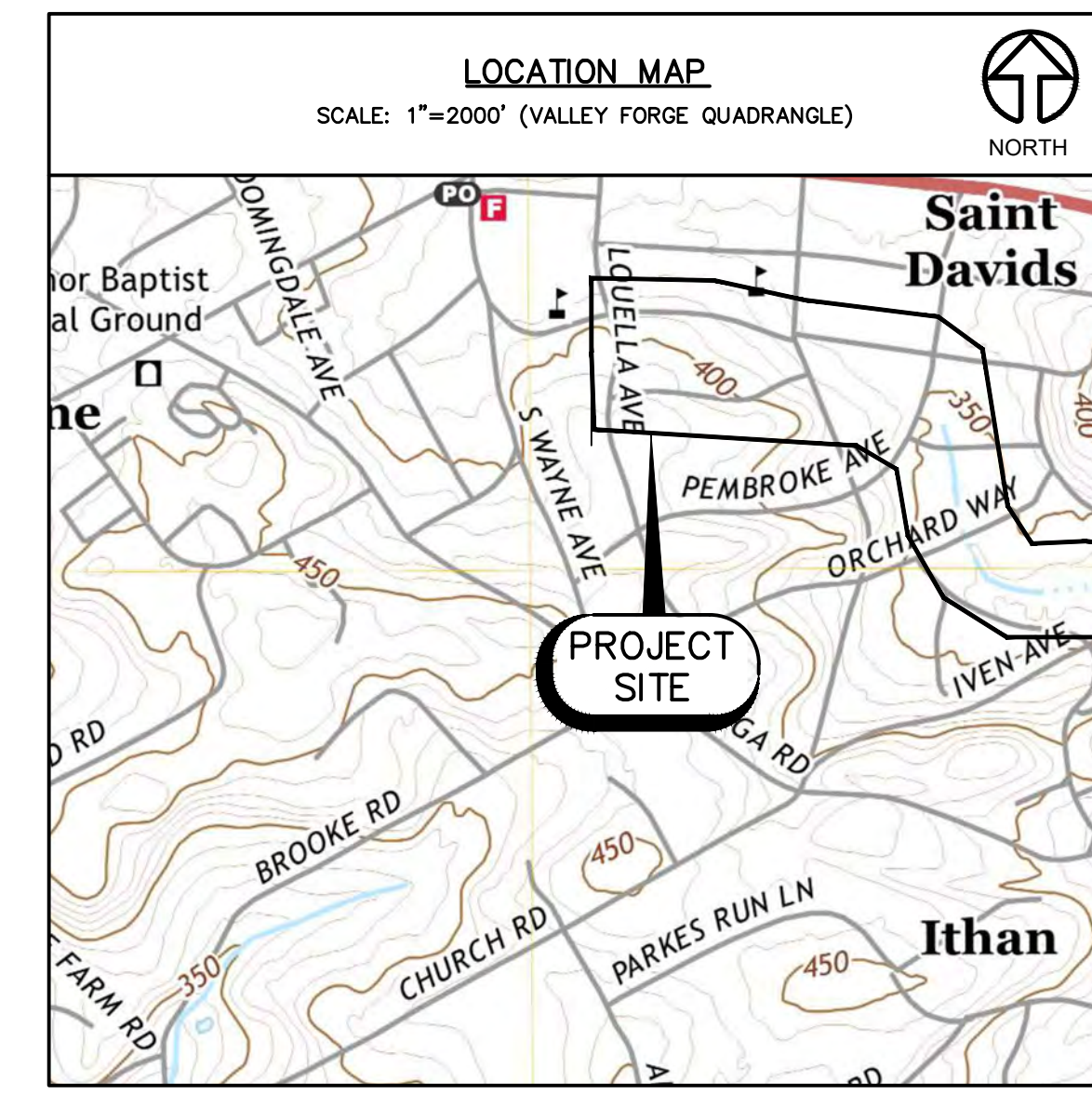
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CONCEPTUAL STORM SEWER  
 INDEX PLAN  
 SOUTH WAYNE DRAINAGE IMPROVEMENTS  
 FEASIBILITY STUDY  
 SITUATED IN  
 RADNOR TOWNSHIP  
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 RADNOR TOWNSHIP  
 301 IVEN AVENUE  
 WAYNE, PENNSYLVANIA, 19087-5297

DRAWING INDEX

SHT. NO.	DWG. NO.	DESCRIPTION
1	-	COVER
2	G-001	EXISTING FEATURES INDEX PLAN
3	V-101	EXISTING FEATURES IVEN AVENUE
4	V-102	EXISTING FEATURES BROOKSIDE AVENUE
5	V-103	EXISTING FEATURES ORCHARD WAY
6	V-104	EXISTING FEATURES PEMBROKE AVENUE & ORCHARD WAY
7	V-105	EXISTING FEATURES PEMBROKE AVENUE & MEADOWBROOK AVENUE
8	V-106	EXISTING FEATURES PLAN PEMBROKE AVENUE & SAINT DAVIDS ROAD
9	V-107	EXISTING FEATURES PLAN PEMBROKE AVENUE & MIDLAND AVENUE
10	V-108	EXISTING FEATURES PLAN SOUTH ABERDEEN & MIDLAND AVENUE
11	V-109	EXISTING FEATURES PLAN MIDLAND AVENUE (WEST)
12	G-002	CONCEPTUAL STORM SEWER INDEX PLAN
13	C-101	CONCEPTUAL STORM SEWER MIDLAND AVENUE BTW PEMBROKE & S. ABERDEEN
14	C-102	CONCEPTUAL STORM SEWER MIDLAND AVENUE BTW PEMBROKE & S. ABERDEEN
15	C-103	CONCEPTUAL STORM SEWER MIDLAND AVENUE BTW LOUELLA & S. ABERDEEN
16	C-104	CONCEPTUAL STORM SEWER MIDLAND AVENUE BTW LOUELLA & S. ABERDEEN
17	C-105	CONCEPTUAL STORM SEWER SAINT DAVIDS BTW PEMBROKE & S. ABERDEEN

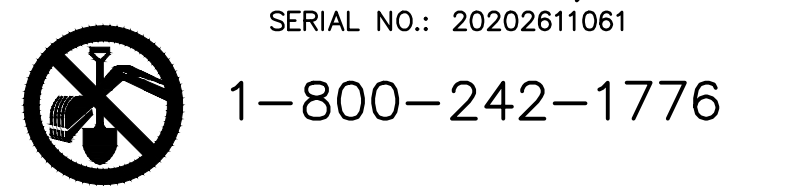


**SYMBOLS / LINE TYPES LEGEND:**

320 - - - - -	CONTOURS	LP	LIGHT POLE
- - - - -	WATER DELINEATOR	ACU	AIR CONDITIONING UNIT
- - - - -	TREELINE	FP	FLAG POLE
- - - - -	CURB LINE	MB	MAILBOX
- - - - -	CENTERLINE	CB	CABLE BOX
- - - - -	RIGHT-OF-WAY LINE	BOL	BOLLARD
- - - - -	PROPERTY LINE	TSB	TRAFFIC SIGNAL BOX
- - - - -	EASEMENT LINE	TL	TRAFFIC LIGHT
- - - - -	FENCE	SP	SIGN POST
- - - - -	STORM SEWER	SS	STREET SIGN
W	WATER MAIN	DF	DIRECTION OF FLOW
WS	WATER SERVICE LINE		
SS	SANITARY SEWER	DT	DECIDUOUS TREE
FM	FORCE MAIN	ET	EVERGREEN TREE
SLAT	SANITARY SEWER LATERAL		
G	GAS LINE		
GS	GAS SERVICE	TI	TYPE "C" INLET
E	ELECTRIC LINE	SM	STORM MANHOLE
SM	SANITARY MANHOLE	GV	GAS VALVE
C/O	CLEANOUT	GM	GAS METER
V	VENT		
SI	STORM INLET	SM	STORM MANHOLE
WV	WATER VALVE	SS	STORM SEWER
FH	FIRE HYDRANT	SI	STORM INLET
UP	UTILITY POLE		
UP	UTILITY POLE W/GUY WIRE		
EM	ELECTRIC MANHOLE		

**CALL BEFORE YOU DIG!**  
 PENNSYLVANIA LAW REQUIRES  
 3 WORKING DAYS NOTICE FOR  
 CONSTRUCTION PHASE AND 10 WORKING  
 DAYS IN DESIGN STAGE--STOP CALL

PENNSYLVANIA ONE CALL SYSTEM, INC.  
 SERIAL NO.: 20202611061



**ACT 287 UNDERGROUND USERS LIST**

DESIGN ONE CALL SERIAL NO(S): 20220170662,  
 20220170688, 20220170712, 20220170654, 20220170712,  
 20220171008, 20220271331, 20220272100, 20220201654,

USER	ADDRESS	TELEPHONE/EMAIL
AQUA PENNSYLVANIA, INC.	762 LANCASTER AVENUE BRYN MAWR, PA 19010	SBPIZZI@AQUAAMERICA.COM
COMCAST	100 SPRINGBROOKE BLVD ASTON, PA 19014	RICHARD_KAIN@CABLE.COMCAST.COM
PECO ENERGY	450 S. HENDERSON ROAD, SUITE B. KING OF PRUSSIA, PA 19406	484-681-5720
VERIZON PA, INC.	15 MONTGOMERY AVENUE, FLOOR 2 PITTSBURGH, PA 15212	412-359-2000
RADNOR TOWNSHIP	301 IVEN AVENUE WAYNE, PA 19087	SMCNELIS@RADNOR.ORG

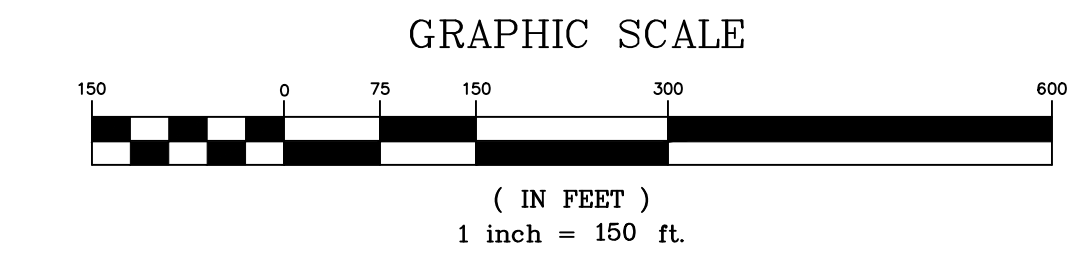
PA ONE CALL SYSTEM 1-800-242-1776

LOCATIONS OF EXISTING UTILITIES SHOWN HEREON HAVE BEEN DEVELOPED FROM EXISTING RECORDS AND/OR ABOVE-GROUND OBSERVATIONS AT THE SITE. COMPLETENESS OR ACCURACY OF LOCATION CANNOT BE GUARANTEED. ALL CONTRACTORS AND OTHER PERSONS UTILIZING THIS PLAN AND THE INFORMATION CONTAINED HEREON ARE CAUTIONED TO COMPLY WITH THE REQUIREMENTS OF PENNSYLVANIA ACT 287, AS AMENDED, TITLED "EXCAVATION AND DEMOLITION WORK PROTECTION OF UNDERGROUND UTILITIES." EACH INDIVIDUAL USING THIS PLAN MUST VERIFY THE DEPTH AND LOCATION OF ALL UNDERGROUND FACILITIES BEFORE STARTING WORK.

**CALL BEFORE YOU DIG**

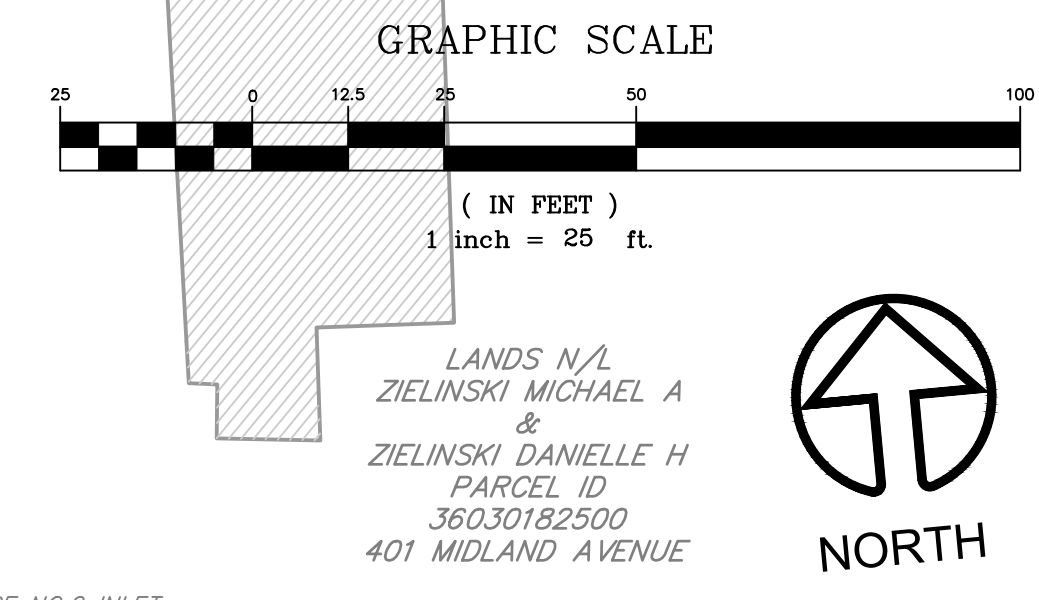
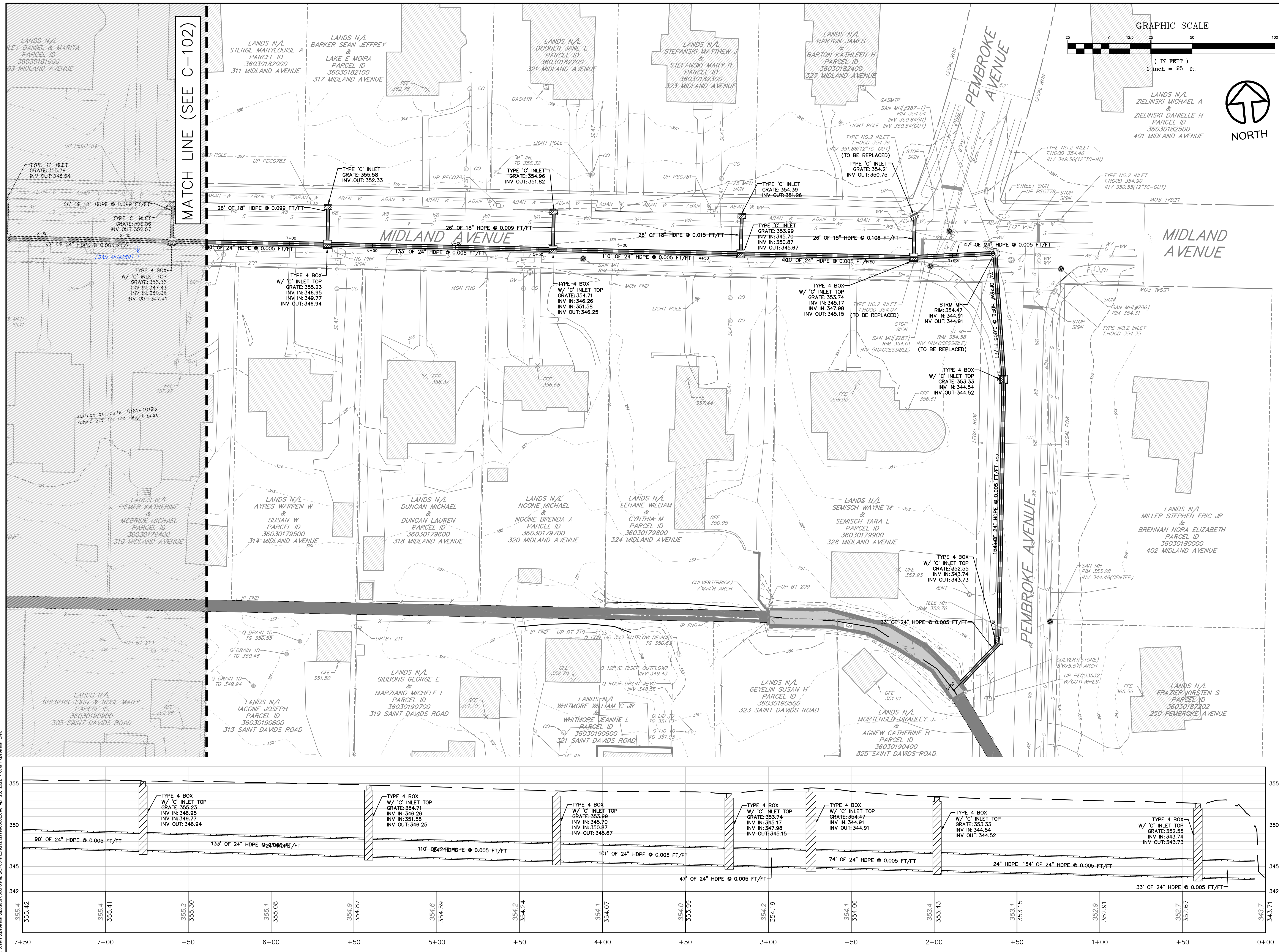
"CALL BEFORE YOU DIG" PA ONE CALL AT 1-800-242-1776 IN ACCORDANCE WITH ACT 187 CARROLL ENGINEERING CORPORATION HAS CONTACTED THE PENNSYLVANIA "ONE CALL" SYSTEM. THE SITE SERIAL NUMBERS ARE LISTED NEXT TO THE ONE CALL LOGO THE UTILITIES LISTED ON THIS SHEET HAVE UNDERGROUND FACILITIES LOCATED AT THIS SITE. IT SHALL BE THE DUTY OF EACH CONTRACTOR WHO INTENDS TO PERFORM EXCAVATION OR DEMOLITION WORK AT A SITE WITHIN THIS COMMONWEALTH:

- TO ASCERTAIN THE LOCATIONS AND TYPE OF USERS LINES BY INSPECTION OR DRAWINGS.
- TO SECURE ALL NECESSARY MUNICIPAL PERMITS RELATED TO ROAD OCCUPANCY PRIOR TO COMMENCING EXCAVATION.
- TO NOTIFY EACH USER OF CONTRACTOR'S INTENT TO PERFORM SUCH WORK AT SITE NOT LESS THAN 3 OR MORE THAN 10 WORKING DAYS PRIOR TO THE BEGINNING OF WORK FOR THE PURPOSE OF:
  - REQUEST THE UTILITY TO FIELD LOCATE ITS LINES.
  - INITIATE COOPERATION WHICH WILL AVOID DAMAGE.
  - REQUEST PROCEDURES WHICH WILL AVOID DAMAGE.
- TO INFORM EACH OPERATOR EMPLOYED BY THE CONTRACTOR AT THE SITE OF SUCH WORK OF THE INFORMATION OBTAINED.
- TO REPORT IMMEDIATELY TO THE OCCUPANTS OF THE PREMISES AS TO ANY EMERGENCY THAT THE CONTRACTOR MAY CREATE OR DISCOVER AT OR NEAR SUCH PREMISES.
- TO REPORT IMMEDIATELY TO THE USER ANY BREAK OR LEAK ON ITS LINES OR ANY DENT, GOUGE, GROOVE OR OTHER DAMAGE TO SUCH LINES OR TO THEIR COATING OR CATHODIC PROTECTION, MADE OR DISCOVERED IN THE COURSE OF THE EXCAVATION OR DEMOLITION WORK.
- TO TAKE ALL REASONABLE STEPS NECESSARY TO AVOID INJURY OR OTHERWISE INTERFERE WITH ALL LINES WHERE POSITIONS HAVE BEEN PROVIDED TO THE CONTRACTOR BY USERS.
- TO EMPLOY PRUDENT TECHNIQUES, WHICH MAY INCLUDE HAND-DUG TEST HOLES, TO ASCERTAIN THE PRECISE POSITION OF SUCH FACILITIES.



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JOB NO	21-1990
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DWN BY	TSB
CKD BY	CAP
SCALE	1"=150'
DRAWER NUMBER	-
SHEET	12 OF 17 SHEETS
DRAWING NUMBER	G-002





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CONCEPTUAL STORM SEWER PLAN  
 MIDLAND AVENUE BTW PEMBROKE & S. ABERDEEN  
 SOUTH WAYNE DRAINAGE IMPROVEMENTS  
 FEASIBILITY STUDY  
 SITUATED IN  
 RADNOR TOWNSHIP  
 PREPARED FOR  
 RADNOR TOWNSHIP  
 301 IVEN AVENUE  
 WAYNE, PENNSYLVANIA, 19087-5297

NO.	DATE	DESCRIPTION	INITIALS

DATE	4-1-2022
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JOB NO	21-1990
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SHEET	13 OF 17 SHEETS
DRAWING NUMBER	C-101

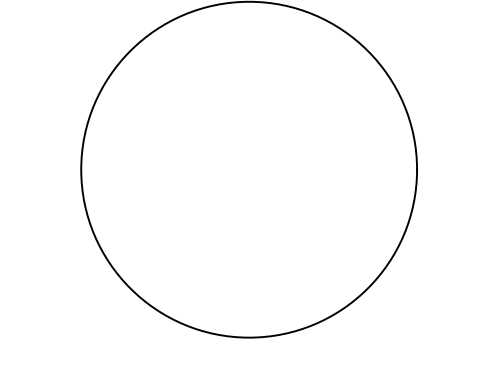
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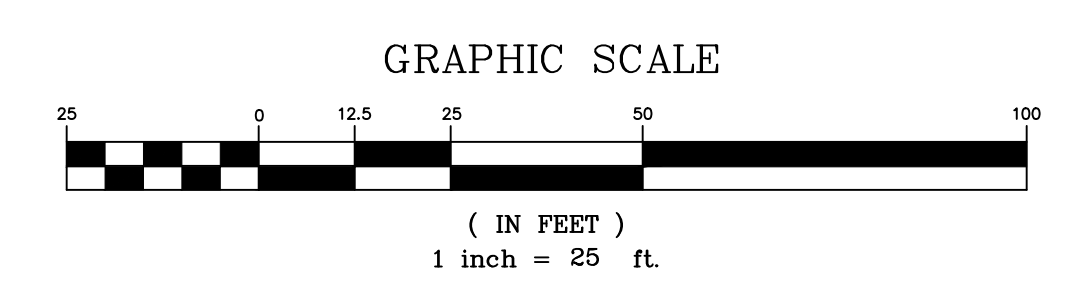
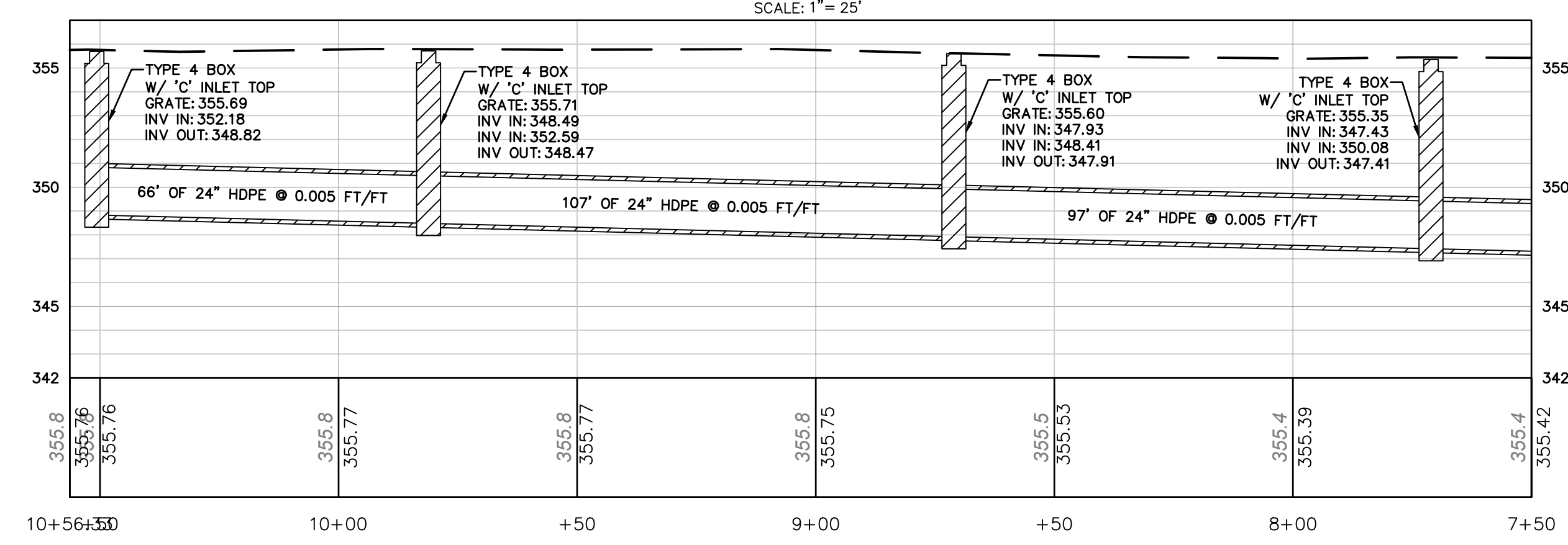
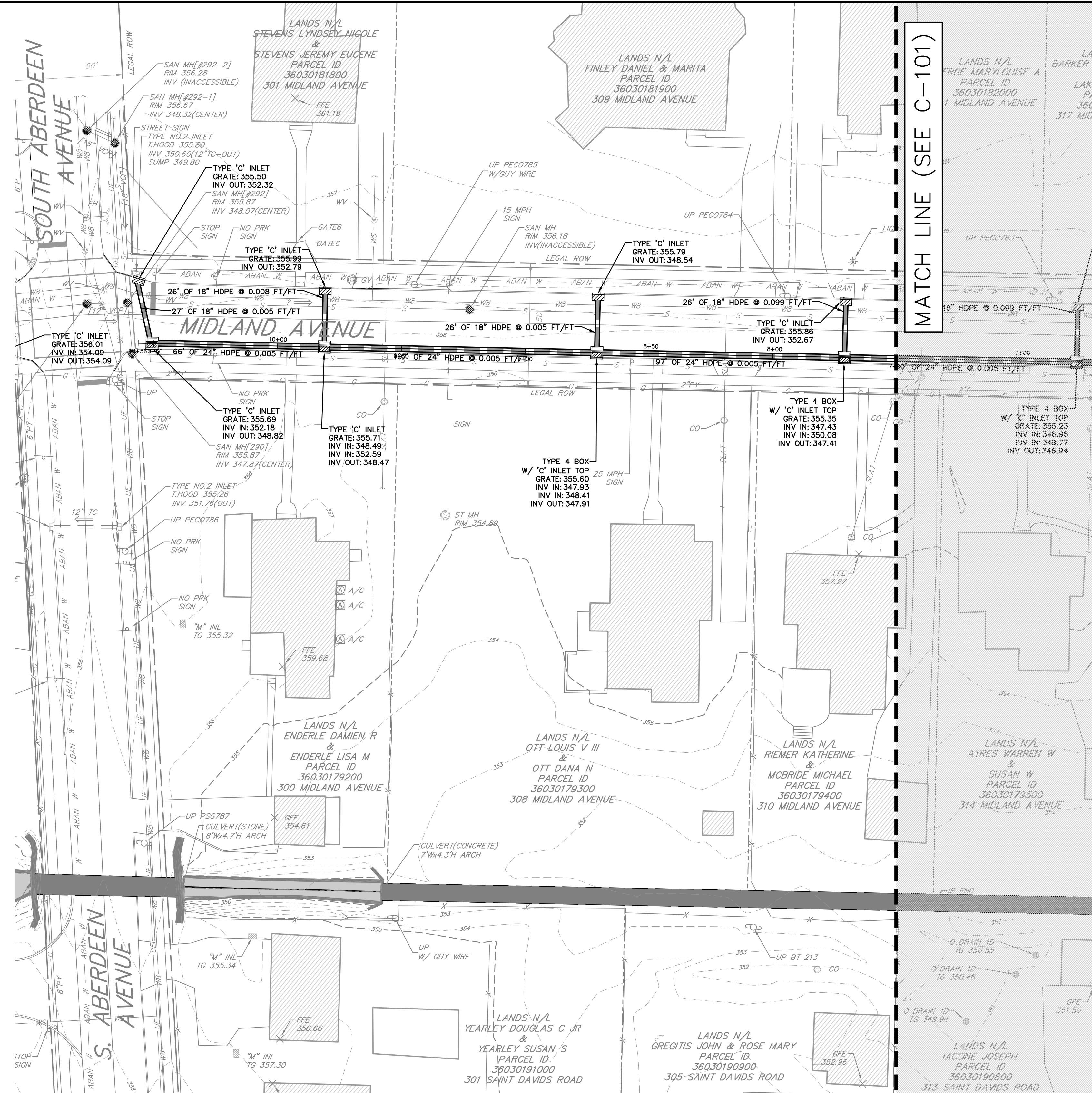
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CONCEPTUAL STORM SEWER PLAN  
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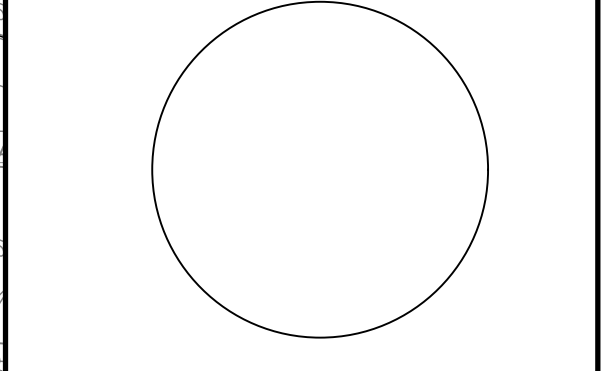
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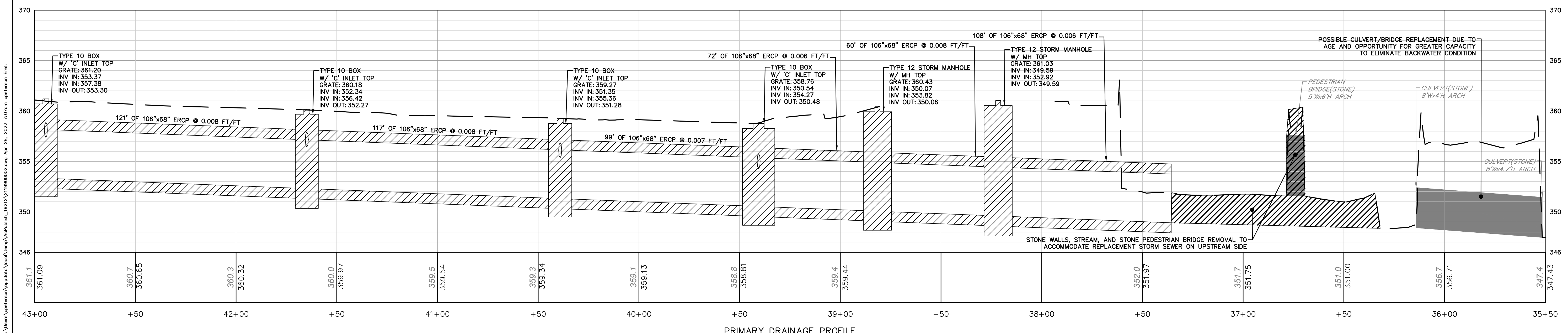
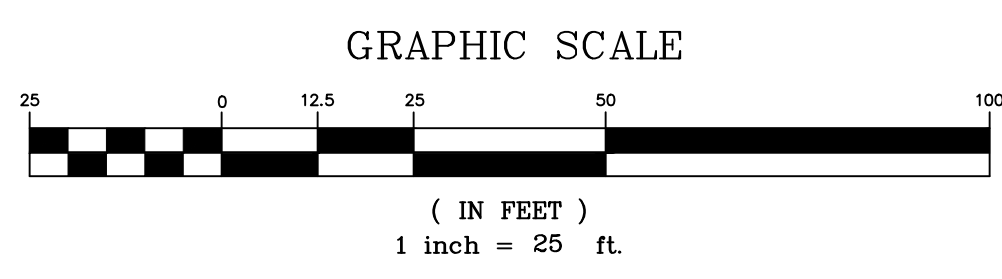
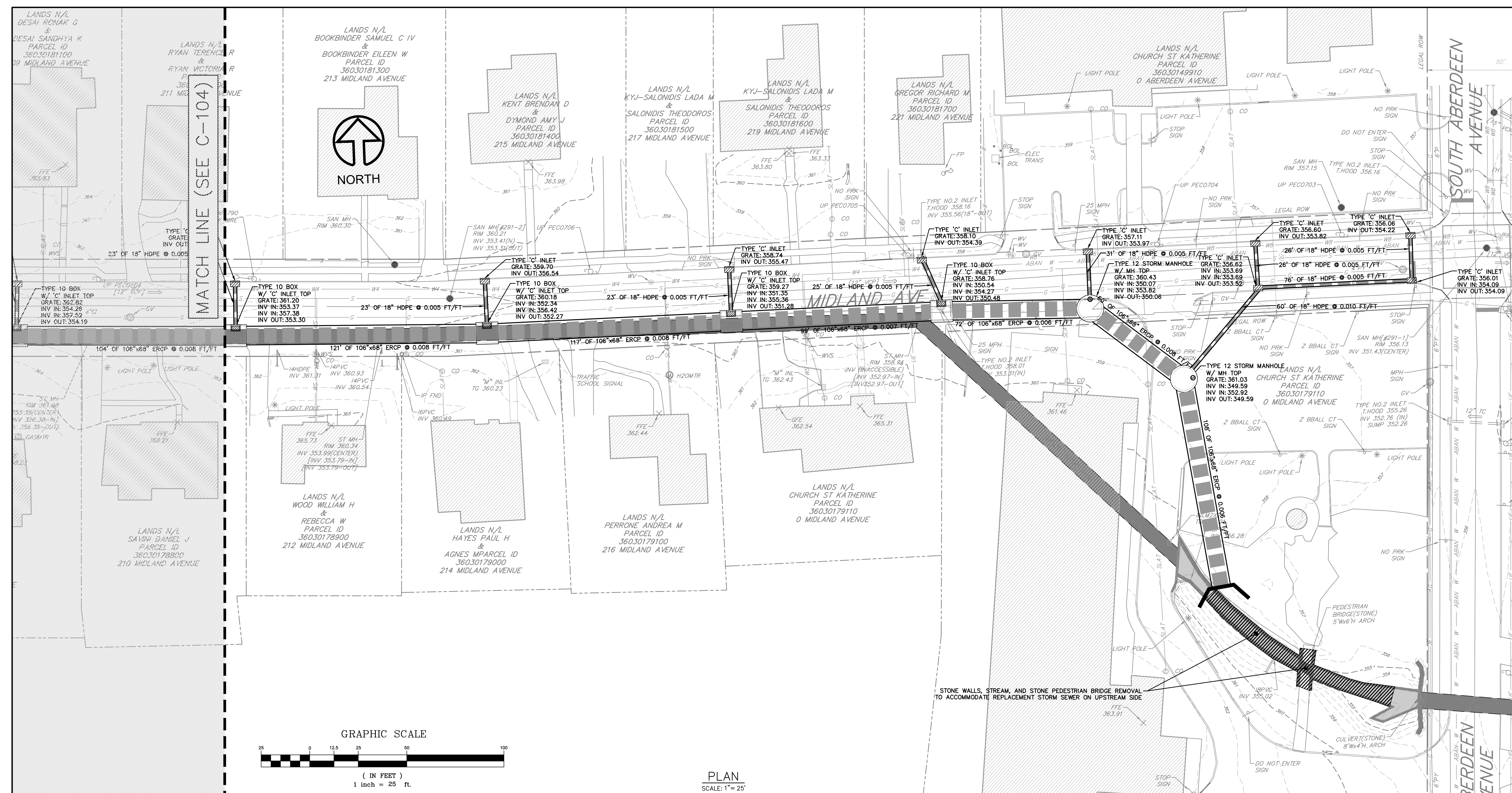
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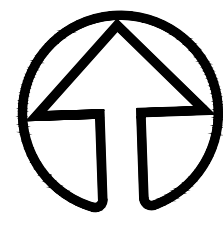
**CONCEPTUAL STORM SEWER PLAN**  
**MIDLAND AVENUE BTW LOUELLA & S. ABERDEEN**  
**SOUTH WAYNE DRAINAGE IMPROVEMENTS**  
**FEASIBILITY STUDY**  
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**WAYNE, PENNSYLVANIA, 19087-5297**



NO.	DATE	DESCRIPTION

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SHEET	15 OF 17 SHEETS



NORTH



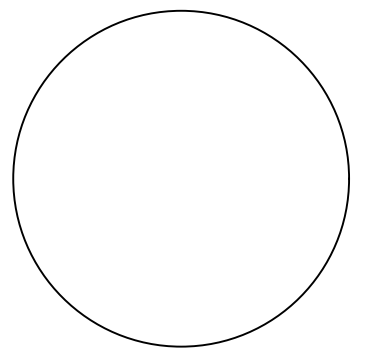
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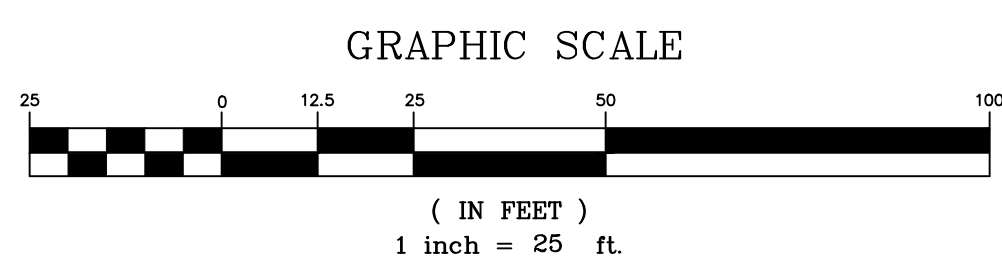
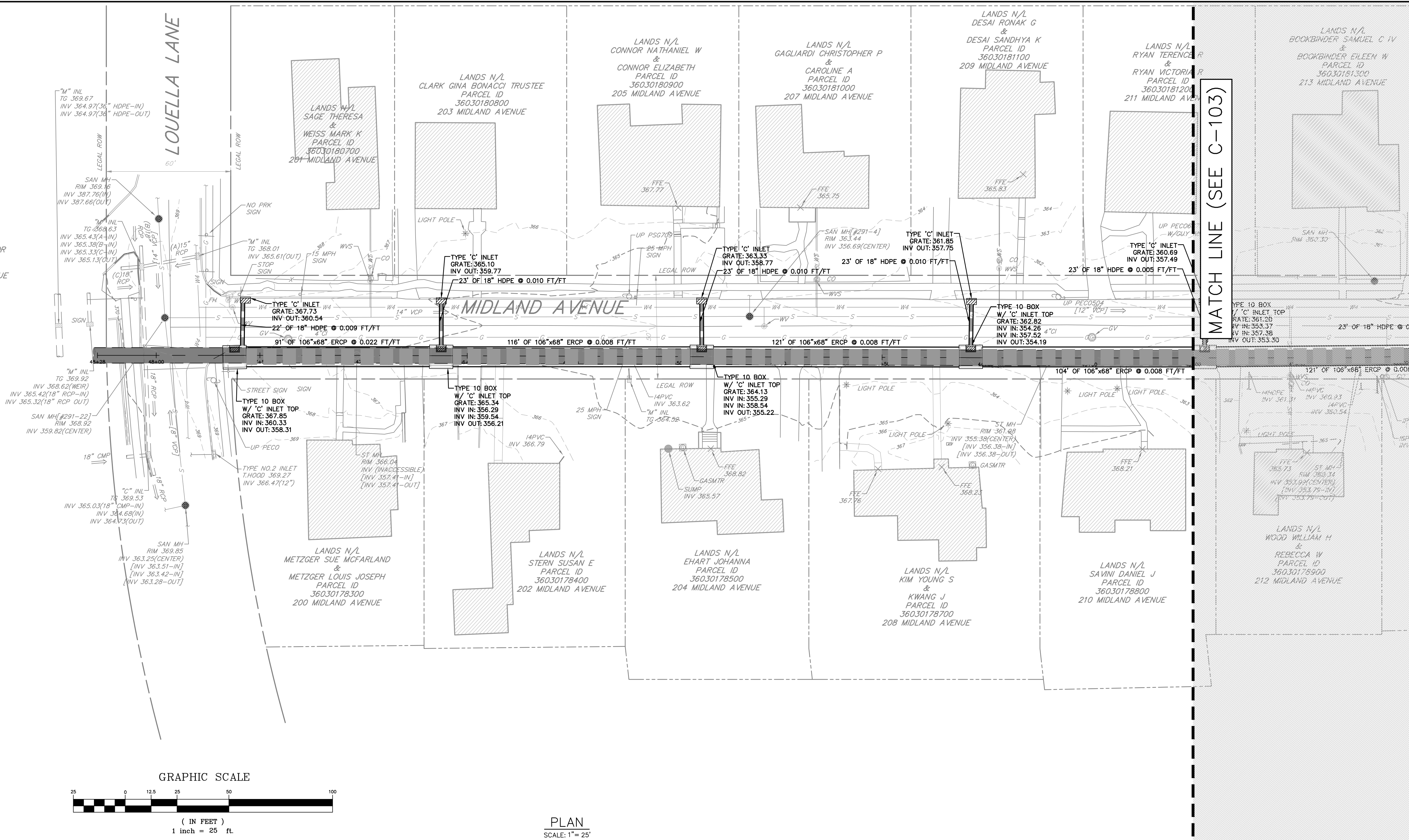
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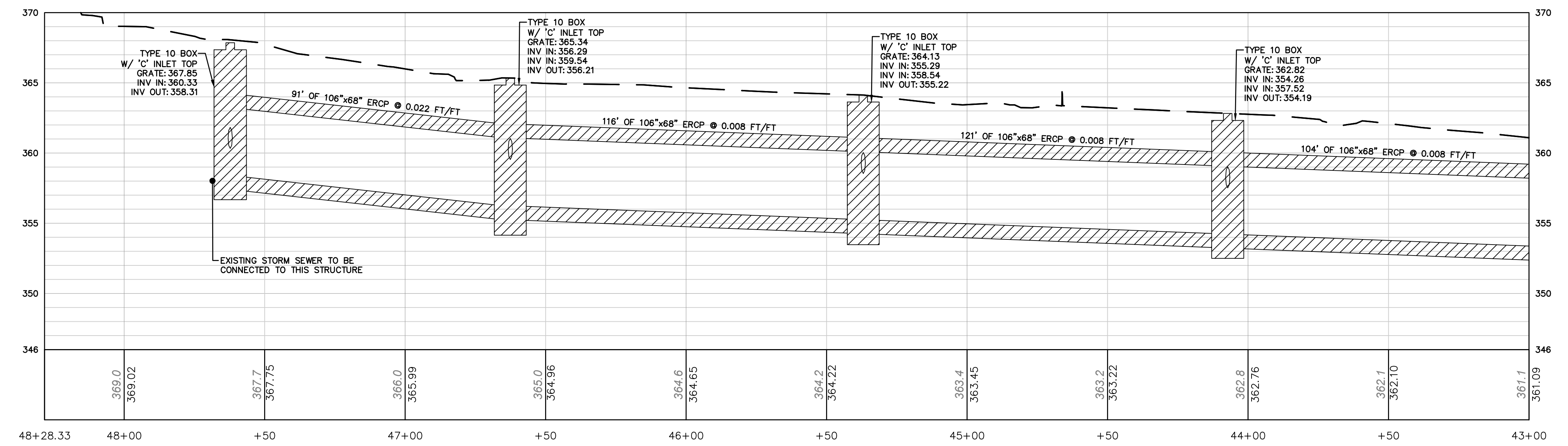
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DWN BY	TSB
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SHEET	16 OF 17 SHEETS
DRAWING NUMBER	C-104



PLAN  
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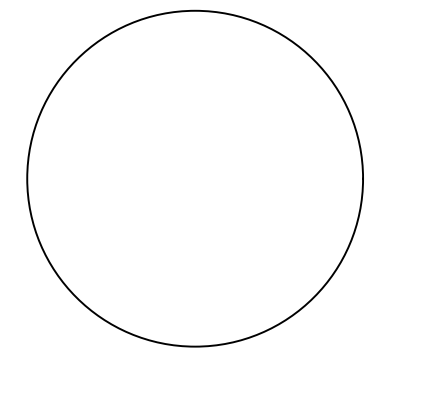
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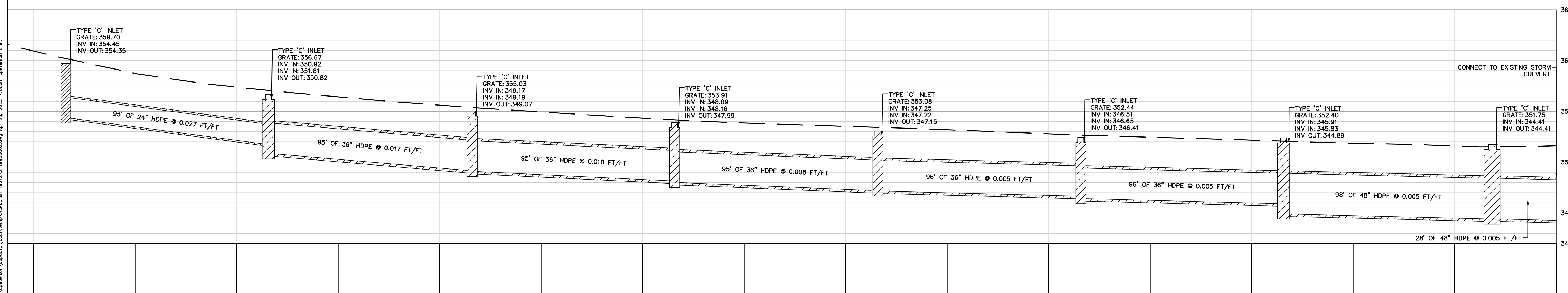
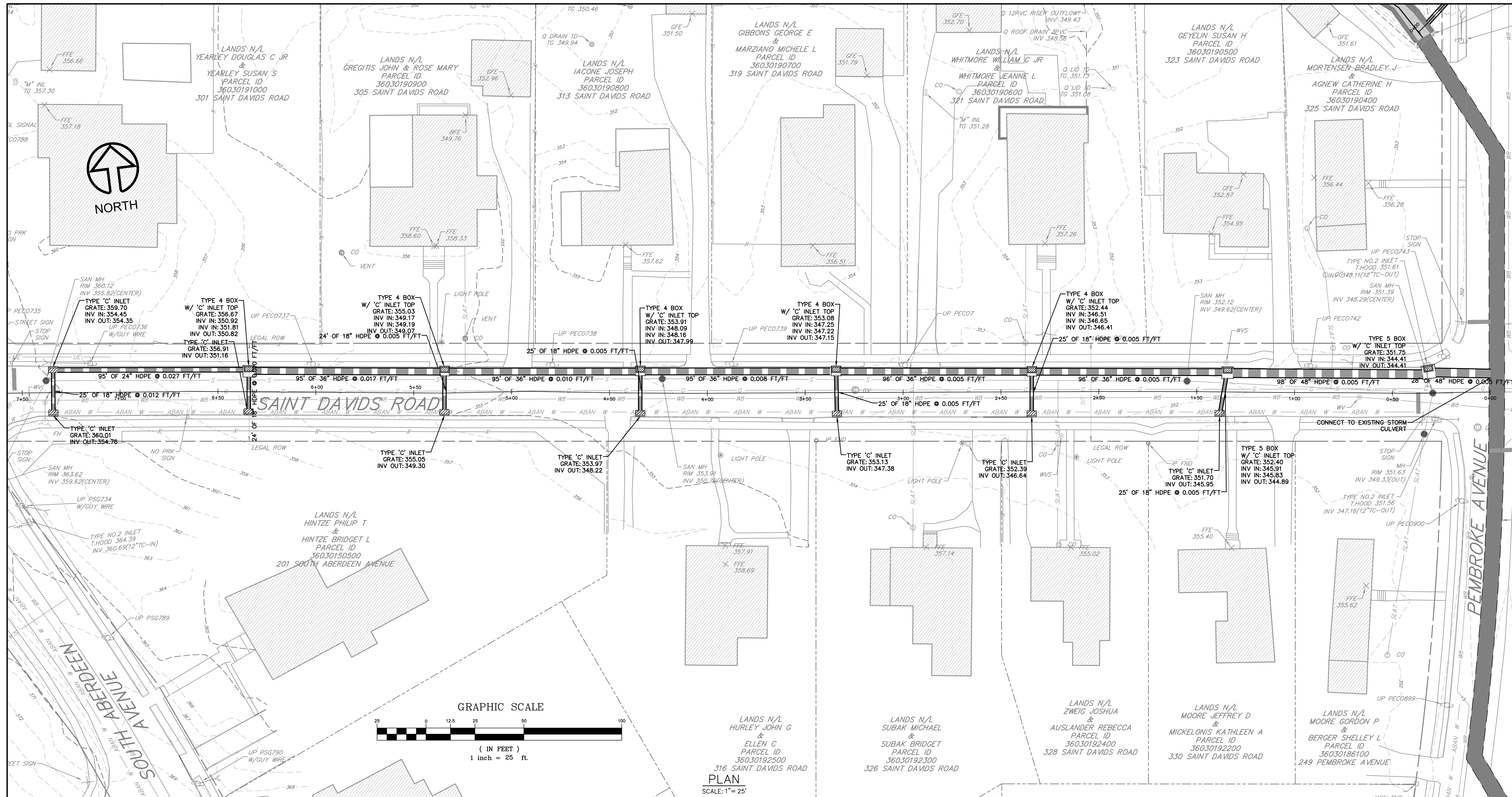
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**CONCEPTUAL STORM SEWER PLAN**  
**SAINT DAVIDS BTW PEMBROKE & S. ABERDEEN**  
**SOUTH WAYNE DRAINAGE IMPROVEMENTS**  
**FEASIBILITY STUDY**  
 SITUATED IN  
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**WAYNE, PENNSYLVANIA, 19087-5297**



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JOB NO	21-1990
DSG BY	CAP
DWN BY	TSB
CKD BY	CAP
SCALE	1"=25'
DRAWER NUMBER	-
SHEET	17 OF 17 SHEETS

**APPENDIX B: ITHAN CREEK SECTIONS – INDEX PLAN**



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ITHAN CREEK SECTIONS  
 INDEX PLAN  
 SOUTH WAYNE DRAINAGE IMPROVEMENTS  
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 RADNOR TOWNSHIP  
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 WAYNE, PENNSYLVANIA, 19087-5297

SECTION NOTES:

- \* STONE ARCH CULVERT AT MEADOWBROOK AVENUE HAS NEGATIVE SLOPE AS SUCH, SLOPE OF THE UPSTREAM REACH IS USED FOR THEORETICAL CAPACITY.
- \*\* STONE ARCH CULVERT AT ORCHARD AND IVEN AVENUE HAVE NEGATIVE SLOPE AS SUCH, THE AVERAGE OF THE UP AND DOWNSTREAM STREAM SLOPE IS USED FOR THEORETICAL CAPACITY.

GENERAL NOTES:

1. DRAINAGE AREA AND PEAK FLOW RATES OBTAINED FROM STREAMSTATS.USGS.GOV REPORTS.
2. PEAK FLOW RATES FOR SECTIONS BASED ON DRAINAGE CONDITIONS AT START OF REACH.
3. THEORETICAL CAPACITY CALCULATED USING MANNING'S EQUATION AND FULL FLOWING SECTIONS.
4. MANNING'S N VALUES OBTAINED FROM TABLES IN THE PUBLICATION (CHOW, 1959).
5. MEAN SLOPE OF REACH USED IN CALCULATION WHEN MEASURED SLOPE IS UNSUITABLE DUE TO CURRENT CONDITIONS.
6. \*REQUIRED SECTIONS\* OR PROPOSED SECTIONS WERE APPROXIMATELY SIZED TO CONVEY THE 100-YEAR FLOW RATE WITH THE EXCEPTION OF SECTION 1 WHERE SPACE LIMITS THE SIZE OF THE CONDUIT WHICH CAN BE USED WITHOUT MAJOR UTILITY RELOCATIONS.

SECTION RANKING

RANK	SECTION	CAPACITY	100-YR FLOW	DIFFERENCE
1	9	165 CFS	858 CFS	(693 CFS)
2	14	352 CFS	1,040 CFS	(688 CFS)
3	15	393 CFS	1,040 CFS	(647 CFS)
4	7	234 CFS	813 CFS	(579 CFS)
5	5	164 CFS	668 CFS	(504 CFS)
6	3	165 CFS	657 CFS	(492 CFS)
7	11	429 CFS	875 CFS	(446 CFS)
8	8	441 CFS	813 CFS	(372 CFS)
9	10	554 CFS	867 CFS	(313 CFS)
10	12	579 CFS	884 CFS	(305 CFS)
11	4	426 CFS	657 CFS	(231 CFS)
12	1	339 CFS	548 CFS	(209 CFS)
13	2	542 CFS	626 CFS	(84 CFS)
14	6	659 CFS	678 CFS	(19 CFS)
15	13	1,216 CFS	1,040 CFS	+176 CFS

**SECTION 13**  
 NORTHERN REACH BETWEEN ORCHARD WAY AND IVEN AVENUE  
 REACH LENGTH: 1,323 FT  
 MEAN SLOPE OF REACH: 0.62%  
 MANNING'S N: 0.024  
 THEORETICAL CAPACITY: 1,216 CFS  
 DRAINAGE AREA: 524 ACRES  
 PEAK FLOW RATES:  
 2-YR: 201 CFS 25-YR 691 CFS  
 5-YR: 359 CFS 50-YR 858 CFS  
 10-YR 493 CFS 100-YR 1040 CFS

**SECTION 14**  
 STONE ARCH CULVERT UNDER IVEN AVENUE  
 MEASURED SLOPE OF REACH: -0.8%  
 REACH LENGTH: 25 FT  
 MEAN SLOPE OF REACH: 1.11%\*  
 MANNING'S N: 0.017  
 THEORETICAL CAPACITY: 352 CFS  
 DRAINAGE AREA: 531 ACRES  
 PEAK FLOW RATES:  
 2-YR: 201 CFS 25-YR 691 CFS  
 5-YR: 359 CFS 50-YR 858 CFS  
 10-YR 493 CFS 100-YR 1040 CFS

**SECTION 15**  
 CORRUGATED METAL PIPE UNDER TWP ENTRANCE  
 REACH LENGTH: 33 FT  
 MEAN SLOPE OF REACH: 1.0%  
 MANNING'S N: 0.019  
 THEORETICAL CAPACITY: 393 CFS  
 DRAINAGE AREA: 531 ACRES  
 PEAK FLOW RATES:  
 2-YR: 201 CFS 25-YR 691 CFS  
 5-YR: 359 CFS 50-YR 858 CFS  
 10-YR 493 CFS 100-YR 1040 CFS

**SECTION 1**  
 BRICK BOX CULVERT BELOW MIDLAND AVENUE  
 REACH LENGTH: 990 FT  
 MEAN SLOPE OF REACH: 0.54%±  
 MANNING'S N: 0.017  
 THEORETICAL CAPACITY: 339 CFS  
 DRAINAGE AREA: 192 ACRES  
 PEAK FLOW RATES:  
 2-YR: 98.6 CFS 25-YR 358 CFS  
 5-YR: 181 CFS 50-YR 449 CFS  
 10-YR 252 CFS 100-YR 548 CFS

**SECTION 2**  
 STONE/CONCRETE WALLS ALONG CHANNEL  
 REACH LENGTH: 82 FT  
 SLOPE OF REACH: 0.90%±  
 MANNING'S N: 0.017  
 THEORETICAL CAPACITY: 542 CFS  
 DRAINAGE AREA: 237 ACRES  
 PEAK FLOW RATES:  
 2-YR: 114 CFS 25-YR 410 CFS  
 5-YR: 208 CFS 50-YR 513 CFS  
 10-YR 289 CFS 100-YR 626 CFS

**SECTION 3**  
 PEDESTRIAN BRIDGE AT SAINT KATHERINES  
 REACH LENGTH: 9 FT  
 SLOPE OF REACH: 0.35%±  
 MANNING'S N: 0.017  
 THEORETICAL CAPACITY: 165 CFS  
 DRAINAGE AREA: 256 ACRES  
 PEAK FLOW RATES:  
 2-YR: 121 CFS 25-YR 431 CFS  
 5-YR: 220 CFS 50-YR 539 CFS  
 10-YR 305 CFS 100-YR 657 CFS

**SECTION 4**  
 CULVERT BELOW SOUTH ABERDEEN AVENUE  
 REACH LENGTH: 63 FT  
 SLOPE OF REACH: 1.52%±  
 MANNING'S N: 0.017  
 THEORETICAL CAPACITY: 426 CFS  
 DRAINAGE AREA: 256 ACRES  
 PEAK FLOW RATES:  
 2-YR: 121 CFS 25-YR 431 CFS  
 5-YR: 220 CFS 50-YR 539 CFS  
 10-YR 305 CFS 100-YR 657 CFS

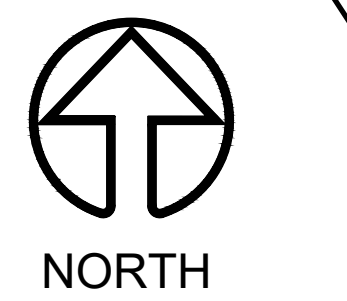
**SECTION 5**  
 REACH BETWEEN SOUTH ABERDEEN AVENUE AND PEMBROKE AVENUE  
 REACH LENGTH: 548 FT  
 SLOPE OF REACH: 0.295%±  
 MANNING'S N: 0.017  
 THEORETICAL CAPACITY: 164 CFS  
 DRAINAGE AREA: 262 ACRES  
 PEAK FLOW RATES:  
 2-YR: 123 CFS 25-YR 438 CFS  
 5-YR: 223 CFS 50-YR 547 CFS  
 10-YR 310 CFS 100-YR 668 CFS

**SECTION 6**  
 WESTERN REACH BETWEEN SOUTH ABERDEEN AVENUE AND PEMBROKE AVENUE  
 REACH LENGTH: 130 FT  
 SLOPE OF REACH: 1.100%  
 MANNING'S N: 0.017  
 THEORETICAL CAPACITY: 659 CFS  
 DRAINAGE AREA: 269 ACRES  
 PEAK FLOW RATES:  
 2-YR: 125 CFS 25-YR 445 CFS  
 5-YR: 227 CFS 50-YR 556 CFS  
 10-YR 315 CFS 100-YR 678 CFS

**SECTION 7**  
 CULVERT UNDERNEATH PEMBROKE AVENUE  
 REACH LENGTH: 422 FT  
 MEAN SLOPE OF REACH: 0.26%  
 MANNING'S N: 0.017  
 THEORETICAL CAPACITY: 234 CFS  
 DRAINAGE AREA: 359 ACRES  
 PEAK FLOW RATES:  
 2-YR: 153 CFS 25-YR 536 CFS  
 5-YR: 275 CFS 50-YR 668 CFS  
 10-YR 380 CFS 100-YR 813 CFS

**SECTION 8**  
 REACH BETWEEN PEMBROKE CONDUIT AND MEADOWBROOK  
 REACH LENGTH: 321 FT  
 MEAN SLOPE OF REACH: 0.27%  
 MANNING'S N: 0.017  
 THEORETICAL CAPACITY: 441 CFS  
 DRAINAGE AREA: 359 ACRES  
 PEAK FLOW RATES:  
 2-YR: 153 CFS 25-YR 536 CFS  
 5-YR: 275 CFS 50-YR 668 CFS  
 10-YR 380 CFS 100-YR 813 CFS

**SECTION 9**  
 STONE ARCH CULVERT BELOW MEADOWBROOK AVENUE  
 REACH LENGTH: 33 FT  
 MEAN SLOPE OF REACH: 0.27%\*  
 MANNING'S N: 0.017  
 THEORETICAL CAPACITY: 165 CFS  
 DRAINAGE AREA: 390 ACRES  
 PEAK FLOW RATES:  
 2-YR: 162 CFS 25-YR 566 CFS  
 5-YR: 292 CFS 50-YR 705 CFS  
 10-YR 402 CFS 100-YR 858 CFS



**PROPOSED SECTION 1**  
 MEAN SLOPE OF REACH: 0.8%±  
 MANNING'S N: 0.017  
 THEORETICAL CAPACITY: 437 CFS

**PROPOSED SECTION 2 AND SECTION 3**  
 MEAN SLOPE OF REACH: 0.90%±  
 MANNING'S N: 0.024  
 THEORETICAL CAPACITY: 651 CFS

**PROPOSED SECTION 4**  
 MEAN SLOPE OF REACH: 1.52%±  
 MANNING'S N: 0.017  
 THEORETICAL CAPACITY: 677 CFS

**PROPOSED SECTION 5**  
 MEAN SLOPE OF REACH: 0.30%±  
 MANNING'S N: 0.024  
 THEORETICAL CAPACITY: 672 CFS

**PROPOSED SECTION 7**  
 MEAN SLOPE OF REACH: 0.26%±  
 MANNING'S N: 0.017  
 THEORETICAL CAPACITY: 828 CFS

**PROPOSED SECTION 8**  
 MEAN SLOPE OF REACH: 0.27%±  
 MANNING'S N: 0.024  
 THEORETICAL CAPACITY: 816 CFS  
 NOTE: THIS SECTION WOULD CONFLICT WITH ADJACENT RESIDENTIAL DRIVEWAY ALONG PEMBROKE AVENUE

**PROPOSED SECTION 9**  
 MEAN SLOPE OF REACH: 0.27%±  
 MANNING'S N: 0.017  
 THEORETICAL CAPACITY: 885 CFS

NO CHANGES PROPOSED

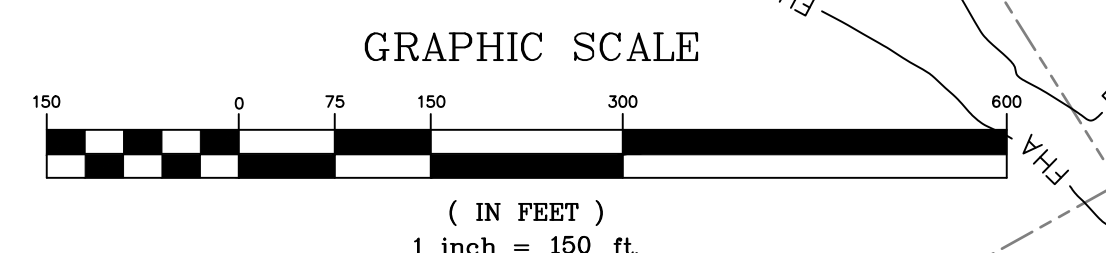
REQUIRED SECTIONS

**PROPOSED SECTION 10 AND 11**  
 MEAN SLOPE OF REACH: 0.27%±  
 MANNING'S N: 0.024  
 THEORETICAL CAPACITY: 885 CFS

**PROPOSED SECTION 12**  
 MEAN SLOPE OF REACH: 0.92%±  
 MANNING'S N: 0.017  
 THEORETICAL CAPACITY: 929 CFS

NO CHANGES PROPOSED

**PROPOSED SECTION 14**  
 SLOPE OF REACH: 1.0%  
 MANNING'S N: 0.017  
 THEORETICAL CAPACITY: 1,078 CFS



\\cnc-01\new\formal\dwg\211990007.dwg, Jun 01, 2022, 12:26pm, operation, Erat

DATE	4-20-2022
CADD FILE	2119900007
JOB NO	21-1990
DSG BY	CAP
DWN BY	MEW
CKD BY	CAP
SCALE	1"=150'
DRAWER NUMBER	-
SHEET	1 OF 1 SHEETS
DRAWING NUMBER	G-001

## **APPENDIX C: MANNINGS CALCULATIONS**



## **EXISTING SECTIONS**

# Channel Report

## Section 1 - Brick Arch Culvert

### User-defined

Invert Elev (ft) = 100.00  
Slope (%) = 0.54  
N-Value = Composite

### Highlighted

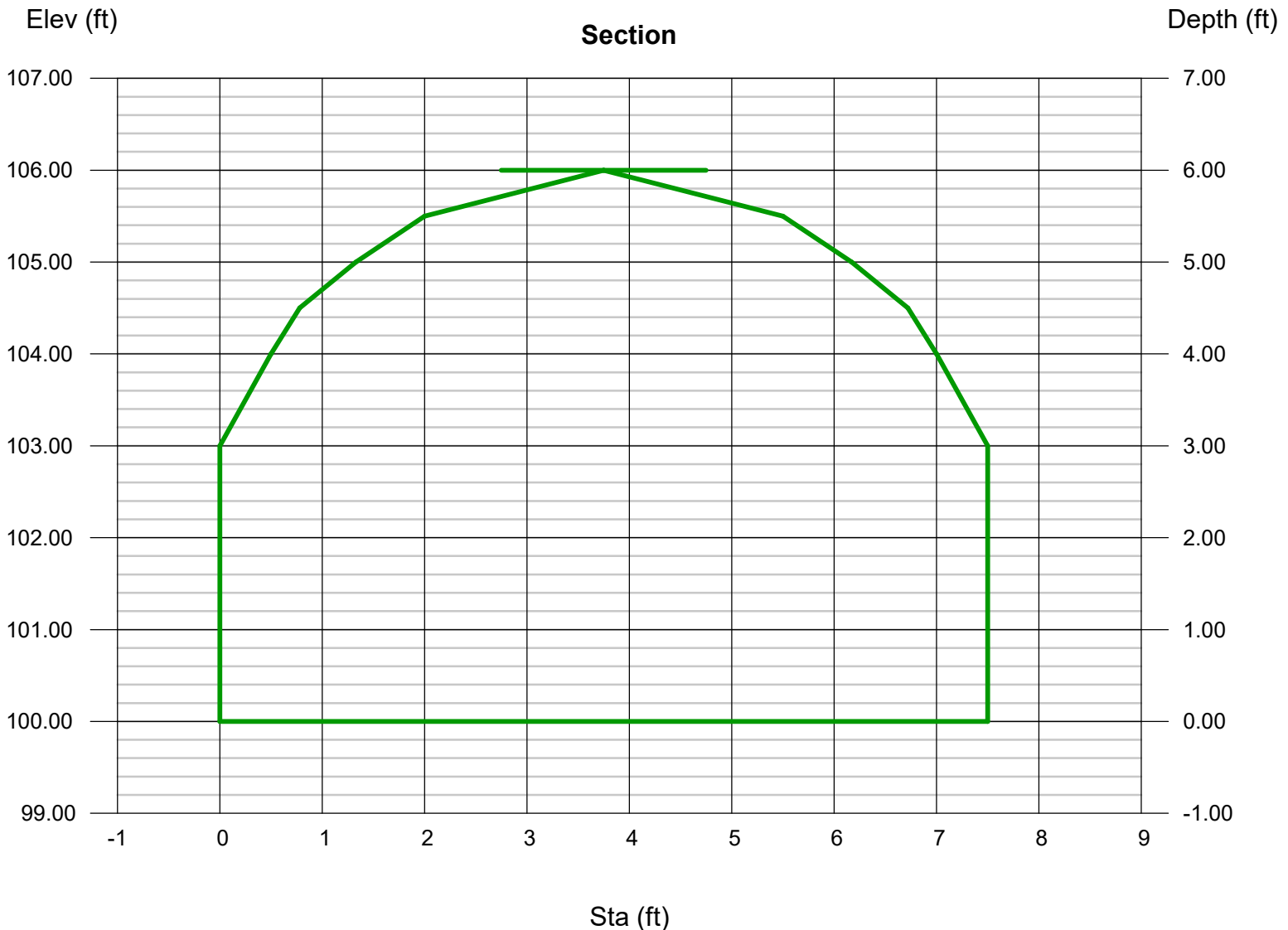
Depth (ft) = 6.00  
Q (cfs) = 339.20  
Area (sqft) = 38.27  
Velocity (ft/s) = 8.86  
Wetted Perim (ft) = 23.68  
Crit Depth, Yc (ft) = 3.89  
Top Width (ft) = 0.00  
EGL (ft) = 7.22

### Calculations

Compute by: Q vs Depth  
No. Increments = 1

### (Sta, El, n)-(Sta, El, n)...

(3.75, 106.00)-(2.00, 105.50, 0.017)-(1.33, 105.00, 0.017)-(0.78, 104.50, 0.017)-(0.50, 104.00, 0.017)-(7.50, 100.00, 0.017)-(7.50, 103.00, 0.017)  
-(7.00, 104.00, 0.017)-(6.72, 104.50, 0.017)-(6.17, 105.00, 0.017)-(5.50, 105.50, 0.017)-(3.75, 106.00, 0.017)



# Channel Report

## Section 2 - Stone Wall Channel (Saint Katherines)

### User-defined

Invert Elev (ft) = 100.00  
Slope (%) = 0.90  
N-Value = Composite

### Highlighted

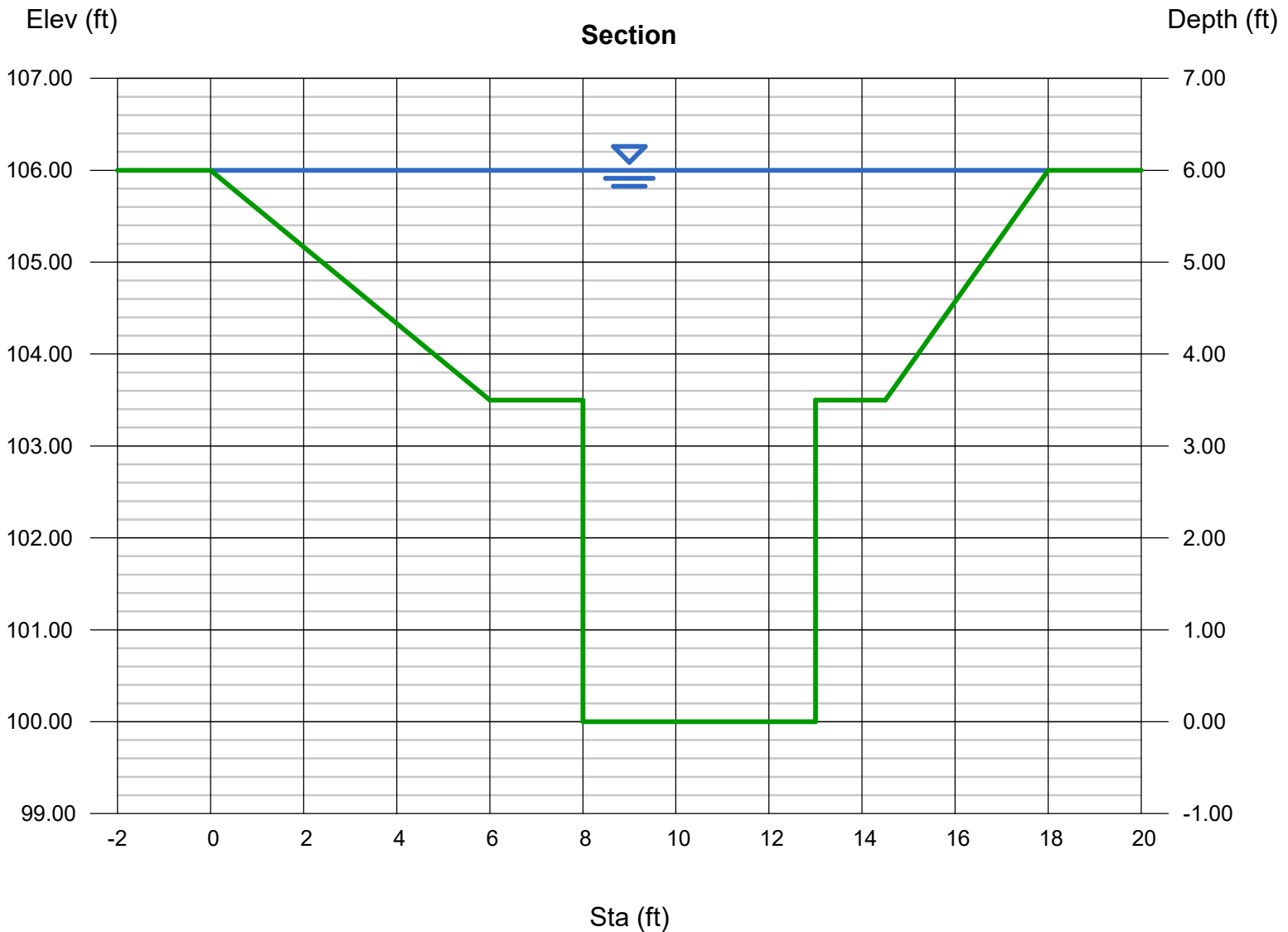
Depth (ft) = 6.00  
Q (cfs) = 541.88  
Area (sqft) = 50.63  
Velocity (ft/s) = 10.70  
Wetted Perim (ft) = 26.30  
Crit Depth, Yc (ft) = 6.00  
Top Width (ft) = 18.00  
EGL (ft) = 7.78

### Calculations

Compute by: Q vs Depth  
No. Increments = 12

### (Sta, El, n)-(Sta, El, n)...

(0.00, 106.00)-(6.00, 103.50, 0.024)-(8.00, 103.50, 0.017)-(8.00, 100.00, 0.017)-(13.00, 100.00, 0.017)-(13.00, 103.50, 0.017)-(14.50, 103.50, 0.024)  
-(18.00, 106.00, 0.024)



# Channel Report

## Section 3 - Pedestrian Bridge

### User-defined

Invert Elev (ft) = 100.00  
Slope (%) = 0.35  
N-Value = Composite

### Highlighted

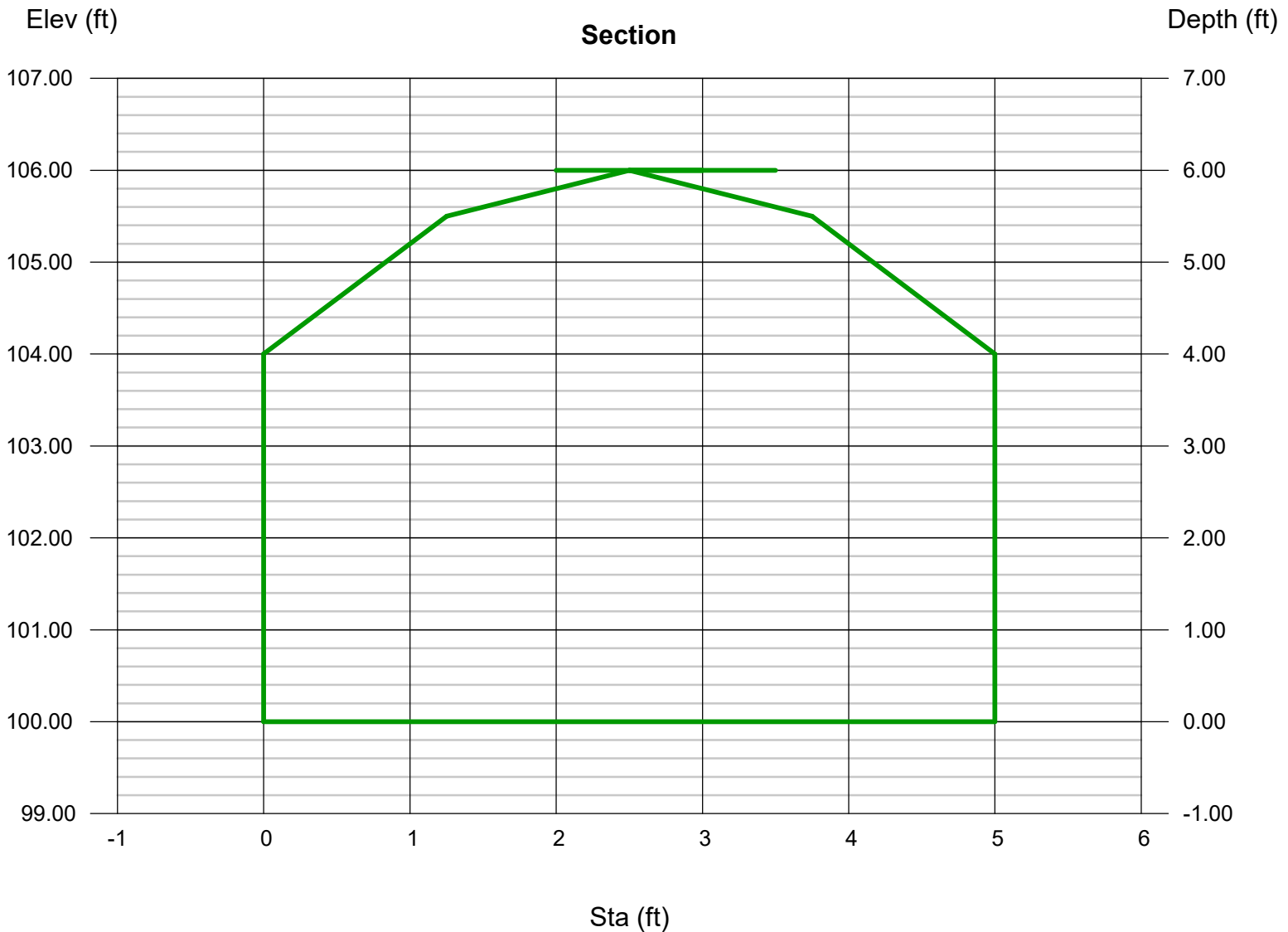
Depth (ft) = 6.00  
Q (cfs) = 165.30  
Area (sqft) = 26.25  
Velocity (ft/s) = 6.30  
Wetted Perim (ft) = 19.60  
Crit Depth, Yc (ft) = 3.24  
Top Width (ft) = 0.00  
EGL (ft) = 6.62

### Calculations

Compute by: Q vs Depth  
No. Increments = 1

### (Sta, El, n)-(Sta, El, n)...

(3.00, 106.00, 0.017)-(2.50, 106.00, 0.017)-(1.25, 105.50, 0.017)-(5.00, 100.00, 0.017)-(5.00, 104.00, 0.017)-(3.75, 105.50, 0.017)-(2.50, 106.00, 0.017)



# Channel Report

## Section 4 - Aberdeen Bridge

### User-defined

Invert Elev (ft) = 100.00  
Slope (%) = 1.52  
N-Value = Composite

### Highlighted

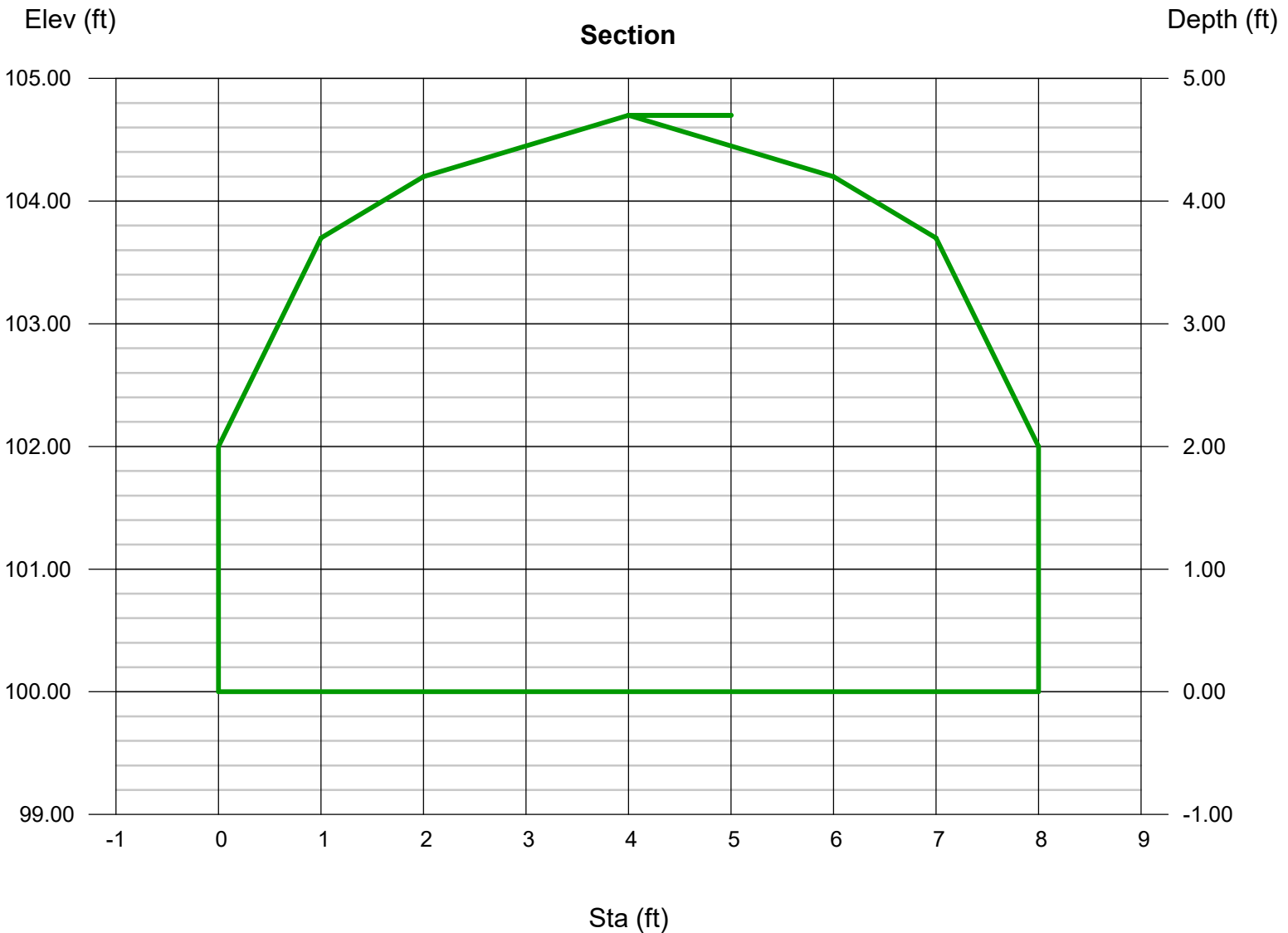
Depth (ft) = 4.70  
Q (cfs) = 425.98  
Area (sqft) = 31.40  
Velocity (ft/s) = 13.57  
Wetted Perim (ft) = 22.30  
Crit Depth, Yc (ft) = 4.04  
Top Width (ft) = 0.00  
EGL (ft) = 7.56

### Calculations

Compute by: Q vs Depth  
No. Increments = 1

### (Sta, El, n)-(Sta, El, n)...

(5.00, 104.70)-(4.00, 104.70, 0.017)-(2.00, 104.20, 0.017)-(1.00, 103.70, 0.017)-(8.00, 100.00, 0.017)-(8.00, 102.00, 0.017)-(7.00, 103.70, 0.017)  
-(6.00, 104.20, 0.017)-(4.00, 104.70, 0.017)



# Channel Report

## Section 5 - South Aberdeen Conduit

### User-defined

Invert Elev (ft) = 100.00  
Slope (%) = 0.30  
N-Value = Composite

### Highlighted

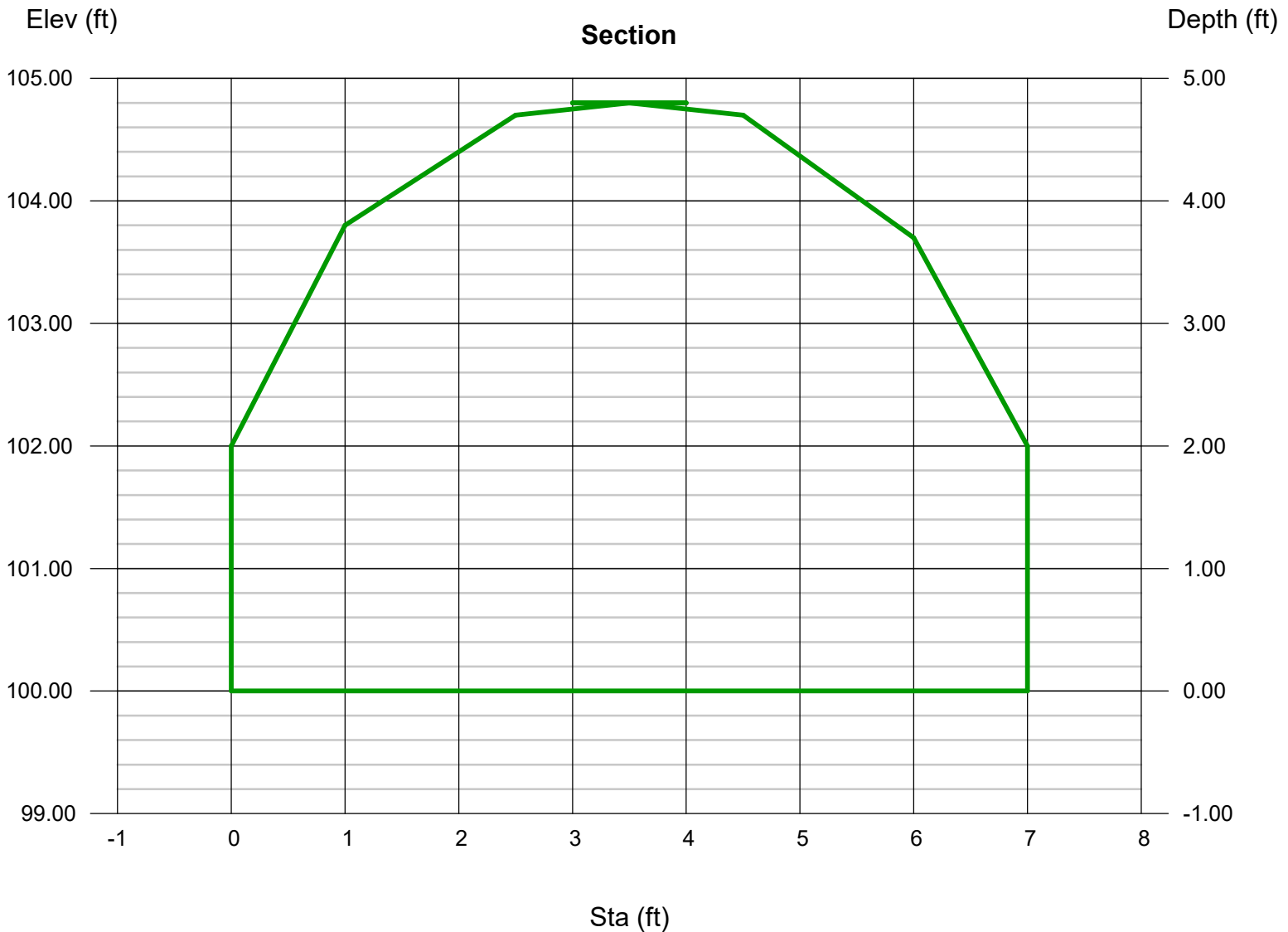
Depth (ft) = 4.80  
Q (cfs) = 164.15  
Area (sqft) = 27.93  
Velocity (ft/s) = 5.88  
Wetted Perim (ft) = 20.59  
Crit Depth, Yc (ft) = 2.53  
Top Width (ft) = 0.00  
EGL (ft) = 5.34

### Calculations

Compute by: Q vs Depth  
No. Increments = 1

### (Sta, El, n)-(Sta, El, n)...

(4.00, 104.80)-(3.50, 104.80, 0.017)-(2.50, 104.70, 0.017)-(1.00, 103.80, 0.017)-(7.00, 100.00, 0.017)-(7.00, 102.00, 0.017)-(6.00, 103.70, 0.017)  
-(4.50, 104.70, 0.017)-(3.50, 104.80, 0.017)-(3.00, 104.80, 0.017)



# Channel Report

## Section 6 - Open Channel Before Pembroke Conduit

### User-defined

Invert Elev (ft) = 100.00  
Slope (%) = 1.10  
N-Value = Composite

### Highlighted

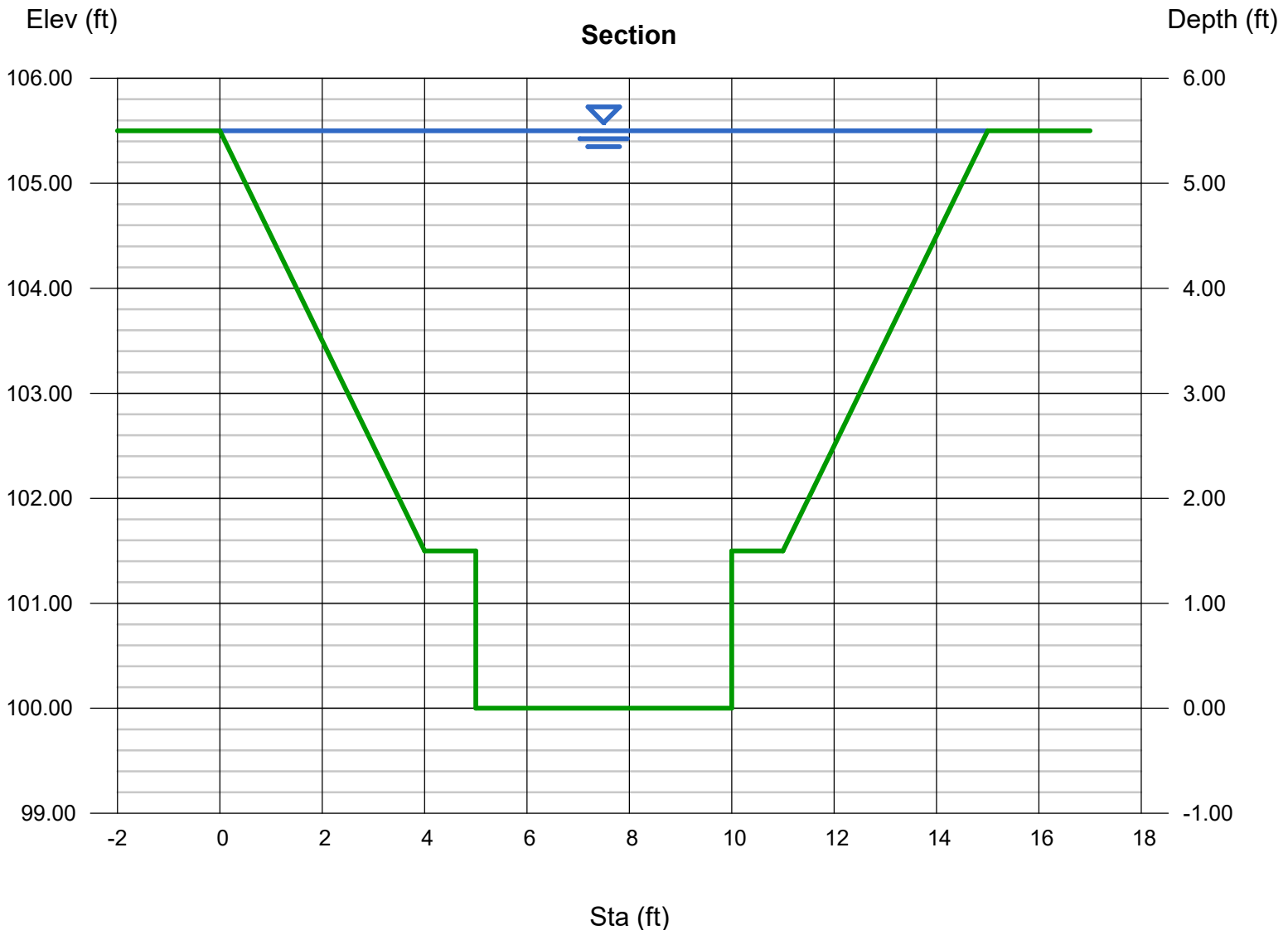
Depth (ft) = 5.50  
Q (cfs) = 658.80  
Area (sqft) = 51.50  
Velocity (ft/s) = 12.79  
Wetted Perim (ft) = 21.31  
Crit Depth, Yc (ft) = 5.50  
Top Width (ft) = 15.00  
EGL (ft) = 8.04

### Calculations

Compute by: Q vs Depth  
No. Increments = 11

### (Sta, El, n)-(Sta, El, n)...

(0.00, 105.50)-(4.00, 101.50, 0.024)-(5.00, 101.50, 0.024)-(5.00, 100.00, 0.017)-(10.00, 100.00, 0.017)-(10.00, 101.50, 0.024)-(11.00, 101.50, 0.024)  
-(15.00, 105.50, 0.024)



# Channel Report

## Section 7 - Pembroke Bridge

### User-defined

Invert Elev (ft) = 100.00  
Slope (%) = 0.26  
N-Value = Composite

### Highlighted

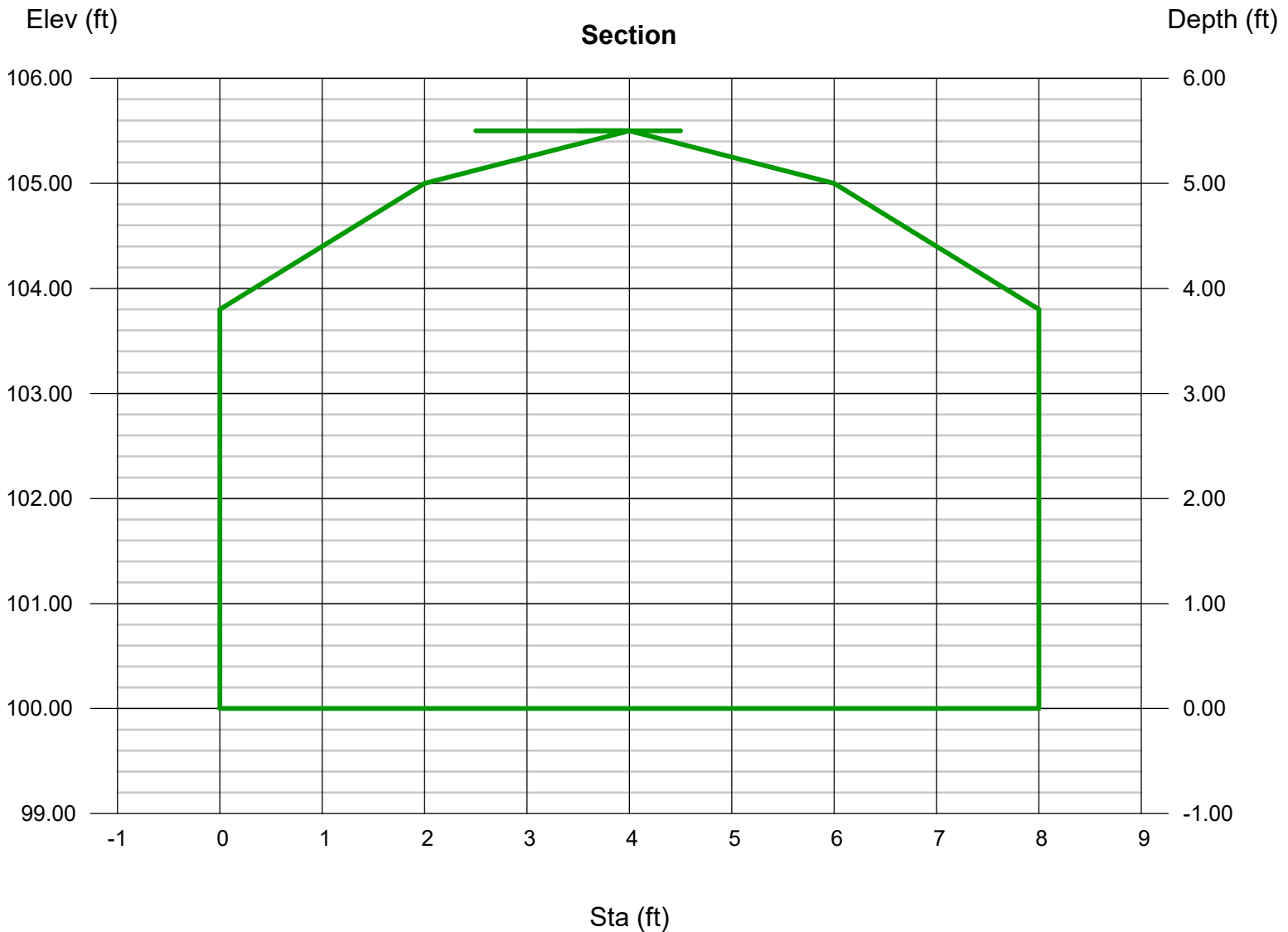
Depth (ft) = 5.50  
Q (cfs) = 234.17  
Area (sqft) = 38.60  
Velocity (ft/s) = 6.07  
Wetted Perim (ft) = 24.39  
Crit Depth, Yc (ft) = 2.99  
Top Width (ft) = 0.00  
EGL (ft) = 6.07

### Calculations

Compute by: Q vs Depth  
No. Increments = 1

### (Sta, El, n)-(Sta, El, n)...

(3.50, 105.50)-(4.00, 105.50, 0.017)-(2.00, 105.00, 0.017)-(8.00, 100.00, 0.017)-(8.00, 103.80, 0.017)-(6.00, 105.00, 0.017)-(4.00, 105.50, 0.017)  
-(3.50, 105.50, 0.017)





# Channel Report

## Section 8 - Reach Between Pembroke Conduit and Meadowbrook Culvert

### User-defined

Invert Elev (ft) = 100.00  
Slope (%) = 0.27  
N-Value = Composite

### Highlighted

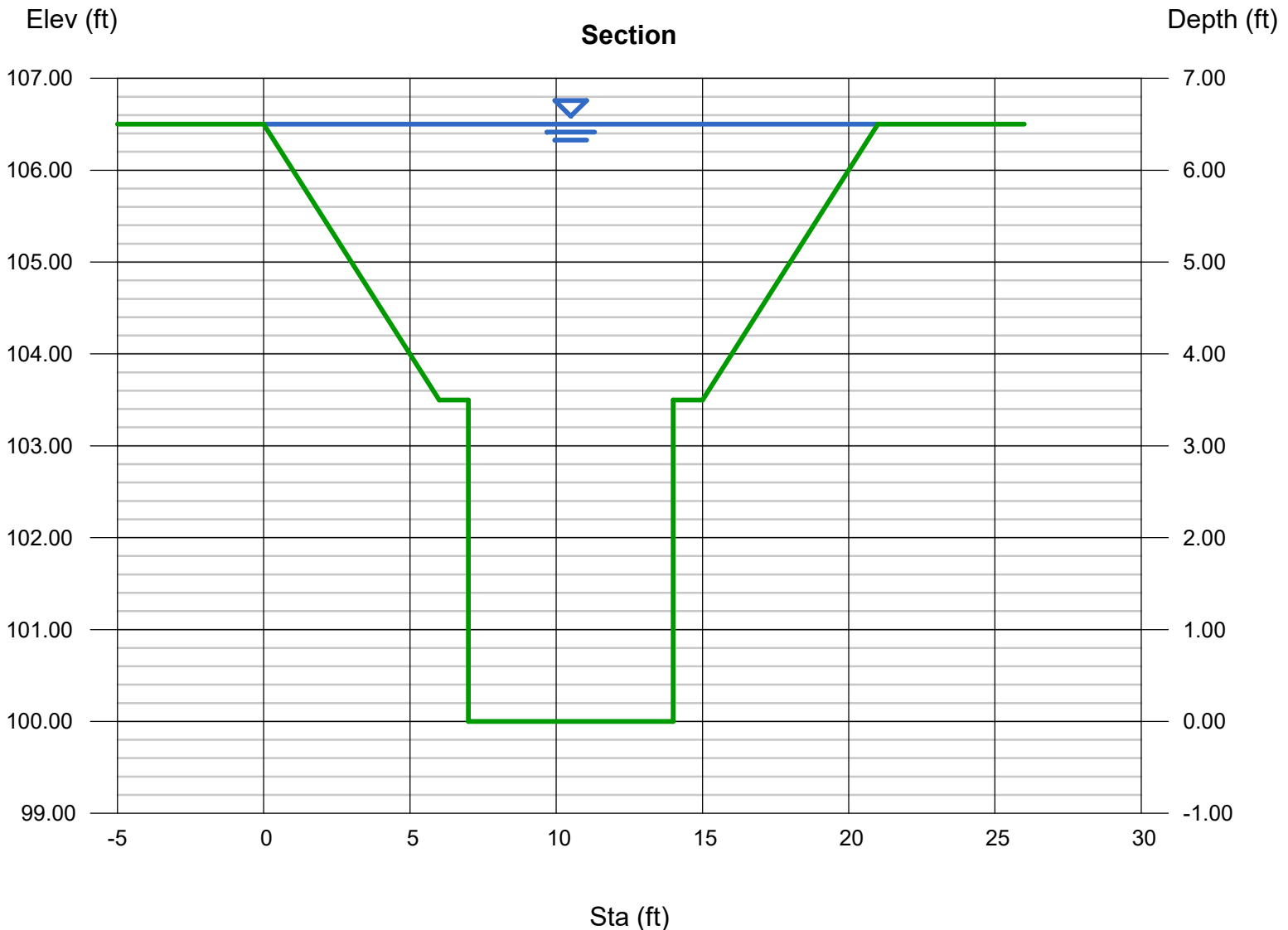
Depth (ft) = 6.50  
Q (cfs) = 440.99  
Area (sqft) = 69.50  
Velocity (ft/s) = 6.35  
Wetted Perim (ft) = 29.42  
Crit Depth, Yc (ft) = 5.22  
Top Width (ft) = 21.00  
EGL (ft) = 7.13

### Calculations

Compute by: Q vs Depth  
No. Increments = 1

### (Sta, El, n)-(Sta, El, n)...

(0.00, 106.50)-(6.00, 103.50, 0.024)-(7.00, 103.50, 0.024)-(7.00, 100.00, 0.017)-(14.00, 100.00, 0.017)-(14.00, 103.50, 0.024)-(15.00, 103.50, 0.024)-(21.00, 106.50, 0.024)



# Channel Report

## Section 9 - Meadowbrook Bridge

### User-defined

Invert Elev (ft) = 100.00  
Slope (%) = 0.27  
N-Value = Composite

### Highlighted

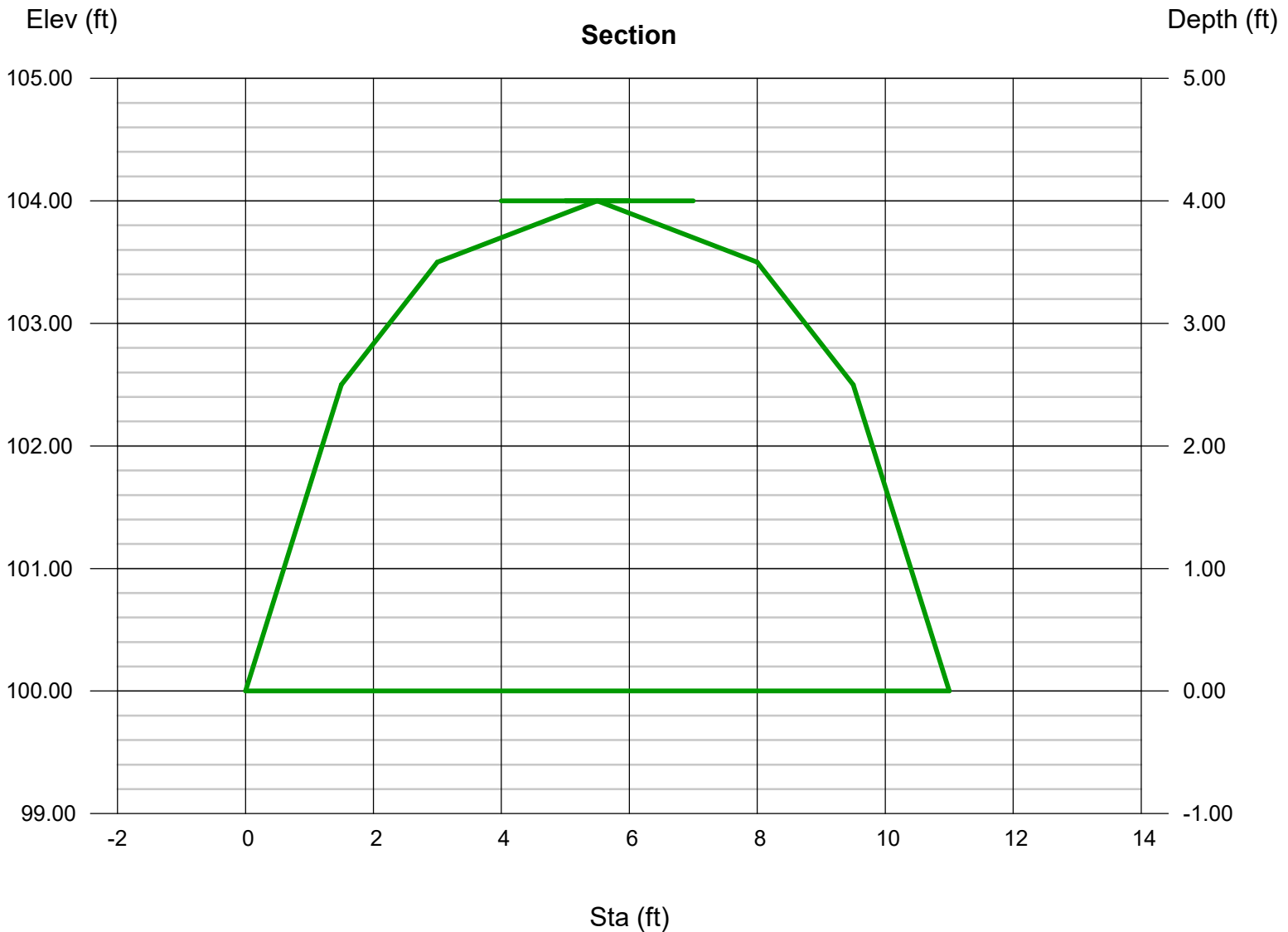
Depth (ft) = 4.00  
Q (cfs) = 164.91  
Area (sqft) = 31.50  
Velocity (ft/s) = 5.24  
Wetted Perim (ft) = 25.54  
Crit Depth, Yc (ft) = 1.98  
Top Width (ft) = 0.00  
EGL (ft) = 4.43

### Calculations

Compute by: Q vs Depth  
No. Increments = 1

### (Sta, El, n)-(Sta, El, n)...

(6.00, 104.00)-(5.50, 104.00, 0.017)-(3.00, 103.50, 0.017)-(1.50, 102.50, 0.017)-(11.00, 100.00, 0.017)-(9.50, 102.50, 0.017)-(8.00, 103.50, 0.017)  
-(5.50, 104.00, 0.017)-(5.00, 104.00, 0.017)



# Channel Report

## Section 10

### Trapezoidal

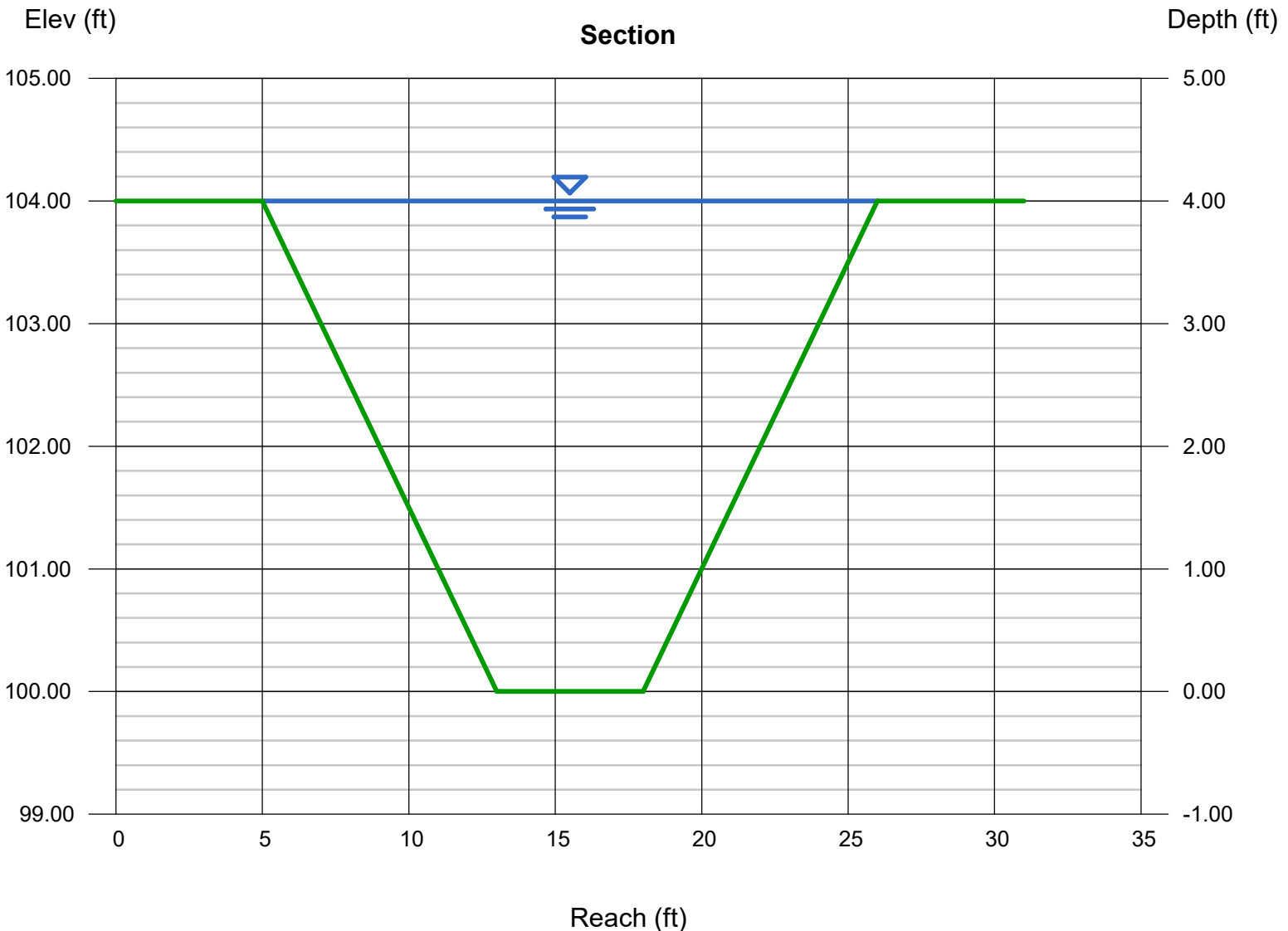
Bottom Width (ft) = 5.00  
Side Slopes (z:1) = 2.00, 2.00  
Total Depth (ft) = 4.00  
Invert Elev (ft) = 100.00  
Slope (%) = 0.99  
N-Value = 0.024

### Highlighted

Depth (ft) = 4.00  
Q (cfs) = 553.78  
Area (sqft) = 52.00  
Velocity (ft/s) = 10.65  
Wetted Perim (ft) = 22.89  
Crit Depth, Yc (ft) = 4.00  
Top Width (ft) = 21.00  
EGL (ft) = 5.76

### Calculations

Compute by: Q vs Depth  
No. Increments = 1



# Channel Report

## Section 11 - Southern Reach Between Meadowbrook Avenue and Orchard Way

### User-defined

Invert Elev (ft) = 100.00  
Slope (%) = 0.99  
N-Value = Composite

### Highlighted

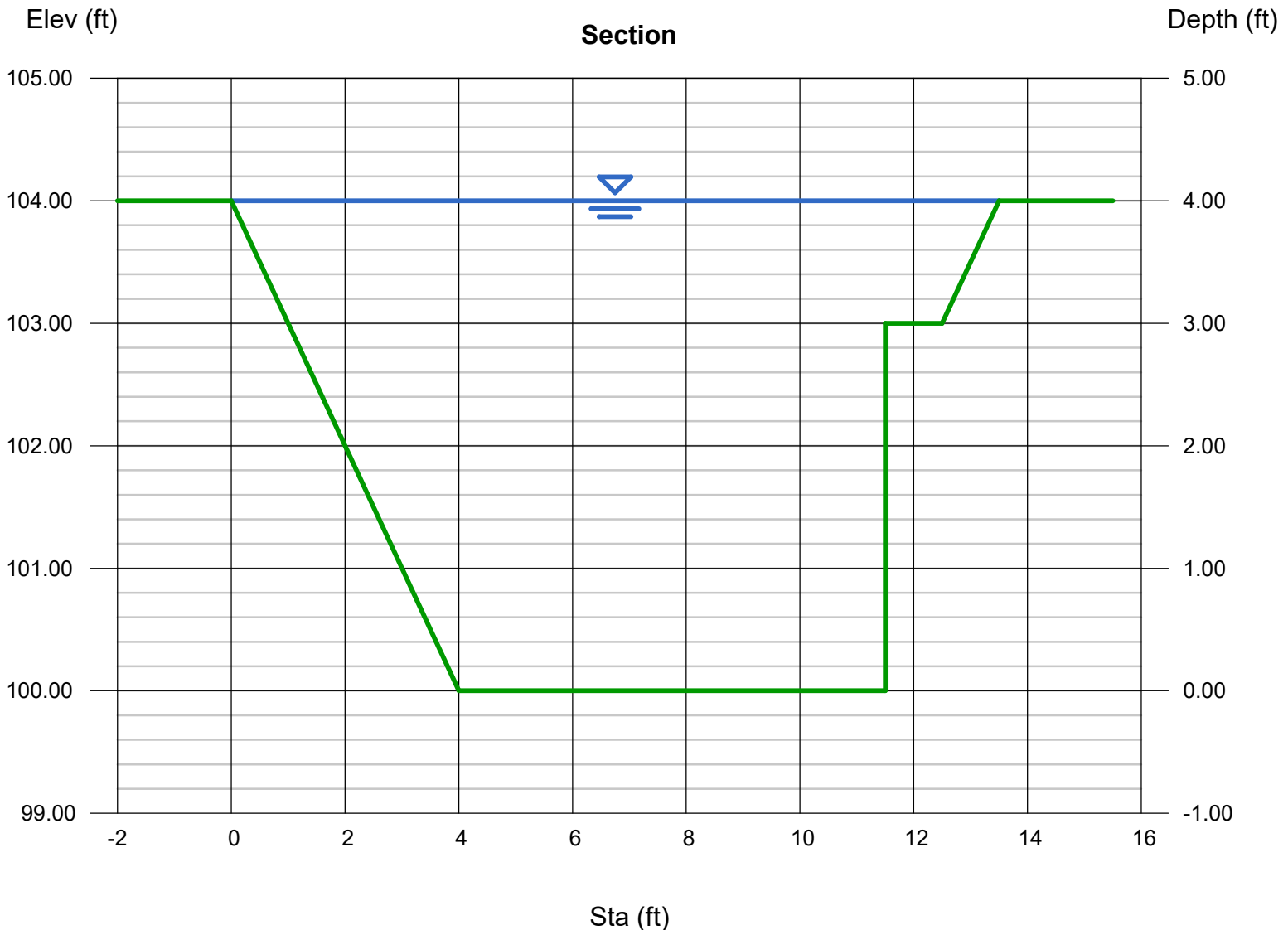
Depth (ft) = 4.00  
Q (cfs) = 428.56  
Area (sqft) = 39.50  
Velocity (ft/s) = 10.85  
Wetted Perim (ft) = 18.57  
Crit Depth, Yc (ft) = 4.00  
Top Width (ft) = 13.50  
EGL (ft) = 5.83

### Calculations

Compute by: Q vs Depth  
No. Increments = 1

### (Sta, El, n)-(Sta, El, n)...

(0.00, 104.00)-(4.00, 100.00, 0.024)-(11.50, 100.00, 0.017)-(11.50, 103.00, 0.017)-(12.50, 103.00, 0.017)-(13.50, 104.00, 0.024)



# Channel Report

## Section 12 - Orchard Bridge

### User-defined

Invert Elev (ft) = 100.00  
Slope (%) = 0.92  
N-Value = Composite

### Highlighted

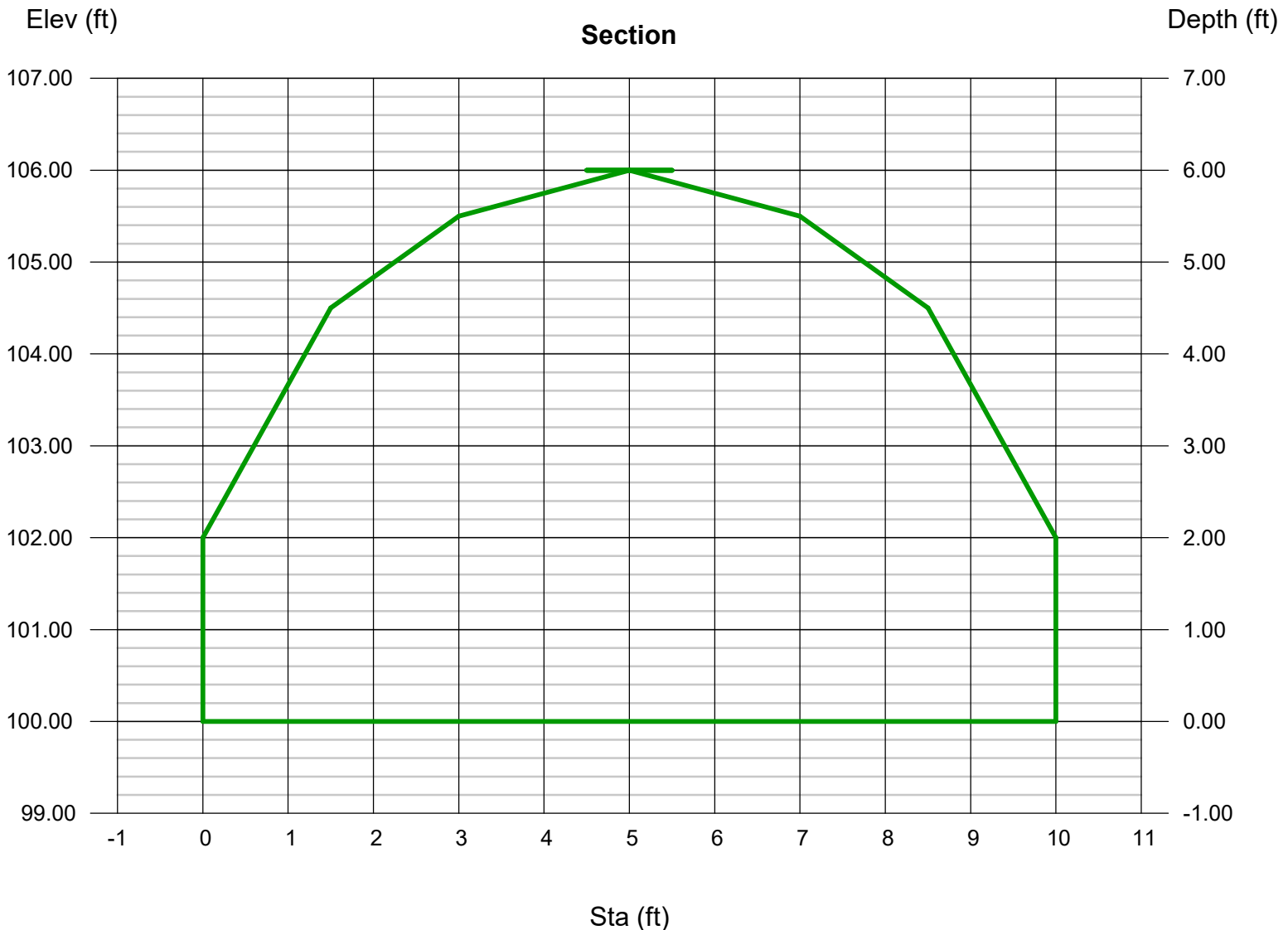
Depth (ft) = 6.00  
Q (cfs) = 578.81  
Area (sqft) = 47.75  
Velocity (ft/s) = 12.12  
Wetted Perim (ft) = 27.56  
Crit Depth, Yc (ft) = 4.55  
Top Width (ft) = 0.00  
EGL (ft) = 8.28

### Calculations

Compute by: Q vs Depth  
No. Increments = 1

### (Sta, El, n)-(Sta, El, n)...

( 5.50, 106.00)-(5.00, 106.00, 0.017)-(3.00, 105.50, 0.017)-(1.50, 104.50, 0.017)-(10.00, 100.00, 0.017)-(10.00, 102.00, 0.017)-(8.50, 104.50, 0.017)  
-(7.00, 105.50, 0.017)-(5.00, 106.00, 0.017)-(4.50, 106.00, 0.017)



# Channel Report

## Section 13 - Reach Between Orchard Way and Iven Avenue

### Trapezoidal

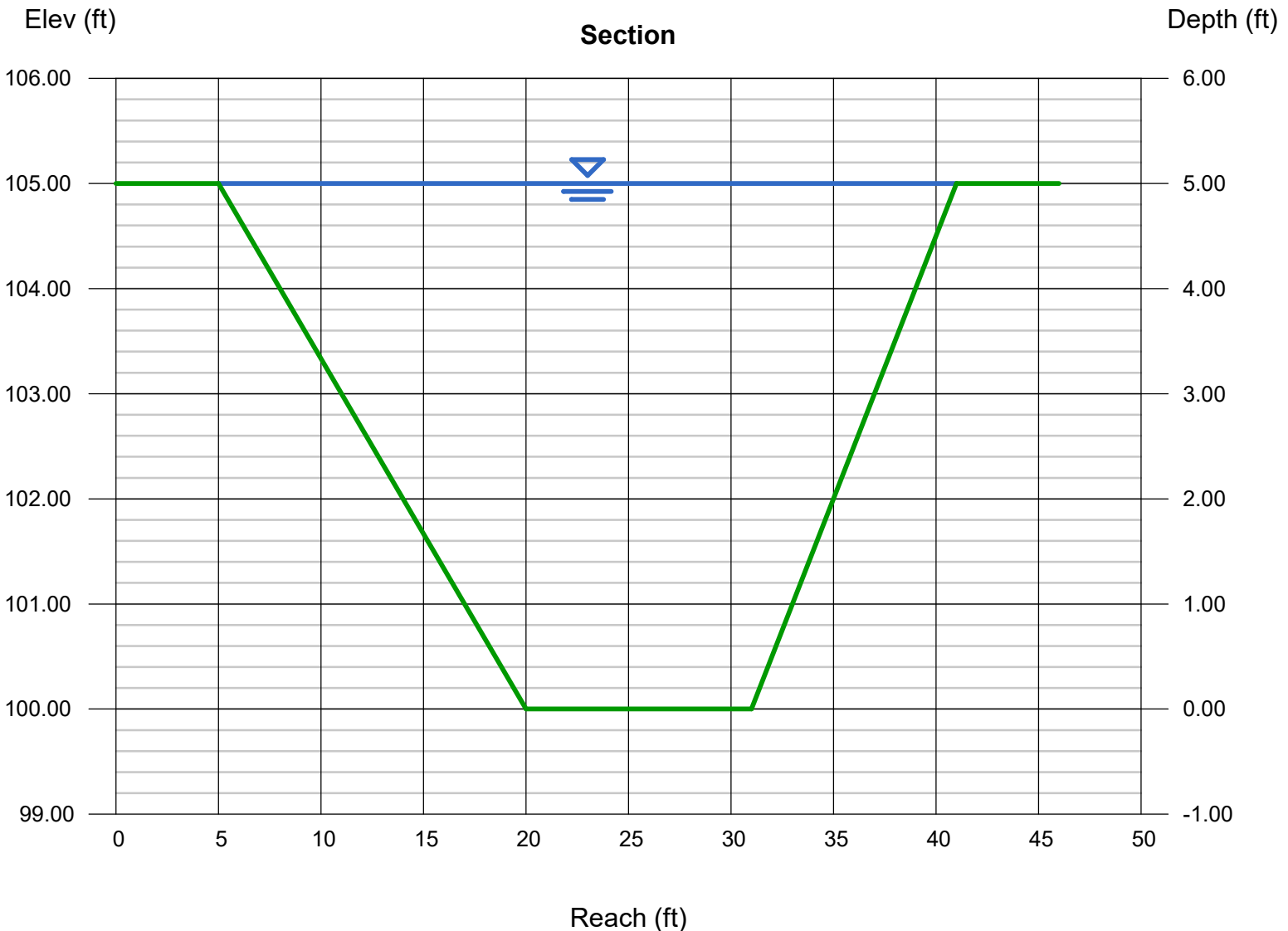
Bottom Width (ft) = 11.00  
Side Slopes (z:1) = 3.00, 2.00  
Total Depth (ft) = 5.00  
Invert Elev (ft) = 100.00  
Slope (%) = 0.62  
N-Value = 0.024

### Highlighted

Depth (ft) = 5.00  
Q (cfs) = 1,216  
Area (sqft) = 117.50  
Velocity (ft/s) = 10.35  
Wetted Perim (ft) = 37.99  
Crit Depth, Yc (ft) = 5.00  
Top Width (ft) = 36.00  
EGL (ft) = 6.67

### Calculations

Compute by: Q vs Depth  
No. Increments = 1



# Channel Report

## Section 14 - Iven Bridge

### User-defined

Invert Elev (ft) = 100.00  
Slope (%) = 1.10  
N-Value = Composite

### Highlighted

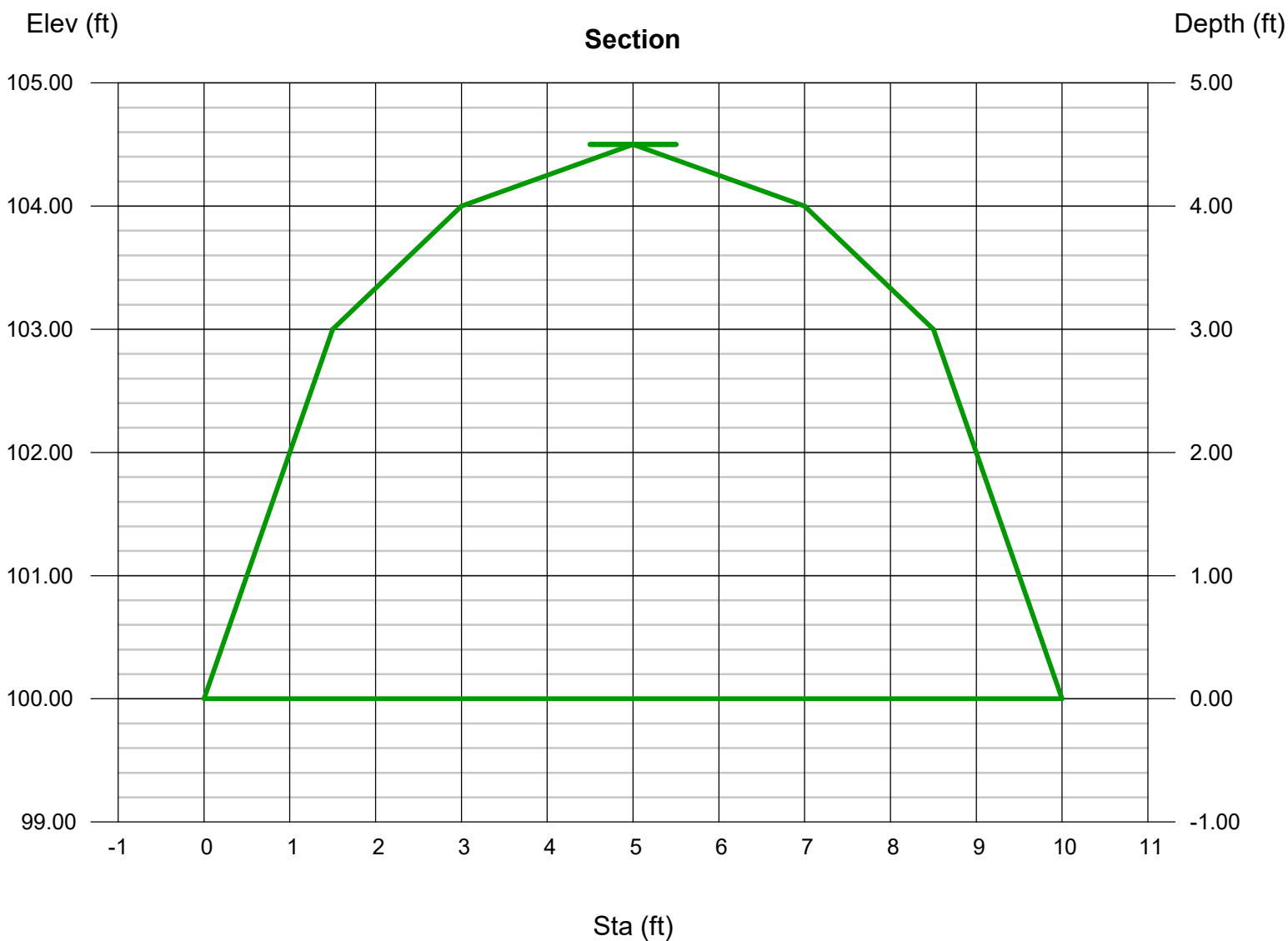
Depth (ft) = 4.50  
Q (cfs) = 351.89  
Area (sqft) = 32.00  
Velocity (ft/s) = 11.00  
Wetted Perim (ft) = 24.44  
Crit Depth, Yc (ft) = 3.41  
Top Width (ft) = 0.00  
EGL (ft) = 6.38

### Calculations

Compute by: Q vs Depth  
No. Increments = 1

### (Sta, El, n)-(Sta, El, n)...

(5.50, 104.50)-(5.00, 104.50, 0.017)-(3.00, 104.00, 0.017)-(1.50, 103.00, 0.017)-(10.00, 100.00, 0.017)-(8.50, 103.00, 0.017)-(7.00, 104.00, 0.017)  
-(5.00, 104.50, 0.017)-(4.50, 104.50, 0.017)



# Channel Report

## Section 15 - Township Entrance Bridge 72x96 ECP

### User-defined

Invert Elev (ft) = 97.00  
Slope (%) = 1.00  
N-Value = Composite

### Highlighted

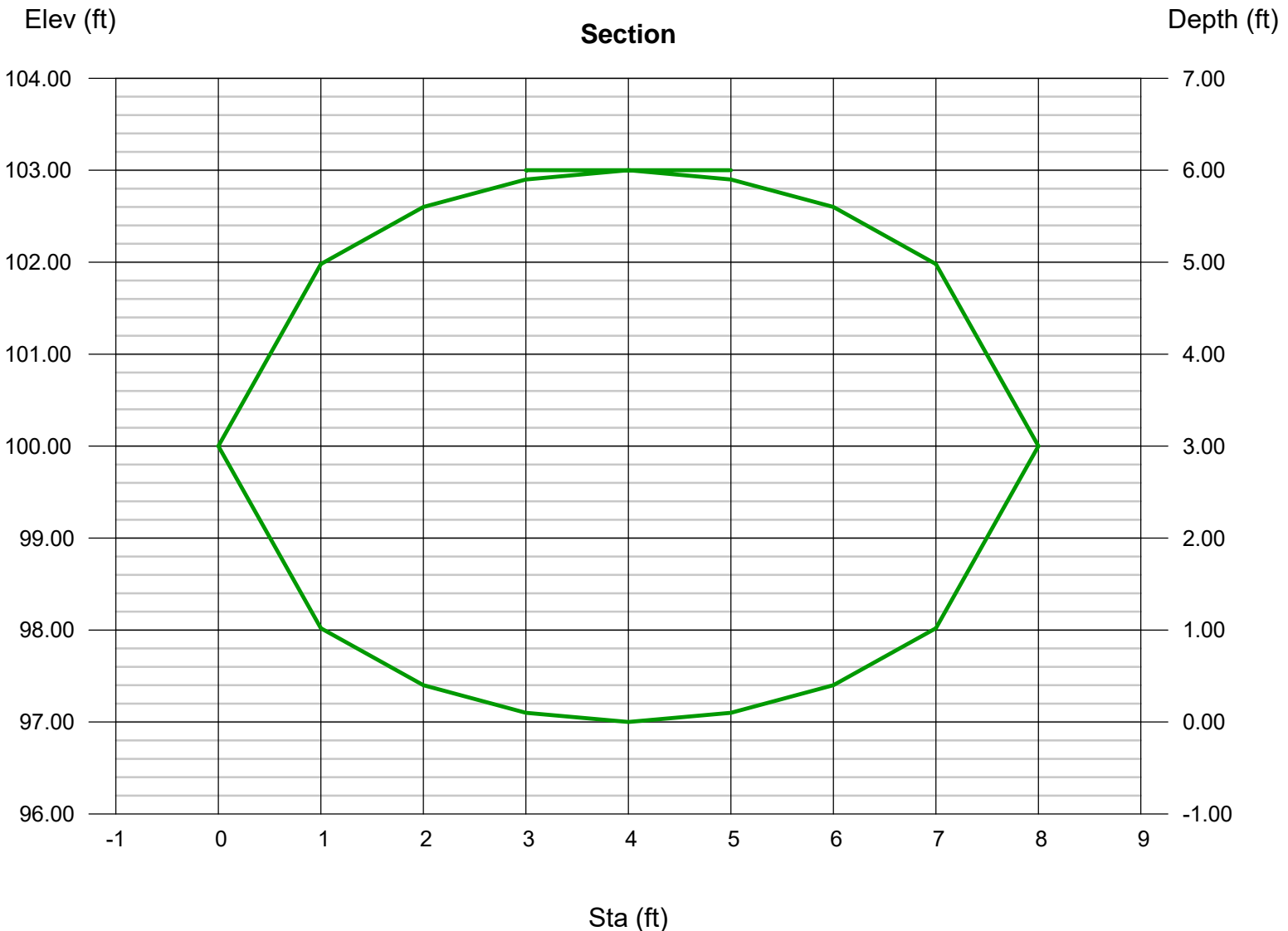
Depth (ft) = 6.00  
Q (cfs) = 393.05  
Area (sqft) = 35.92  
Velocity (ft/s) = 10.94  
Wetted Perim (ft) = 21.78  
Crit Depth, Yc (ft) = 4.84  
Top Width (ft) = 0.00  
EGL (ft) = 7.86

### Calculations

Compute by: Q vs Depth  
No. Increments = 1

### (Sta, El, n)-(Sta, El, n)...

( 4.00, 103.00)-(3.00, 102.90, 0.019)-(2.00, 102.60, 0.019)-(1.00, 101.98, 0.019)-(1.00, 98.02, 0.019)-(2.00, 97.40, 0.019)-(3.00, 97.10, 0.019)  
-(4.00, 97.00, 0.019)-(5.00, 97.10, 0.019)-(6.00, 97.40, 0.019)-(7.00, 98.02, 0.019)-(8.00, 100.00, 0.019)-(7.00, 101.98, 0.019)-(6.00, 102.60, 0.019)  
-(5.00, 102.90, 0.019)-(4.00, 103.00, 0.019)





## **PROPOSED SECTIONS**

# Channel Report

## Section 1 (Equivalent Circular Pipe) - Elliptical Proposed

### Circular

Diameter (ft) = 7.00

Invert Elev (ft) = 100.00

Slope (%) = 0.80

N-Value = 0.017

### Calculations

Compute by: Q vs Depth

No. Increments = 1

### Highlighted

Depth (ft) = 7.00

Q (cfs) = 437.03

Area (sqft) = 38.48

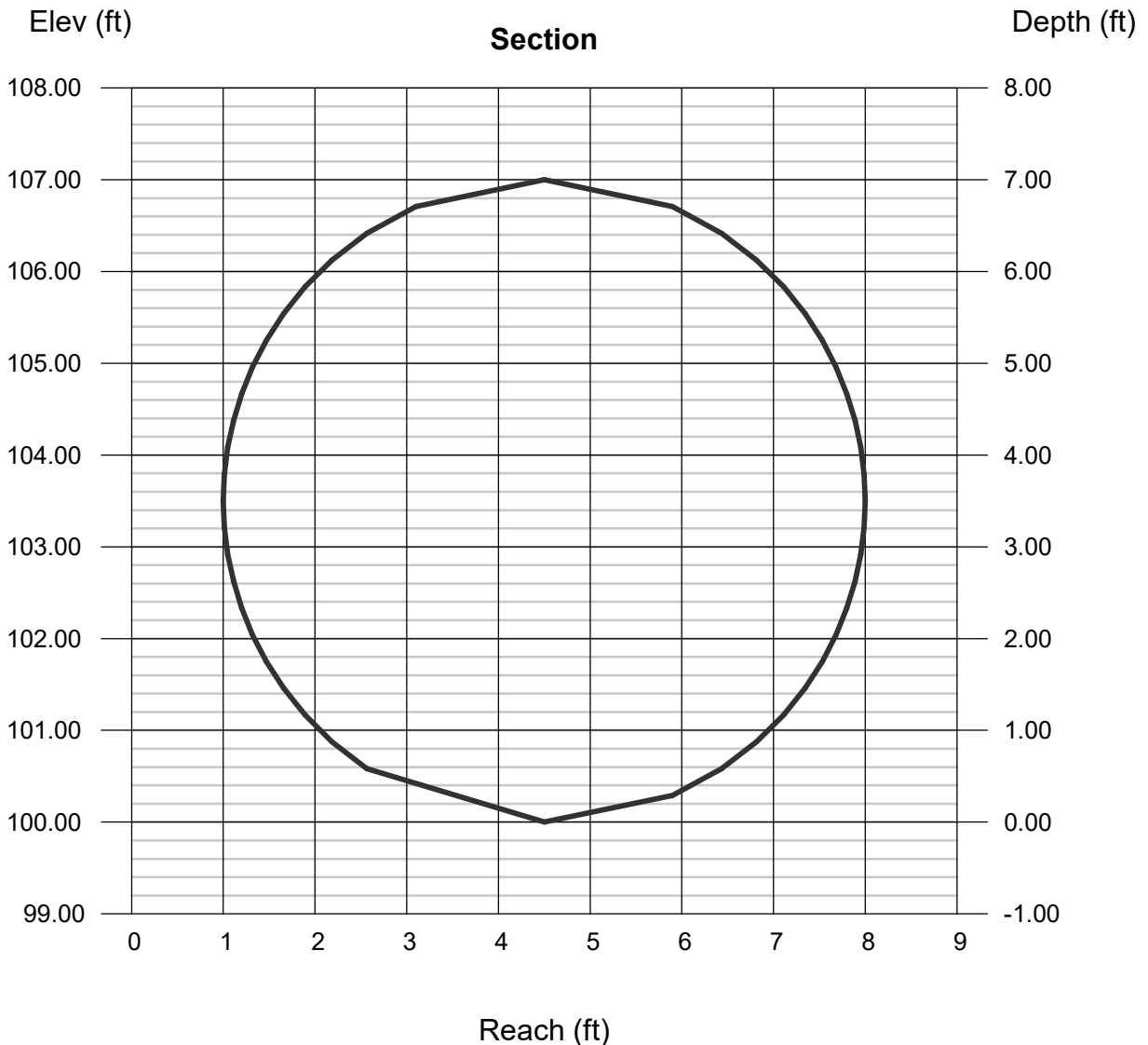
Velocity (ft/s) = 11.36

Wetted Perim (ft) = 21.99

Crit Depth, Yc (ft) = 5.49

Top Width (ft) = 0.00

EGL (ft) = 9.00



# Channel Report

## Section 2 & 3 Proposed

### Rectangular

Bottom Width (ft) = 11.50  
Total Depth (ft) = 5.00

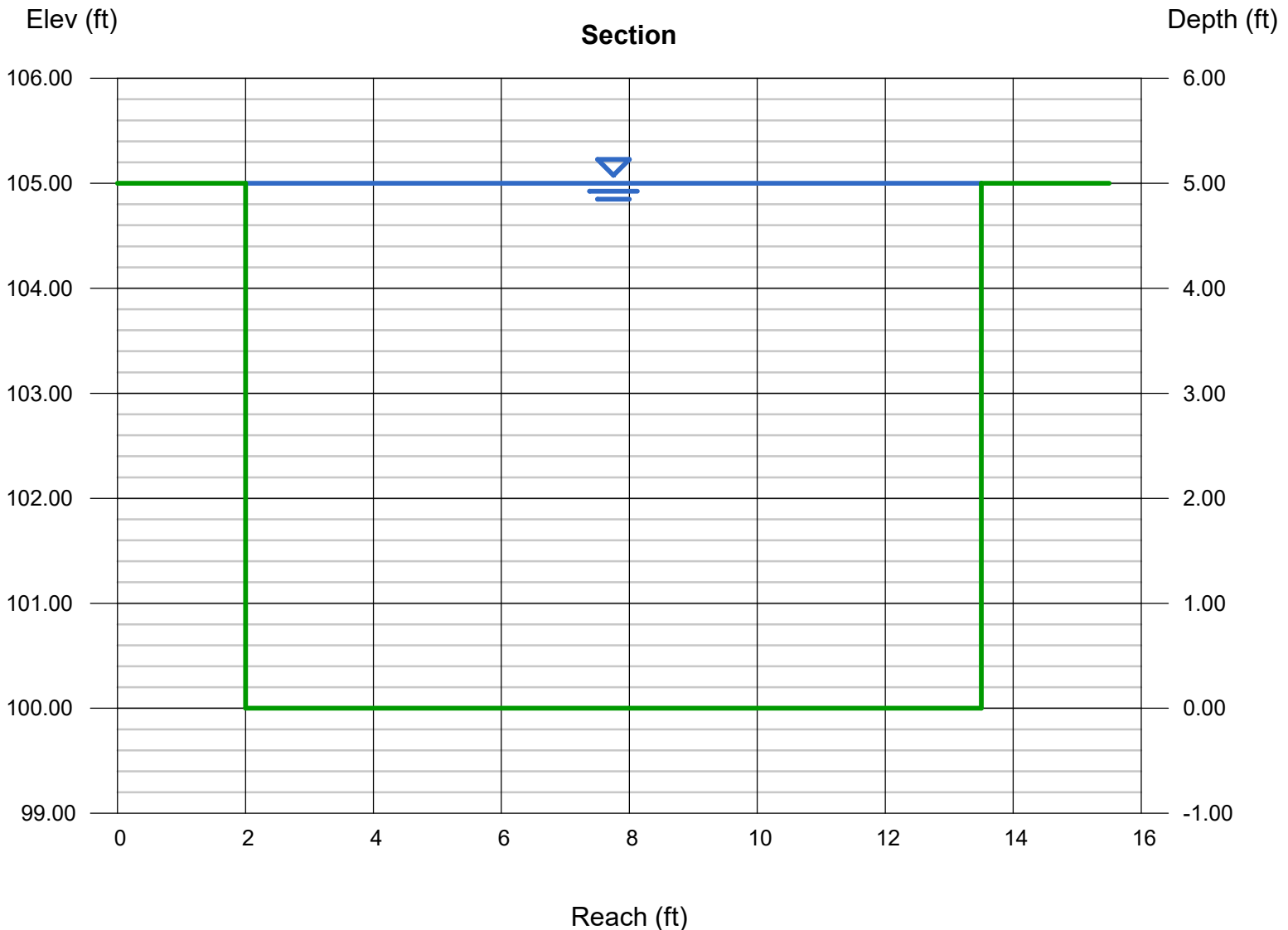
Invert Elev (ft) = 100.00  
Slope (%) = 0.90  
N-Value = 0.024

### Calculations

Compute by: Q vs Depth  
No. Increments = 10

### Highlighted

Depth (ft) = 5.00  
Q (cfs) = 650.97  
Area (sqft) = 57.50  
Velocity (ft/s) = 11.32  
Wetted Perim (ft) = 21.50  
Crit Depth, Yc (ft) = 4.64  
Top Width (ft) = 11.50  
EGL (ft) = 6.99



# Channel Report

## Section 4 Proposed

### Rectangular

Bottom Width (ft) = 8.00  
Total Depth (ft) = 4.70

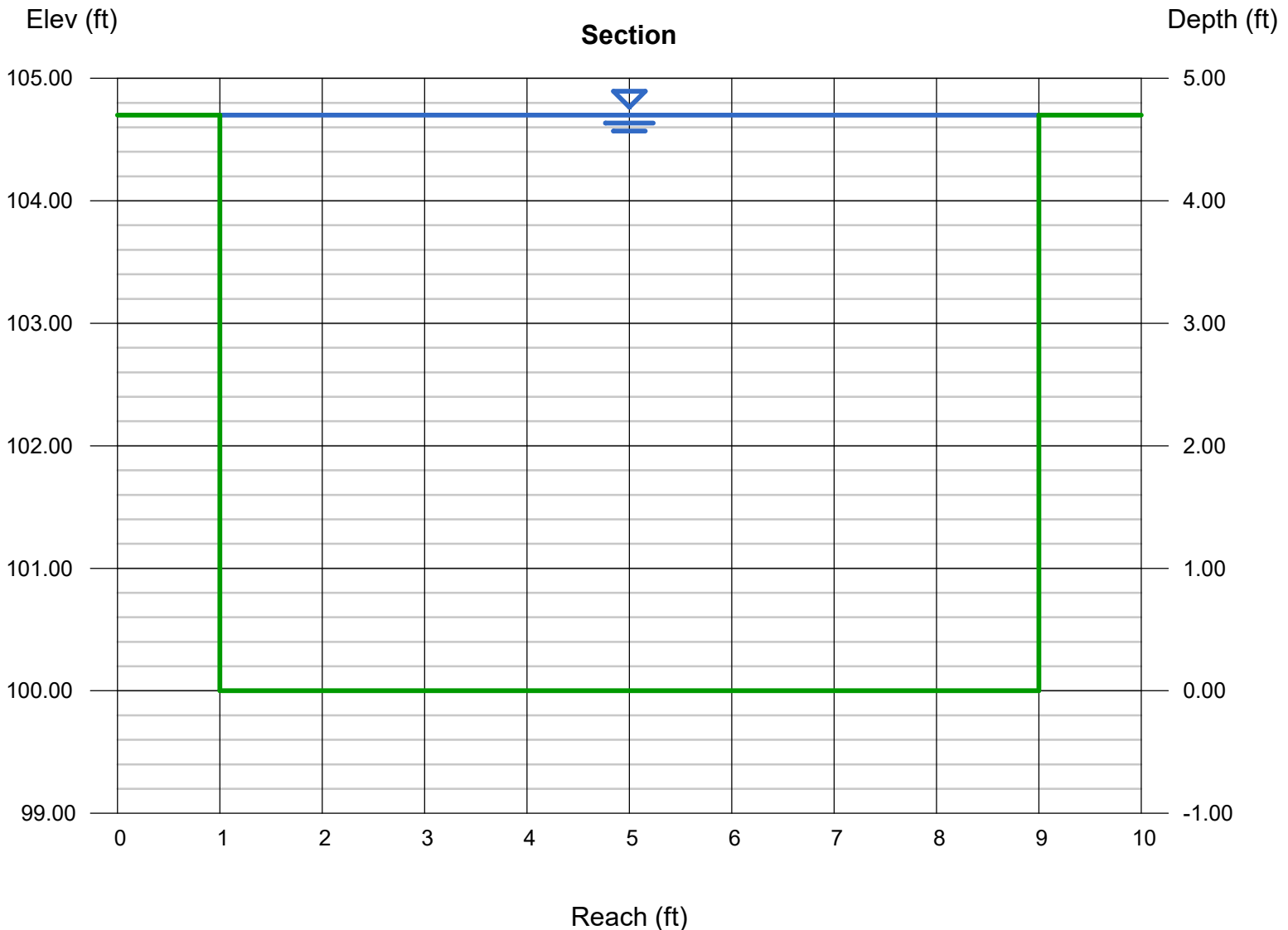
Invert Elev (ft) = 100.00  
Slope (%) = 1.52  
N-Value = 0.017

### Calculations

Compute by: Q vs Depth  
No. Increments = 1

### Highlighted

Depth (ft) = 4.70  
Q (cfs) = 677.46  
Area (sqft) = 37.60  
Velocity (ft/s) = 18.02  
Wetted Perim (ft) = 17.40  
Crit Depth, Yc (ft) = 4.70  
Top Width (ft) = 8.00  
EGL (ft) = 9.75



# Channel Report

## Section 5 Proposed

### Trapezoidal

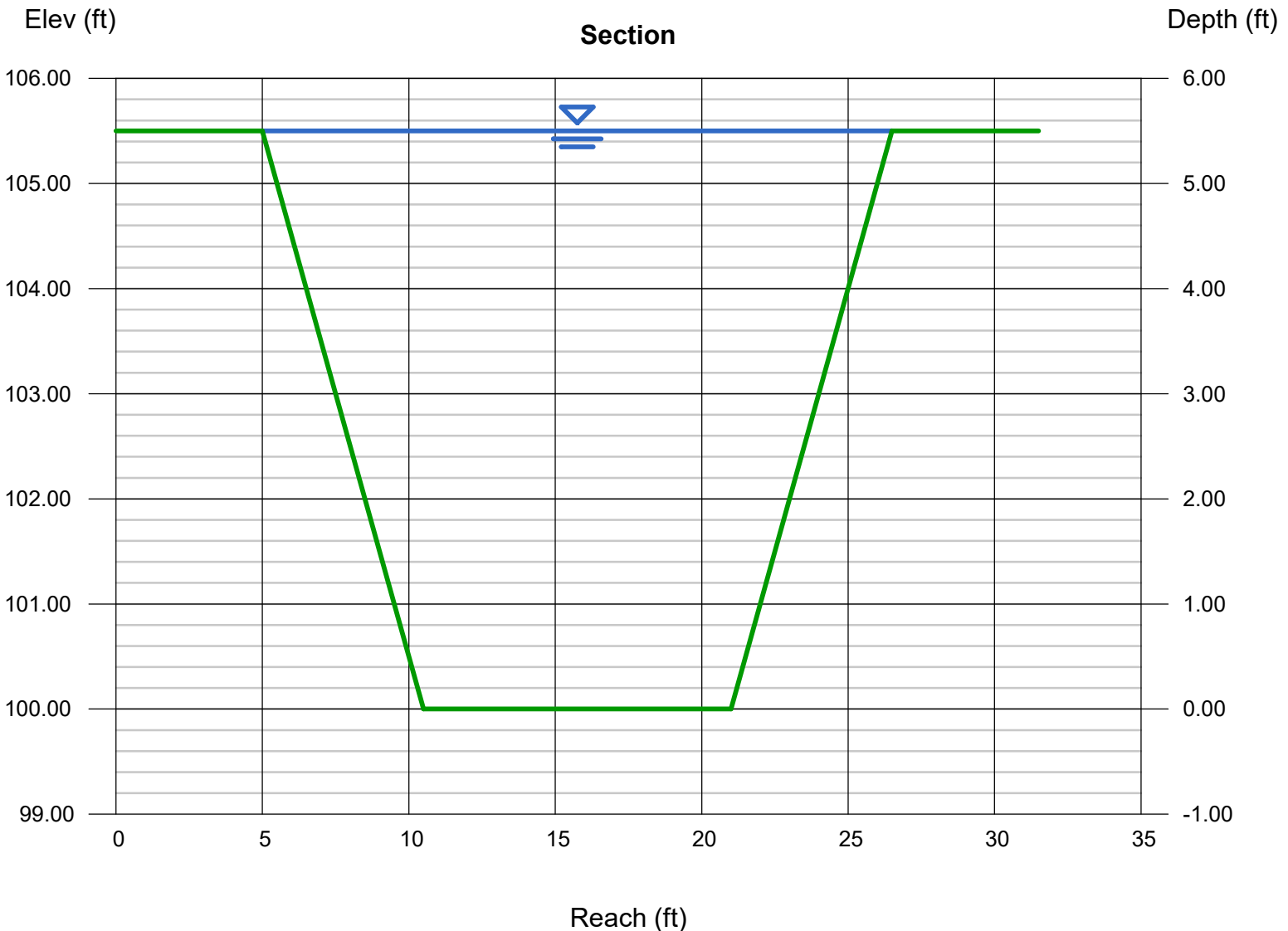
Bottom Width (ft) = 10.50  
Side Slopes (z:1) = 1.00, 1.00  
Total Depth (ft) = 5.50  
Invert Elev (ft) = 100.00  
Slope (%) = 0.30  
N-Value = 0.024

### Highlighted

Depth (ft) = 5.50  
Q (cfs) = 672.06  
Area (sqft) = 88.00  
Velocity (ft/s) = 7.64  
Wetted Perim (ft) = 26.06  
Crit Depth, Yc (ft) = 4.36  
Top Width (ft) = 21.50  
EGL (ft) = 6.41

### Calculations

Compute by: Q vs Depth  
No. Increments = 1



# Channel Report

## Section 7 Proposed

### Rectangular

Bottom Width (ft) = 15.50

Total Depth (ft) = 5.50

Invert Elev (ft) = 100.00

Slope (%) = 0.26

N-Value = 0.017

### Calculations

Compute by: Q vs Depth

No. Increments = 10

### Highlighted

Depth (ft) = 5.50

Q (cfs) = 828.36

Area (sqft) = 85.25

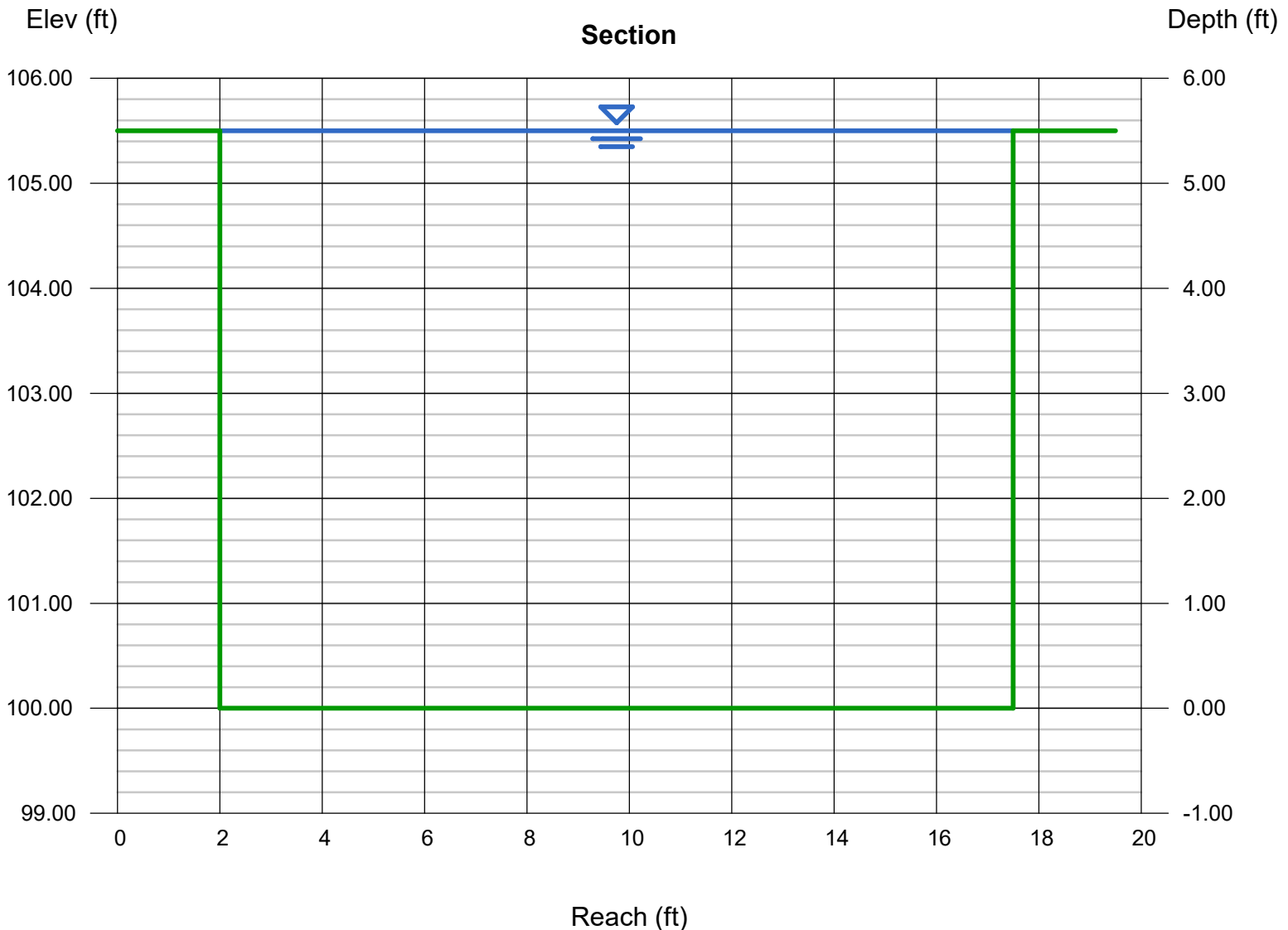
Velocity (ft/s) = 9.72

Wetted Perim (ft) = 26.50

Crit Depth, Yc (ft) = 4.47

Top Width (ft) = 15.50

EGL (ft) = 6.97



# Channel Report

## Section 8 Proposed

### Trapezoidal

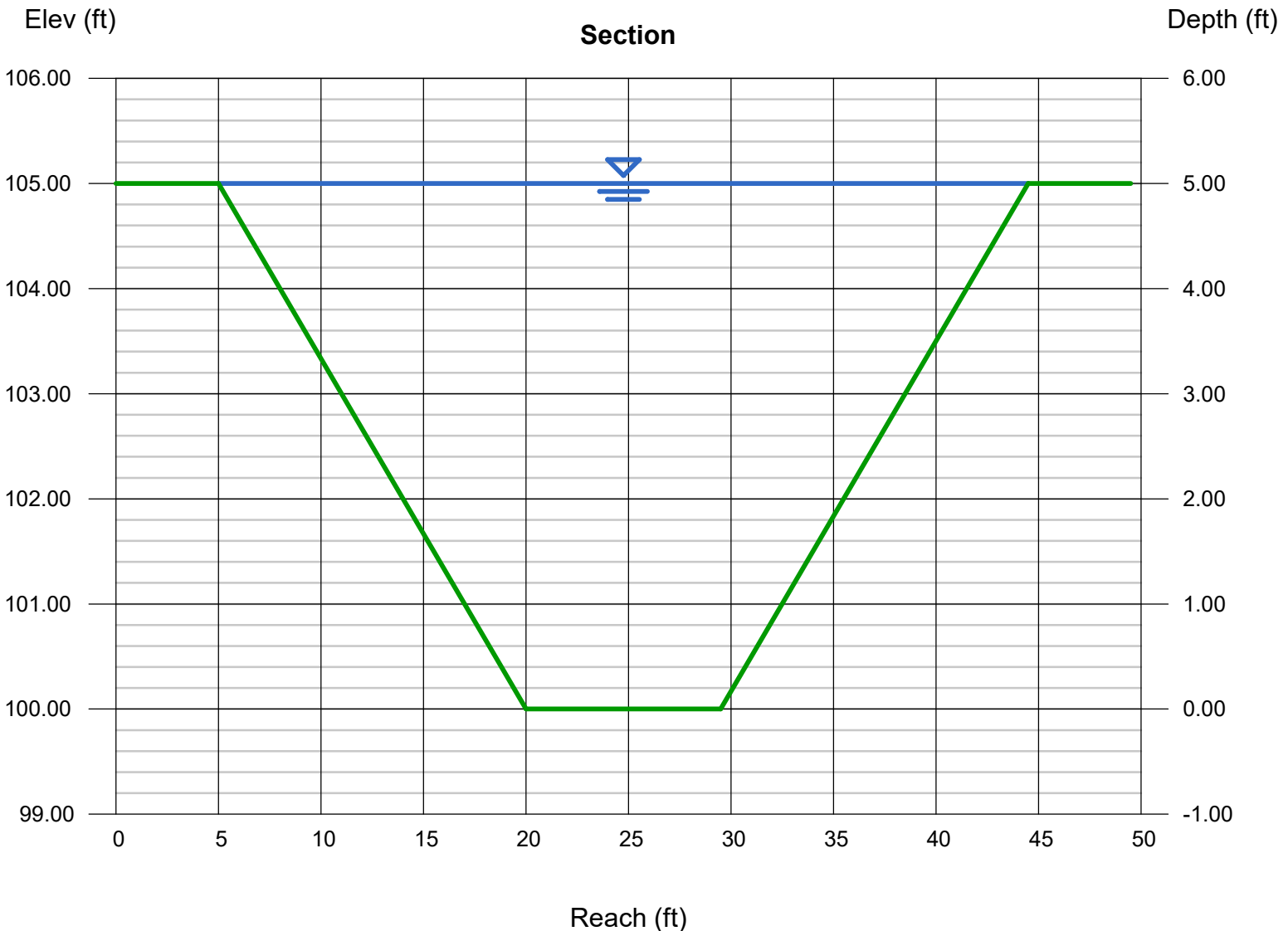
Bottom Width (ft) = 9.50  
Side Slopes (z:1) = 3.00, 3.00  
Total Depth (ft) = 5.00  
Invert Elev (ft) = 100.00  
Slope (%) = 0.27  
N-Value = 0.024

### Highlighted

Depth (ft) = 5.00  
Q (cfs) = 816.24  
Area (sqft) = 122.50  
Velocity (ft/s) = 6.66  
Wetted Perim (ft) = 41.12  
Crit Depth, Yc (ft) = 4.09  
Top Width (ft) = 39.50  
EGL (ft) = 5.69

### Calculations

Compute by: Q vs Depth  
No. Increments = 10



# Channel Report

## Section 9 Proposed

### Rectangular

Bottom Width (ft) = 23.50

Total Depth (ft) = 4.00

Invert Elev (ft) = 100.00

Slope (%) = 0.27

N-Value = 0.017

### Calculations

Compute by: Q vs Depth

No. Increments = 10

### Highlighted

Depth (ft) = 4.00

Q (cfs) = 885.28

Area (sqft) = 94.00

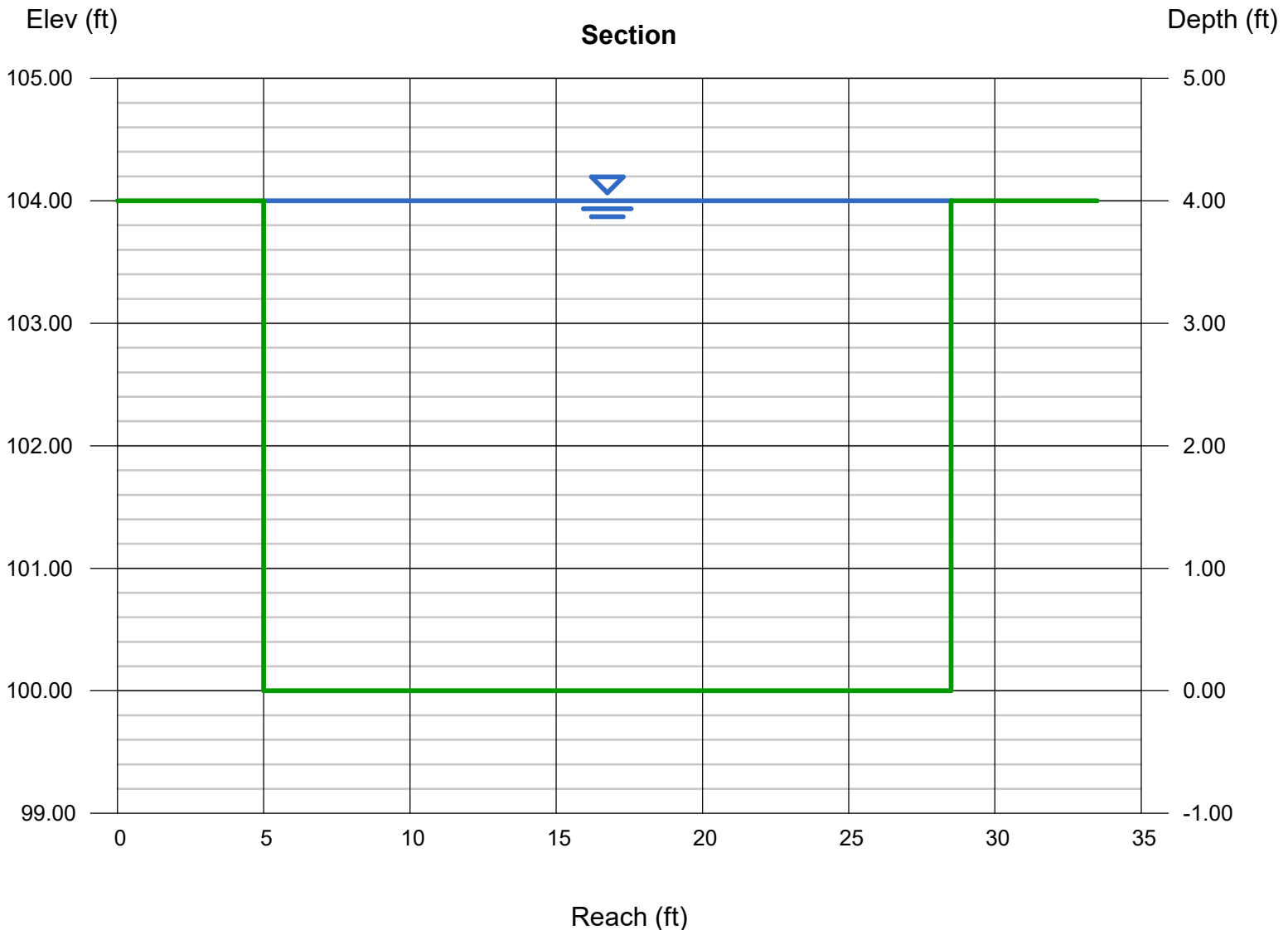
Velocity (ft/s) = 9.42

Wetted Perim (ft) = 31.50

Crit Depth, Yc (ft) = 3.54

Top Width (ft) = 23.50

EGL (ft) = 5.38





# Channel Report

## Section 10 & 11 Proposed

### Trapezoidal

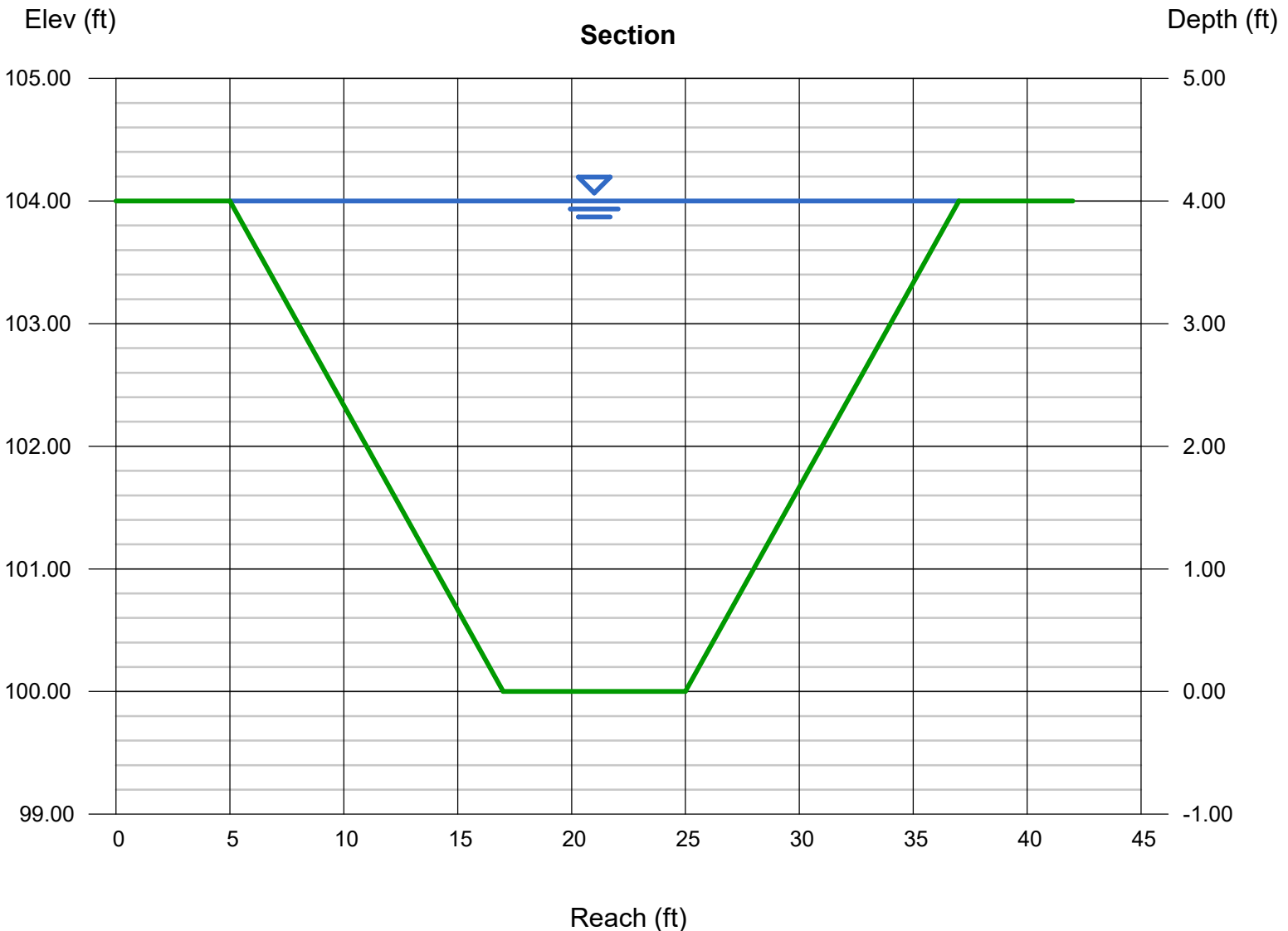
Bottom Width (ft) = 8.00  
Side Slopes (z:1) = 3.00, 3.00  
Total Depth (ft) = 4.00  
Invert Elev (ft) = 100.00  
Slope (%) = 0.99  
N-Value = 0.024

### Highlighted

Depth (ft) = 4.00  
Q (cfs) = 884.34  
Area (sqft) = 80.00  
Velocity (ft/s) = 11.05  
Wetted Perim (ft) = 33.30  
Crit Depth, Yc (ft) = 4.00  
Top Width (ft) = 32.00  
EGL (ft) = 5.90

### Calculations

Compute by: Q vs Depth  
No. Increments = 8



# Channel Report

## Section 12 Proposed

### Rectangular

Bottom Width (ft) = 10.00  
Total Depth (ft) = 5.75

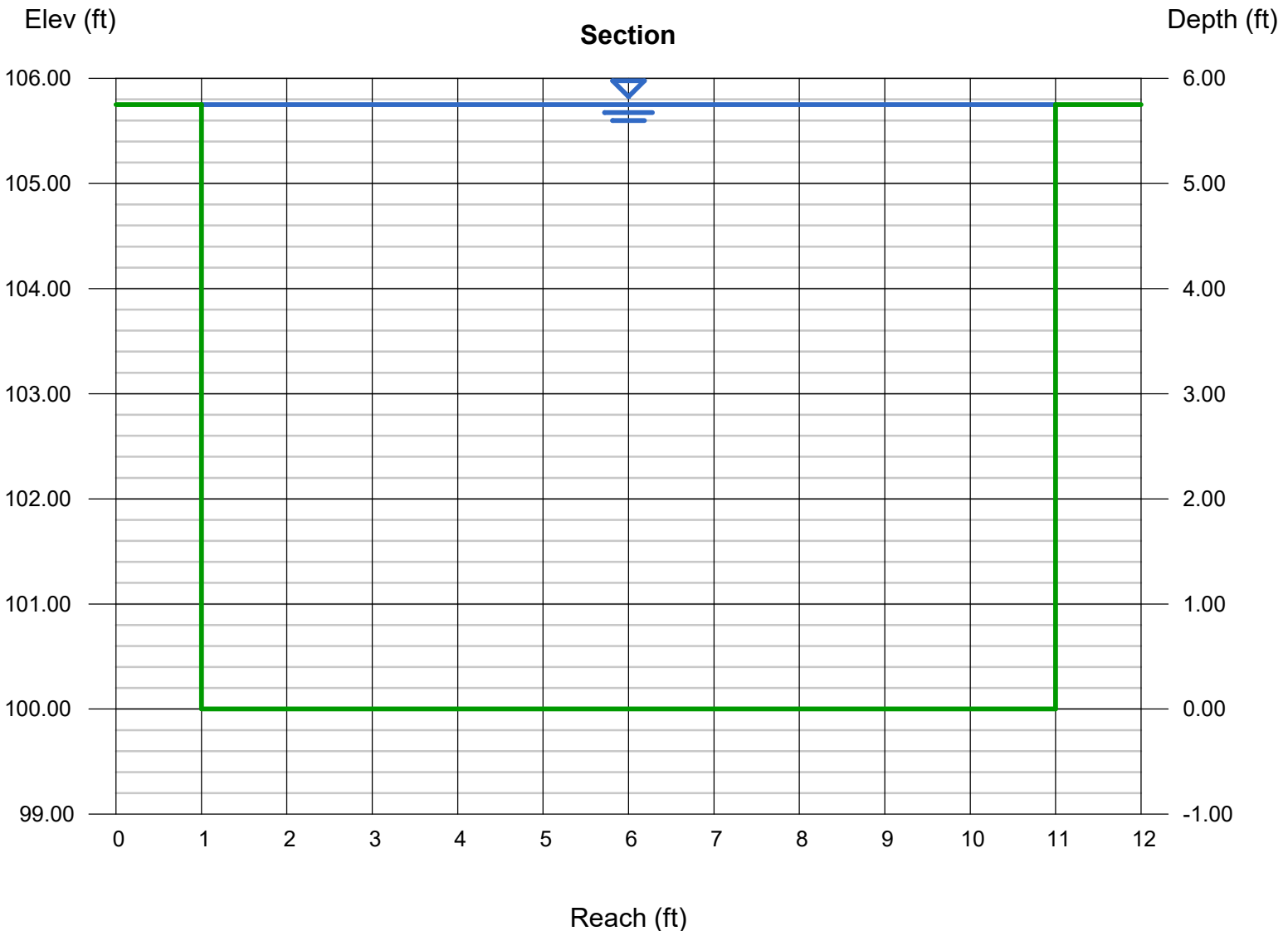
Invert Elev (ft) = 100.00  
Slope (%) = 0.92  
N-Value = 0.017

### Calculations

Compute by: Q vs Depth  
No. Increments = 1

### Highlighted

Depth (ft) = 5.75  
Q (cfs) = 929.17  
Area (sqft) = 57.50  
Velocity (ft/s) = 16.16  
Wetted Perim (ft) = 21.50  
Crit Depth, Yc (ft) = 5.75  
Top Width (ft) = 10.00  
EGL (ft) = 9.81



# Channel Report

## Section 14 Proposed

### Rectangular

Bottom Width (ft) = 14.00

Total Depth (ft) = 4.50

Invert Elev (ft) = 326.15

Slope (%) = 1.00

N-Value = 0.017

### Calculations

Compute by: Q vs Depth

No. Increments = 1

### Highlighted

Depth (ft) = 4.50

Q (cfs) = 1,078

Area (sqft) = 63.00

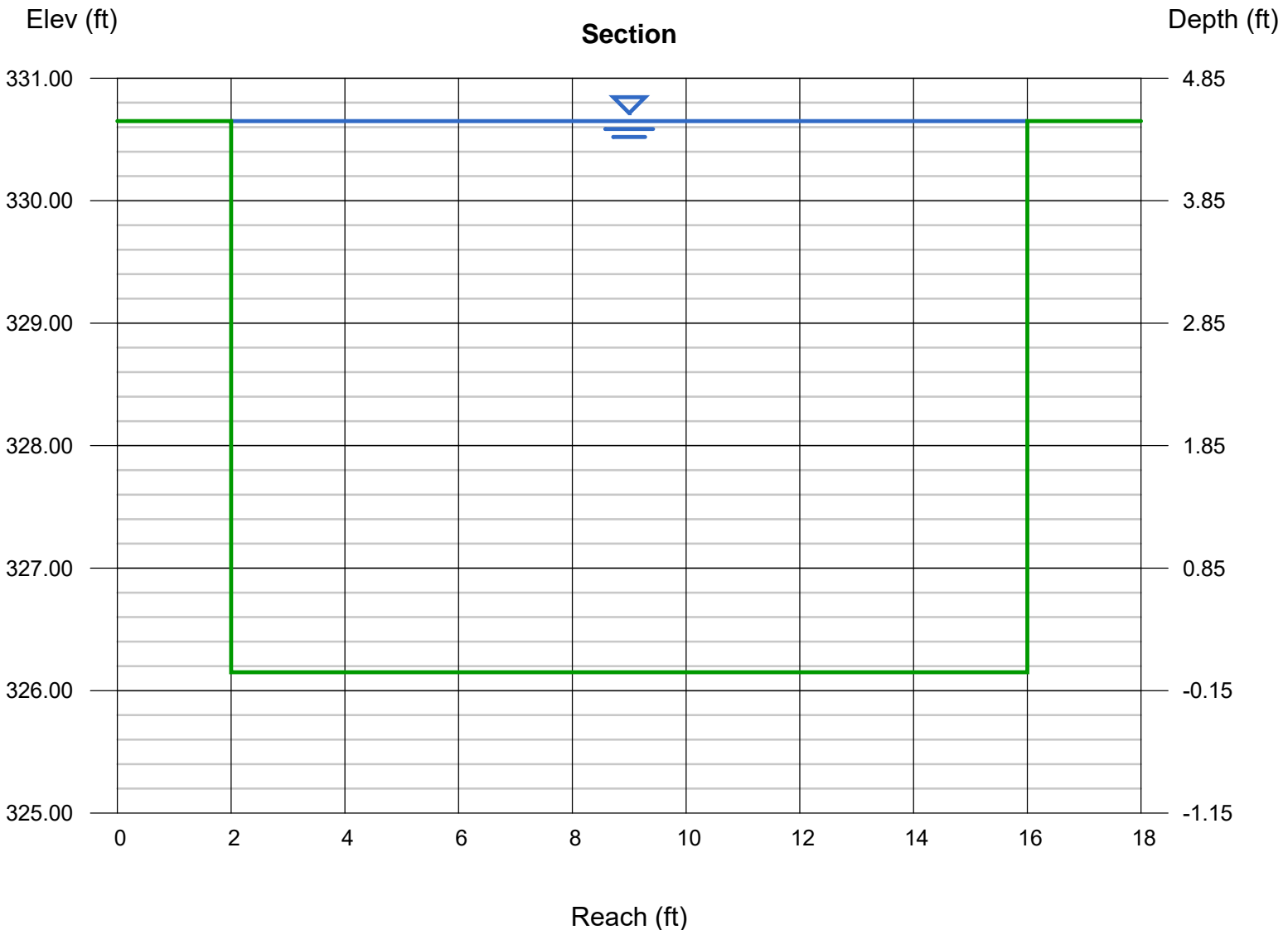
Velocity (ft/s) = 17.12

Wetted Perim (ft) = 23.00

Crit Depth, Yc (ft) = 4.50

Top Width (ft) = 14.00

EGL (ft) = 9.06



# Channel Report

## Section 15 Proposed

### Rectangular

Bottom Width (ft) = 14.00

Total Depth (ft) = 4.50

Invert Elev (ft) = 326.15

Slope (%) = 1.00

N-Value = 0.017

### Highlighted

Depth (ft) = 4.50

Q (cfs) = 1,078

Area (sqft) = 63.00

Velocity (ft/s) = 17.12

Wetted Perim (ft) = 23.00

Crit Depth, Yc (ft) = 4.50

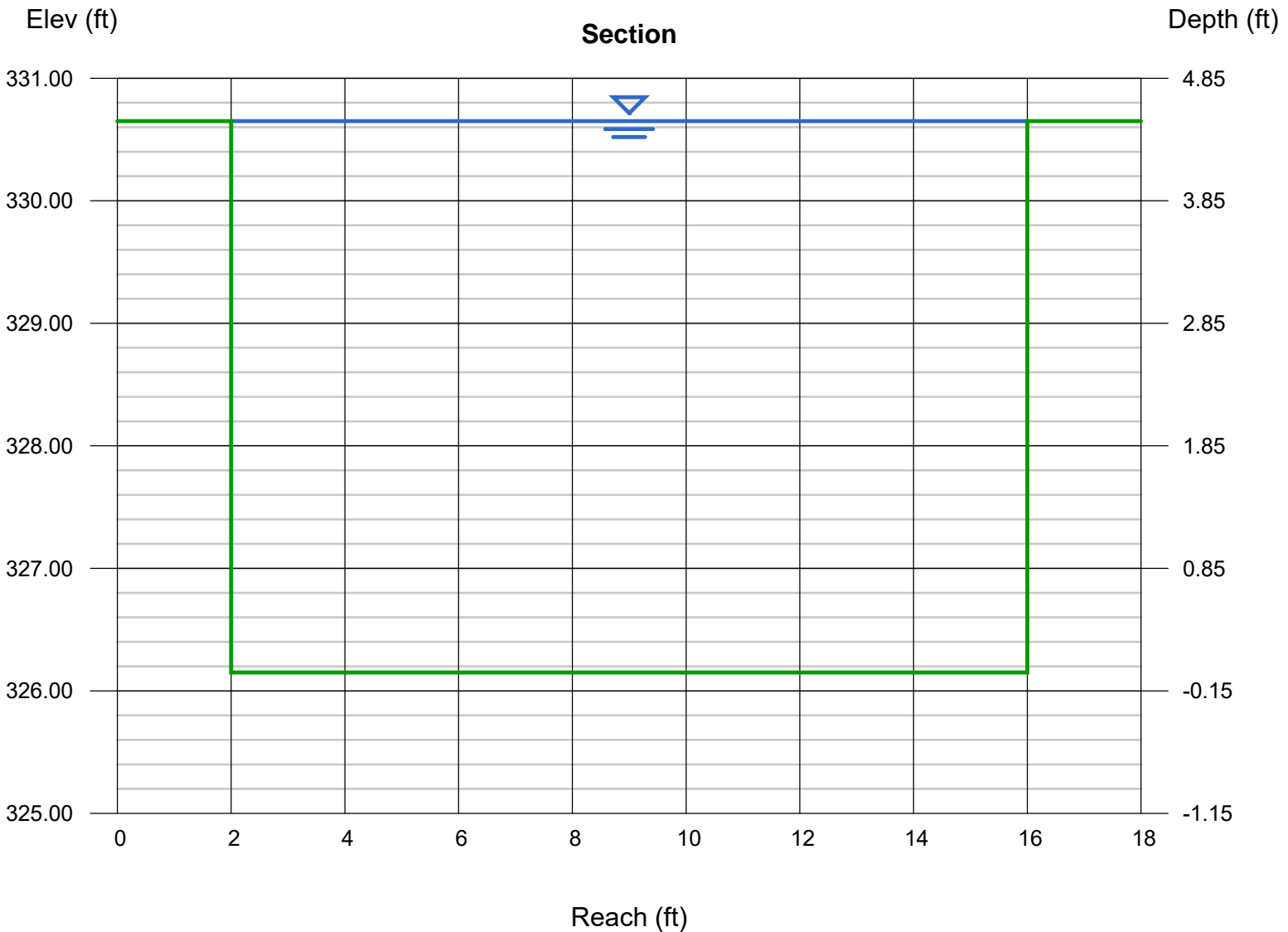
Top Width (ft) = 14.00

EGL (ft) = 9.06

### Calculations

Compute by: Q vs Depth

No. Increments = 1



## **APPENDIX D: DRAINAGE AREA MAPS**

# Louella Ave

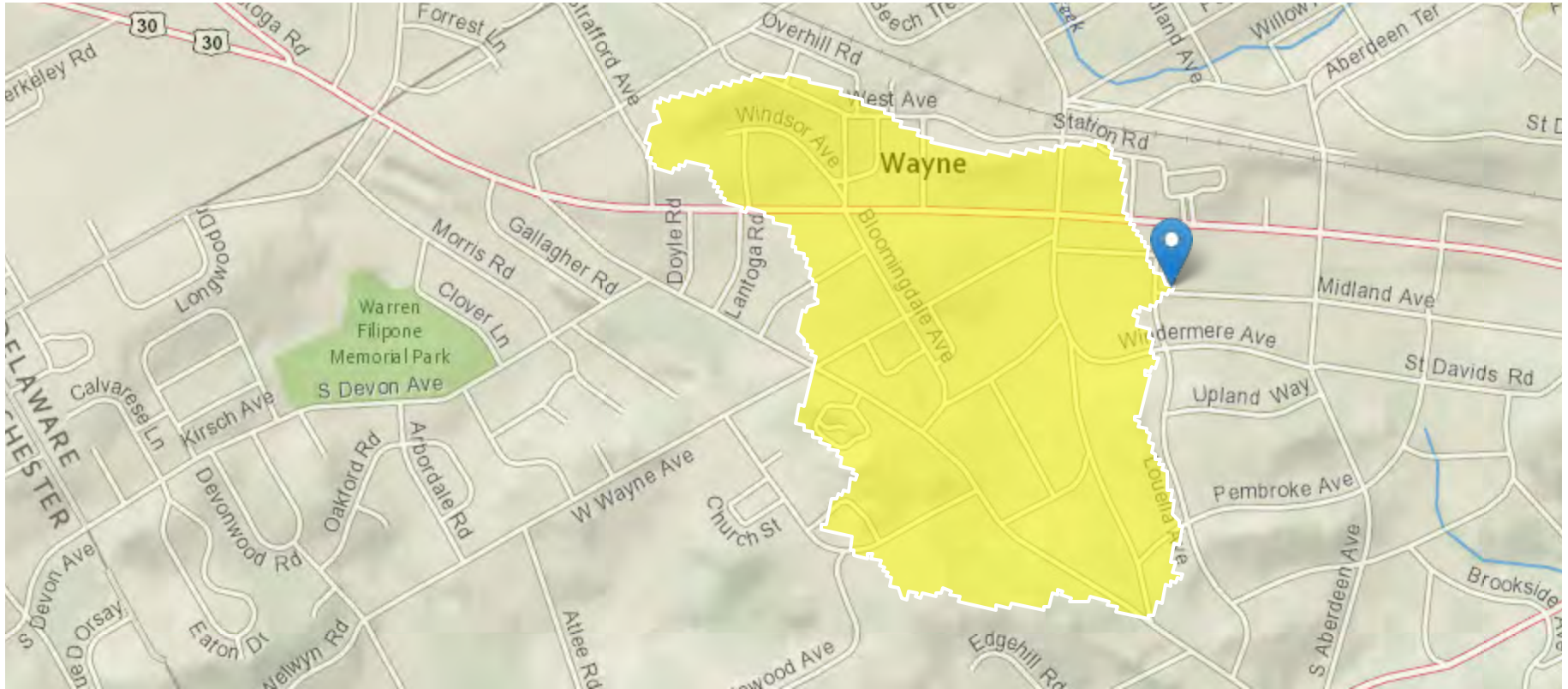
Region ID: PA

Workspace ID: PA20220408132014135000

Clicked Point (Latitude, Longitude): 40.04270, -75.38503

Time: 2022-04-08 09:20:33 -0400

**SECTION 1**



## Basin Characteristics

Parameter Code	Parameter Description	Value	Unit
----------------	-----------------------	-------	------

Parameter Code	Parameter Description	Value	Unit
CARBON	Percentage of area of carbonate rock	0	percent
DRNAREA	Area that drains to a point on a stream	0.3	square miles
FOREST	Percentage of area covered by forest	0.8068	percent
PRECIP	Mean Annual Precipitation	45	inches
URBAN	Percentage of basin with urban development	97.426	percent

### Peak-Flow Statistics Parameters [Peak Flow Region 4 SIR 2019 5094]

Parameter Code	Parameter Name	Value	Units	Min Limit	Max Limit
DRNAREA	Drainage Area	0.3	square miles	1.2	512
CARBON	Percent Carbonate	0	percent	0	68.5

### Peak-Flow Statistics Disclaimers [Peak Flow Region 4 SIR 2019 5094]

One or more of the parameters is outside the suggested range. Estimates were extrapolated with unknown errors.

### Peak-Flow Statistics Flow Report [Peak Flow Region 4 SIR 2019 5094]

Statistic	Value	Unit
50-percent AEP flood	98.6	ft <sup>3</sup> /s
20-percent AEP flood	181	ft <sup>3</sup> /s
10-percent AEP flood	252	ft <sup>3</sup> /s
4-percent AEP flood	358	ft <sup>3</sup> /s

<b>Statistic</b>	<b>Value</b>	<b>Unit</b>
2-percent AEP flood	449	ft <sup>3</sup> /s
1-percent AEP flood	548	ft <sup>3</sup> /s
0.5-percent AEP flood	657	ft <sup>3</sup> /s
0.2-percent AEP flood	820	ft <sup>3</sup> /s

*Peak-Flow Statistics Citations*

**Roland, M.A., and Stuckey, M.H.,2019, Development of regression equations for the estimation of flood flows at ungaged streams in Pennsylvania: U.S. Geological Survey Scientific Investigations Report 2019–5094, 36 p. ([https:// doi.org/10.3133 /sir20195094](https://doi.org/10.3133/sir20195094))**

### Base Flow Statistics Parameters [Statewide Mean and Base Flow]

<b>Parameter Code</b>	<b>Parameter Name</b>	<b>Value</b>	<b>Units</b>	<b>Min Limit</b>	<b>Max Limit</b>
DRNAREA	Drainage Area	0.3	square miles	2.26	1720
PRECIP	Mean Annual Precipitation	45	inches	33.1	50.4
CARBON	Percent Carbonate	0	percent	0	99
FOREST	Percent Forest	0.8068	percent	5.1	100
URBAN	Percent Urban	97.426	percent	0	89

### Base Flow Statistics Disclaimers [Statewide Mean and Base Flow]

One or more of the parameters is outside the suggested range. Estimates were extrapolated with unknown errors.

### Base Flow Statistics Flow Report [Statewide Mean and Base Flow]



<b>Statistic</b>	<b>Value</b>	<b>Unit</b>
Base Flow 10 Year Recurrence Interval	0.137	ft <sup>3</sup> /s
Base Flow 25 Year Recurrence Interval	0.122	ft <sup>3</sup> /s
Base Flow 50 Year Recurrence Interval	0.114	ft <sup>3</sup> /s

*Base Flow Statistics Citations*

**Stuckey, M.H.,2006, Low-flow, base-flow, and mean-flow regression equations for Pennsylvania streams: U.S. Geological Survey Scientific Investigations Report 2006-5130, 84 p. (<http://pubs.usgs.gov/sir/2006/5130/>)**

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Application Version: 4.8.1

StreamStats Services Version: 1.2.22

NSS Services Version: 2.1.2

# StreamStats Report

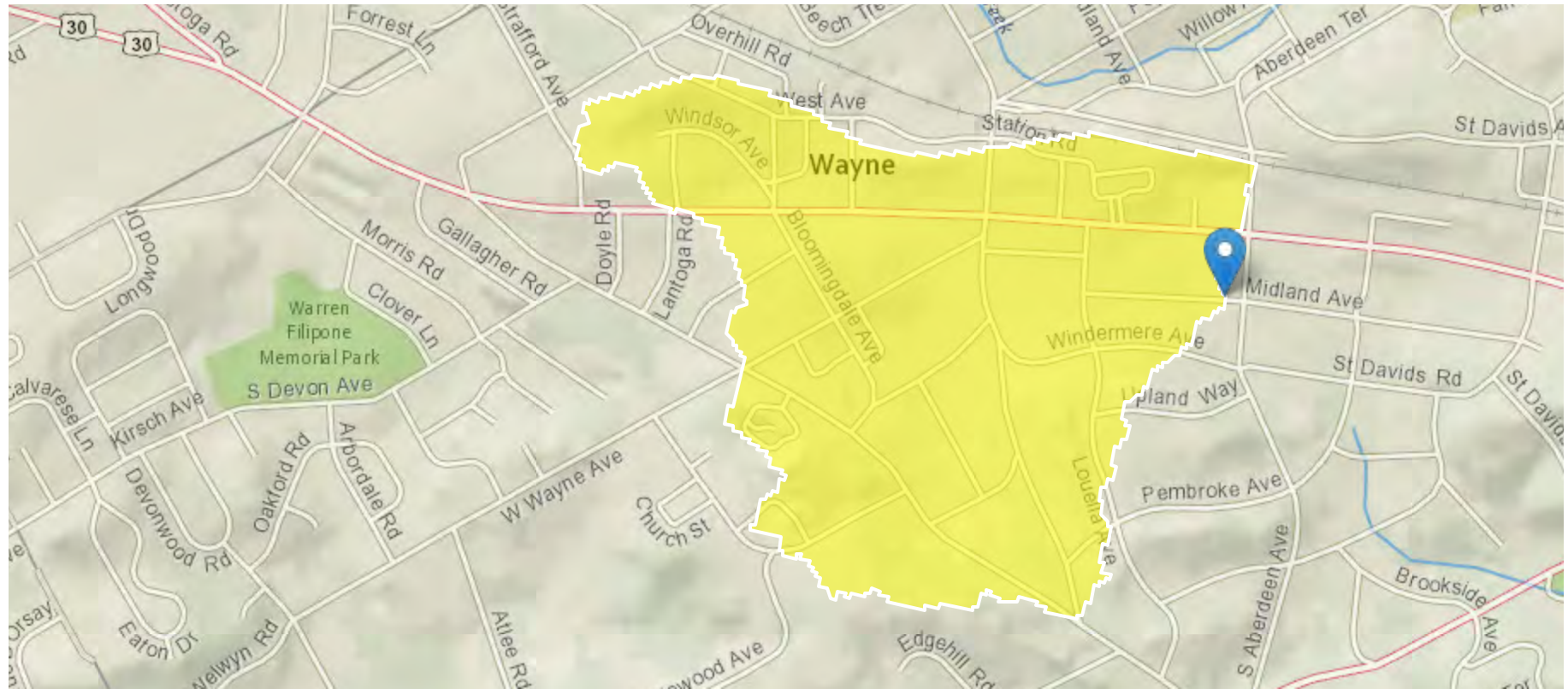
**Region ID:** PA

**Workspace ID:** PA20220421114051027000

**Clicked Point (Latitude, Longitude):** 40.04250, -75.38192

**Time:** 2022-04-21 07:41:10 -0400

**SECTION 2**



## Basin Characteristics

Parameter Code	Parameter Description	Value	Unit
----------------	-----------------------	-------	------

Parameter Code	Parameter Description	Value	Unit
CARBON	Percentage of area of carbonate rock	0	percent
DRNAREA	Area that drains to a point on a stream	0.37	square miles
FOREST	Percentage of area covered by forest	0.7453	percent
PRECIP	Mean Annual Precipitation	45	inches
URBAN	Percentage of basin with urban development	97.5365	percent

### Peak-Flow Statistics Parameters [Peak Flow Region 4 SIR 2019 5094]

Parameter Code	Parameter Name	Value	Units	Min Limit	Max Limit
DRNAREA	Drainage Area	0.37	square miles	1.2	512
CARBON	Percent Carbonate	0	percent	0	68.5

### Peak-Flow Statistics Disclaimers [Peak Flow Region 4 SIR 2019 5094]

One or more of the parameters is outside the suggested range. Estimates were extrapolated with unknown errors.

### Peak-Flow Statistics Flow Report [Peak Flow Region 4 SIR 2019 5094]

Statistic	Value	Unit
50-percent AEP flood	114	ft <sup>3</sup> /s
20-percent AEP flood	208	ft <sup>3</sup> /s
10-percent AEP flood	289	ft <sup>3</sup> /s
4-percent AEP flood	410	ft <sup>3</sup> /s

<b>Statistic</b>	<b>Value</b>	<b>Unit</b>
2-percent AEP flood	513	ft <sup>3</sup> /s
1-percent AEP flood	626	ft <sup>3</sup> /s
0.5-percent AEP flood	749	ft <sup>3</sup> /s
0.2-percent AEP flood	934	ft <sup>3</sup> /s

*Peak-Flow Statistics Citations*

**Roland, M.A., and Stuckey, M.H., 2019, Development of regression equations for the estimation of flood flows at ungaged streams in Pennsylvania: U.S. Geological Survey Scientific Investigations Report 2019–5094, 36 p. ([https:// doi.org/10.3133 /sir20195094](https://doi.org/10.3133/sir20195094))**

### Base Flow Statistics Parameters [Statewide Mean and Base Flow]

<b>Parameter Code</b>	<b>Parameter Name</b>	<b>Value</b>	<b>Units</b>	<b>Min Limit</b>	<b>Max Limit</b>
DRNAREA	Drainage Area	0.37	square miles	2.26	1720
PRECIP	Mean Annual Precipitation	45	inches	33.1	50.4
CARBON	Percent Carbonate	0	percent	0	99
FOREST	Percent Forest	0.7453	percent	5.1	100
URBAN	Percent Urban	97.5365	percent	0	89

### Base Flow Statistics Disclaimers [Statewide Mean and Base Flow]

One or more of the parameters is outside the suggested range. Estimates were extrapolated with unknown errors.

### Base Flow Statistics Flow Report [Statewide Mean and Base Flow]

<b>Statistic</b>	<b>Value</b>	<b>Unit</b>
Base Flow 10 Year Recurrence Interval	0.169	ft <sup>3</sup> /s
Base Flow 25 Year Recurrence Interval	0.15	ft <sup>3</sup> /s
Base Flow 50 Year Recurrence Interval	0.14	ft <sup>3</sup> /s

*Base Flow Statistics Citations*

**Stuckey, M.H.,2006, Low-flow, base-flow, and mean-flow regression equations for Pennsylvania streams: U.S. Geological Survey Scientific Investigations Report 2006-5130, 84 p. (<http://pubs.usgs.gov/sir/2006/5130/>)**

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Application Version: 4.8.1

StreamStats Services Version: 1.2.22

NSS Services Version: 2.1.2

## StreamStats Report

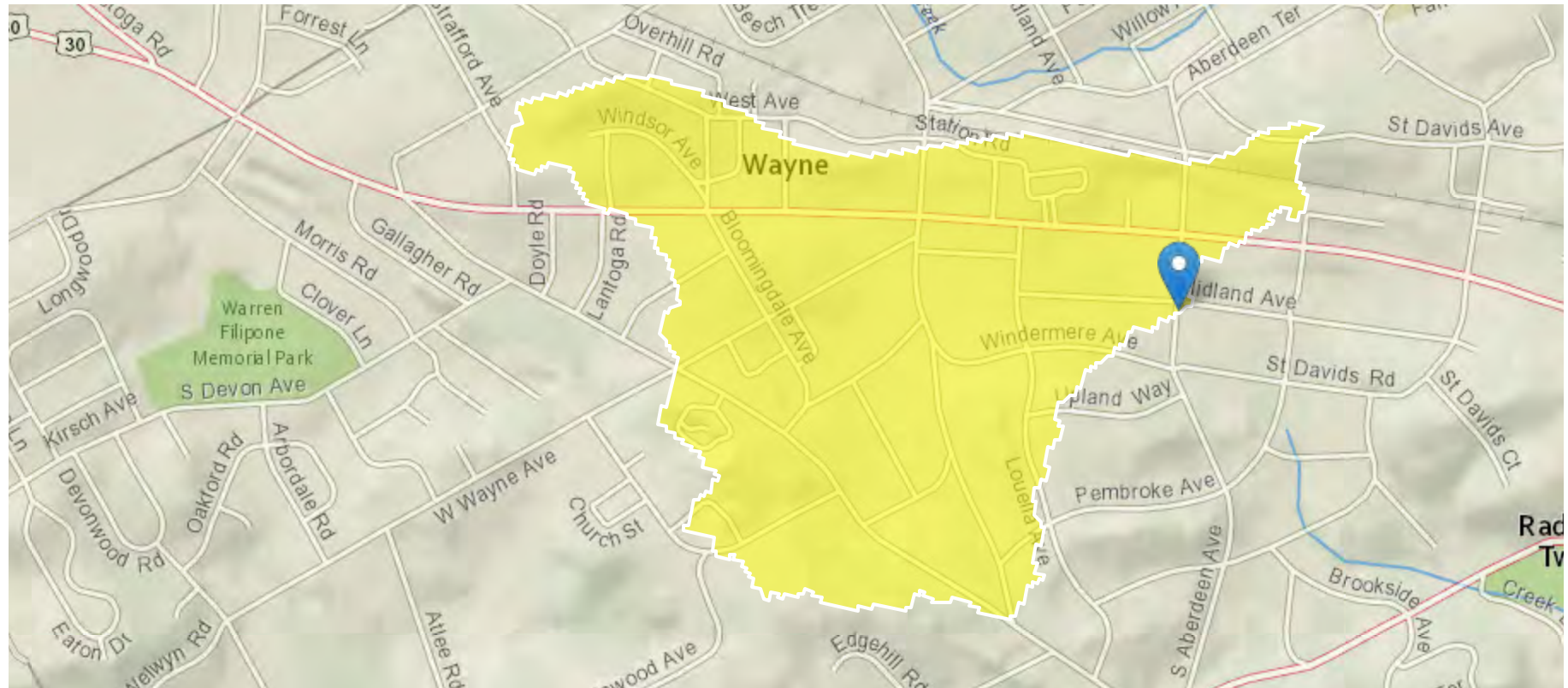
Region ID: PA

Workspace ID: PA20220421115131591000

Clicked Point (Latitude, Longitude): 40.04217, -75.38140

Time: 2022-04-21 07:51:51 -0400

**SECTION 3 & 4**



### Basin Characteristics

Parameter Code	Parameter Description	Value	Unit
----------------	-----------------------	-------	------

Parameter Code	Parameter Description	Value	Unit
CARBON	Percentage of area of carbonate rock	0	percent
DRNAREA	Area that drains to a point on a stream	0.4	square miles
FOREST	Percentage of area covered by forest	0.7858	percent
PRECIP	Mean Annual Precipitation	45	inches
URBAN	Percentage of basin with urban development	97.6038	percent

### Peak-Flow Statistics Parameters [Peak Flow Region 4 SIR 2019 5094]

Parameter Code	Parameter Name	Value	Units	Min Limit	Max Limit
DRNAREA	Drainage Area	0.4	square miles	1.2	512
CARBON	Percent Carbonate	0	percent	0	68.5

### Peak-Flow Statistics Disclaimers [Peak Flow Region 4 SIR 2019 5094]

One or more of the parameters is outside the suggested range. Estimates were extrapolated with unknown errors.

### Peak-Flow Statistics Flow Report [Peak Flow Region 4 SIR 2019 5094]

Statistic	Value	Unit
50-percent AEP flood	121	ft <sup>3</sup> /s
20-percent AEP flood	220	ft <sup>3</sup> /s
10-percent AEP flood	305	ft <sup>3</sup> /s
4-percent AEP flood	431	ft <sup>3</sup> /s

<b>Statistic</b>	<b>Value</b>	<b>Unit</b>
2-percent AEP flood	539	ft <sup>3</sup> /s
1-percent AEP flood	657	ft <sup>3</sup> /s
0.5-percent AEP flood	786	ft <sup>3</sup> /s
0.2-percent AEP flood	980	ft <sup>3</sup> /s

*Peak-Flow Statistics Citations*

**Roland, M.A., and Stuckey, M.H., 2019, Development of regression equations for the estimation of flood flows at ungaged streams in Pennsylvania: U.S. Geological Survey Scientific Investigations Report 2019–5094, 36 p. ([https:// doi.org/10.3133 /sir20195094](https://doi.org/10.3133/sir20195094))**

### Base Flow Statistics Parameters [Statewide Mean and Base Flow]

<b>Parameter Code</b>	<b>Parameter Name</b>	<b>Value</b>	<b>Units</b>	<b>Min Limit</b>	<b>Max Limit</b>
DRNAREA	Drainage Area	0.4	square miles	2.26	1720
PRECIP	Mean Annual Precipitation	45	inches	33.1	50.4
CARBON	Percent Carbonate	0	percent	0	99
FOREST	Percent Forest	0.7858	percent	5.1	100
URBAN	Percent Urban	97.6038	percent	0	89

### Base Flow Statistics Disclaimers [Statewide Mean and Base Flow]

One or more of the parameters is outside the suggested range. Estimates were extrapolated with unknown errors.

### Base Flow Statistics Flow Report [Statewide Mean and Base Flow]



<b>Statistic</b>	<b>Value</b>	<b>Unit</b>
Base Flow 10 Year Recurrence Interval	0.183	ft <sup>3</sup> /s
Base Flow 25 Year Recurrence Interval	0.163	ft <sup>3</sup> /s
Base Flow 50 Year Recurrence Interval	0.152	ft <sup>3</sup> /s

*Base Flow Statistics Citations*

**Stuckey, M.H., 2006, Low-flow, base-flow, and mean-flow regression equations for Pennsylvania streams: U.S. Geological Survey Scientific Investigations Report 2006-5130, 84 p. (<http://pubs.usgs.gov/sir/2006/5130/>)**

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Application Version: 4.8.1

StreamStats Services Version: 1.2.22

NSS Services Version: 2.1.2

## South Aberdeen

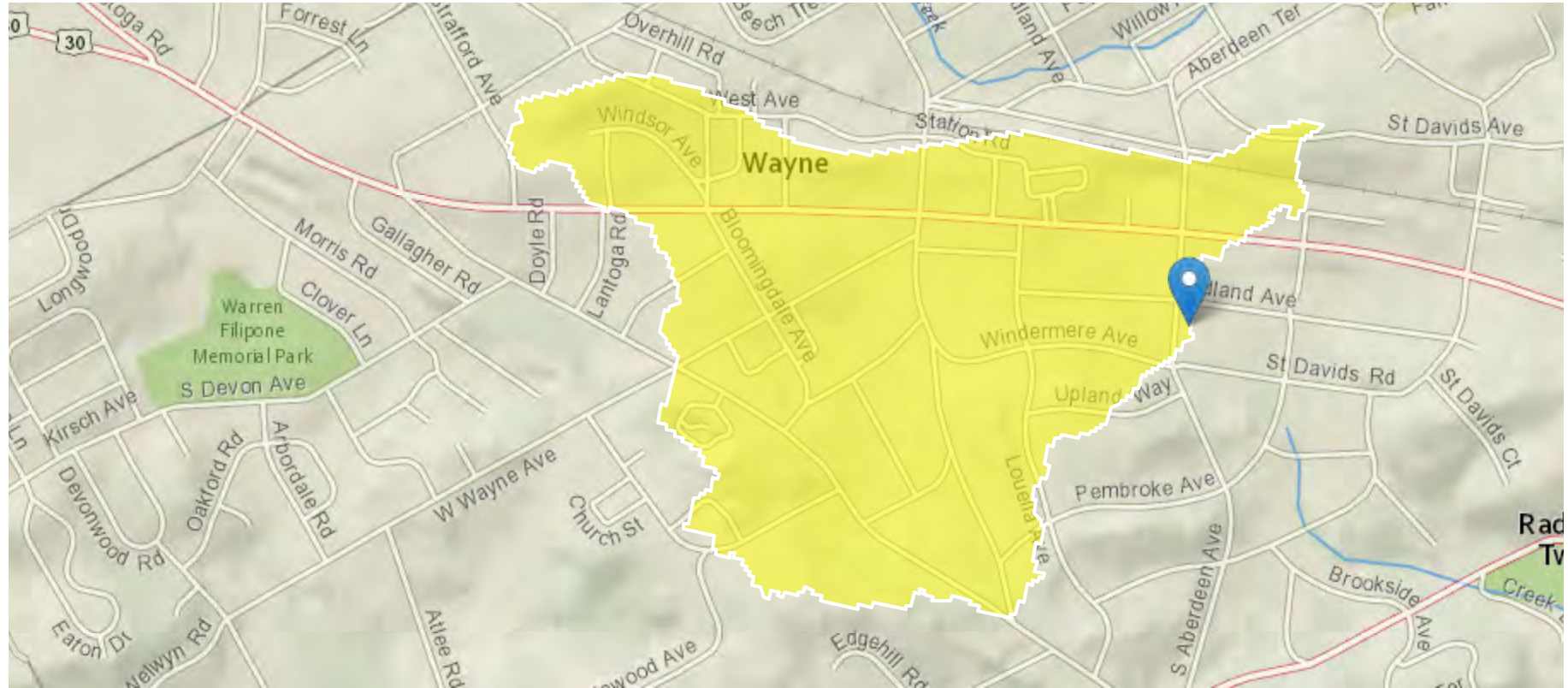
**Region ID:** PA

**Workspace ID:** PA20220408133756708000

**Clicked Point (Latitude, Longitude):** 40.04192, -75.38117

**Time:** 2022-04-08 09:38:17 -0400

**SECTION 5**



### Basin Characteristics

Parameter Code	Parameter Description	Value	Unit
----------------	-----------------------	-------	------

Parameter Code	Parameter Description	Value	Unit
CARBON	Percentage of area of carbonate rock	0	percent
DRNAREA	Area that drains to a point on a stream	0.41	square miles
FOREST	Percentage of area covered by forest	0.763	percent
PRECIP	Mean Annual Precipitation	45	inches
URBAN	Percentage of basin with urban development	97.6733	percent

### Peak-Flow Statistics Parameters [Peak Flow Region 4 SIR 2019 5094]

Parameter Code	Parameter Name	Value	Units	Min Limit	Max Limit
DRNAREA	Drainage Area	0.41	square miles	1.2	512
CARBON	Percent Carbonate	0	percent	0	68.5

### Peak-Flow Statistics Disclaimers [Peak Flow Region 4 SIR 2019 5094]

One or more of the parameters is outside the suggested range. Estimates were extrapolated with unknown errors.

### Peak-Flow Statistics Flow Report [Peak Flow Region 4 SIR 2019 5094]

Statistic	Value	Unit
50-percent AEP flood	123	ft <sup>3</sup> /s
20-percent AEP flood	223	ft <sup>3</sup> /s
10-percent AEP flood	310	ft <sup>3</sup> /s
4-percent AEP flood	438	ft <sup>3</sup> /s

<b>Statistic</b>	<b>Value</b>	<b>Unit</b>
2-percent AEP flood	547	ft <sup>3</sup> /s
1-percent AEP flood	668	ft <sup>3</sup> /s
0.5-percent AEP flood	799	ft <sup>3</sup> /s
0.2-percent AEP flood	995	ft <sup>3</sup> /s

*Peak-Flow Statistics Citations*

**Roland, M.A., and Stuckey, M.H., 2019, Development of regression equations for the estimation of flood flows at ungaged streams in Pennsylvania: U.S. Geological Survey Scientific Investigations Report 2019–5094, 36 p. ([https:// doi.org/10.3133 /sir20195094](https://doi.org/10.3133/sir20195094))**

### Base Flow Statistics Parameters [Statewide Mean and Base Flow]

<b>Parameter Code</b>	<b>Parameter Name</b>	<b>Value</b>	<b>Units</b>	<b>Min Limit</b>	<b>Max Limit</b>
DRNAREA	Drainage Area	0.41	square miles	2.26	1720
PRECIP	Mean Annual Precipitation	45	inches	33.1	50.4
CARBON	Percent Carbonate	0	percent	0	99
FOREST	Percent Forest	0.763	percent	5.1	100
URBAN	Percent Urban	97.6733	percent	0	89

### Base Flow Statistics Disclaimers [Statewide Mean and Base Flow]

One or more of the parameters is outside the suggested range. Estimates were extrapolated with unknown errors.

### Base Flow Statistics Flow Report [Statewide Mean and Base Flow]

<b>Statistic</b>	<b>Value</b>	<b>Unit</b>
Base Flow 10 Year Recurrence Interval	0.188	ft <sup>3</sup> /s
Base Flow 25 Year Recurrence Interval	0.167	ft <sup>3</sup> /s
Base Flow 50 Year Recurrence Interval	0.155	ft <sup>3</sup> /s

*Base Flow Statistics Citations*

**Stuckey, M.H.,2006, Low-flow, base-flow, and mean-flow regression equations for Pennsylvania streams: U.S. Geological Survey Scientific Investigations Report 2006-5130, 84 p. (<http://pubs.usgs.gov/sir/2006/5130/>)**

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Application Version: 4.8.1

StreamStats Services Version: 1.2.22

NSS Services Version: 2.1.2

# StreamStats Report

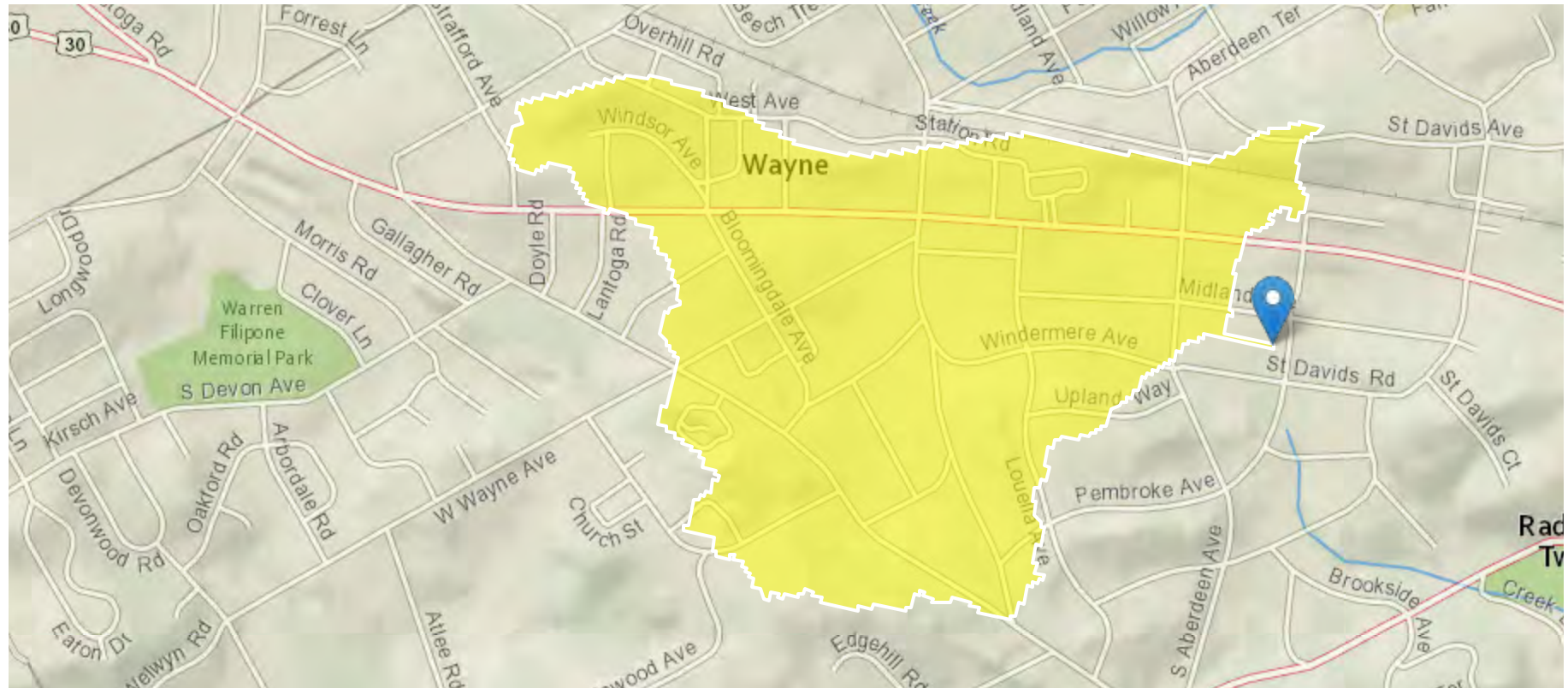
**Region ID:** PA

**Workspace ID:** PA20220421120419748000

**Clicked Point (Latitude, Longitude):** 40.04160, -75.37902

**Time:** 2022-04-21 08:04:46 -0400

**SECTION 6**



## Basin Characteristics

Parameter Code	Parameter Description	Value	Unit
----------------	-----------------------	-------	------

Parameter Code	Parameter Description	Value	Unit
CARBON	Percentage of area of carbonate rock	0	percent
DRNAREA	Area that drains to a point on a stream	0.42	square miles
FOREST	Percentage of area covered by forest	0.9185	percent
PRECIP	Mean Annual Precipitation	45	inches
URBAN	Percentage of basin with urban development	97.3838	percent

### Peak-Flow Statistics Parameters [Peak Flow Region 4 SIR 2019 5094]

Parameter Code	Parameter Name	Value	Units	Min Limit	Max Limit
DRNAREA	Drainage Area	0.42	square miles	1.2	512
CARBON	Percent Carbonate	0	percent	0	68.5

### Peak-Flow Statistics Disclaimers [Peak Flow Region 4 SIR 2019 5094]

One or more of the parameters is outside the suggested range. Estimates were extrapolated with unknown errors.

### Peak-Flow Statistics Flow Report [Peak Flow Region 4 SIR 2019 5094]

Statistic	Value	Unit
50-percent AEP flood	125	ft <sup>3</sup> /s
20-percent AEP flood	227	ft <sup>3</sup> /s
10-percent AEP flood	315	ft <sup>3</sup> /s
4-percent AEP flood	445	ft <sup>3</sup> /s

<b>Statistic</b>	<b>Value</b>	<b>Unit</b>
2-percent AEP flood	556	ft <sup>3</sup> /s
1-percent AEP flood	678	ft <sup>3</sup> /s
0.5-percent AEP flood	811	ft <sup>3</sup> /s
0.2-percent AEP flood	1010	ft <sup>3</sup> /s

*Peak-Flow Statistics Citations*

**Roland, M.A., and Stuckey, M.H., 2019, Development of regression equations for the estimation of flood flows at ungaged streams in Pennsylvania: U.S. Geological Survey Scientific Investigations Report 2019–5094, 36 p. ([https:// doi.org/10.3133 /sir20195094](https://doi.org/10.3133/sir20195094))**

### Base Flow Statistics Parameters [Statewide Mean and Base Flow]

<b>Parameter Code</b>	<b>Parameter Name</b>	<b>Value</b>	<b>Units</b>	<b>Min Limit</b>	<b>Max Limit</b>
DRNAREA	Drainage Area	0.42	square miles	2.26	1720
PRECIP	Mean Annual Precipitation	45	inches	33.1	50.4
CARBON	Percent Carbonate	0	percent	0	99
FOREST	Percent Forest	0.9185	percent	5.1	100
URBAN	Percent Urban	97.3838	percent	0	89

### Base Flow Statistics Disclaimers [Statewide Mean and Base Flow]

One or more of the parameters is outside the suggested range. Estimates were extrapolated with unknown errors.

### Base Flow Statistics Flow Report [Statewide Mean and Base Flow]



<b>Statistic</b>	<b>Value</b>	<b>Unit</b>
Base Flow 10 Year Recurrence Interval	0.192	ft <sup>3</sup> /s
Base Flow 25 Year Recurrence Interval	0.171	ft <sup>3</sup> /s
Base Flow 50 Year Recurrence Interval	0.159	ft <sup>3</sup> /s

*Base Flow Statistics Citations*

**Stuckey, M.H., 2006, Low-flow, base-flow, and mean-flow regression equations for Pennsylvania streams: U.S. Geological Survey Scientific Investigations Report 2006-5130, 84 p. (<http://pubs.usgs.gov/sir/2006/5130/>)**

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Application Version: 4.8.1

StreamStats Services Version: 1.2.22

NSS Services Version: 2.1.2

## StreamStats Report

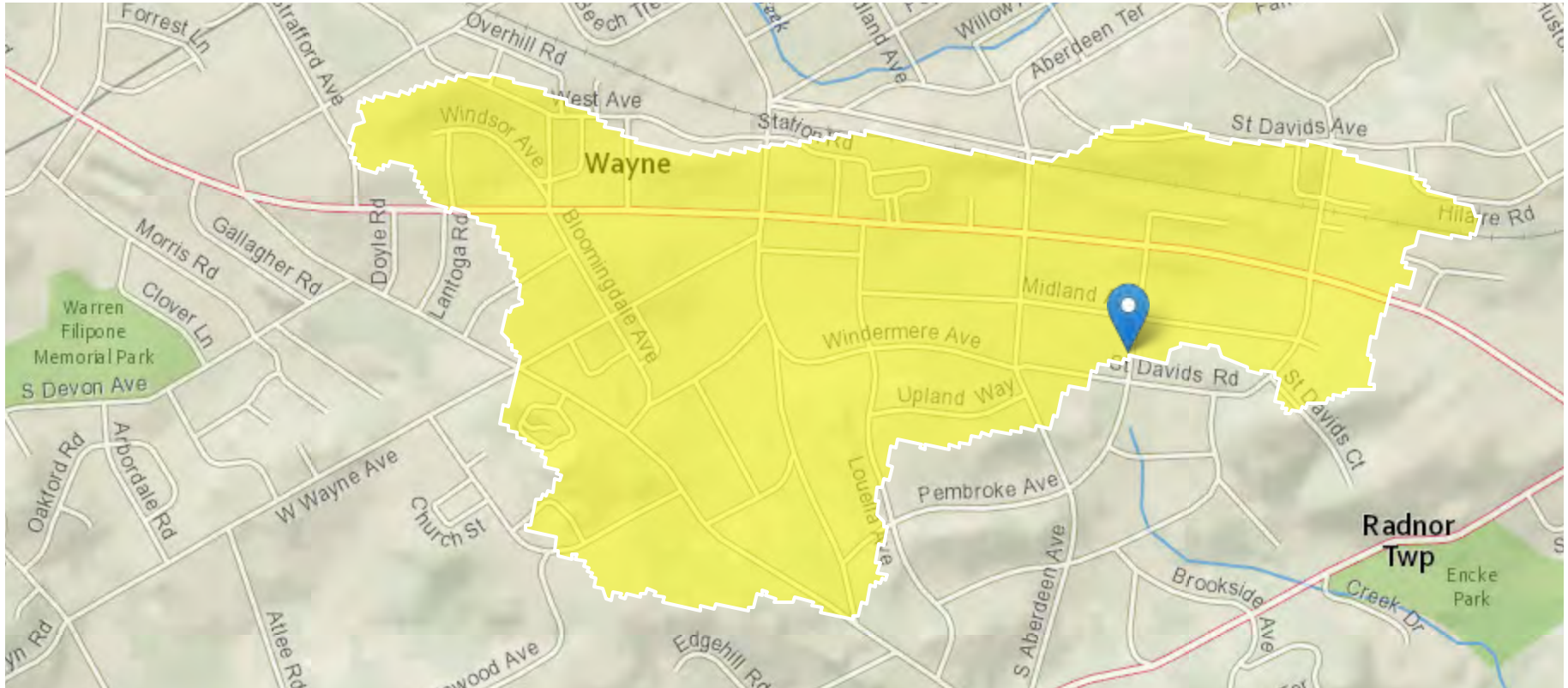
**Region ID:** PA

**Workspace ID:** PA20220421122115687000

**Clicked Point (Latitude, Longitude):** 40.04148, -75.37874

**Time:** 2022-04-21 08:21:39 -0400

**SECTION 7 & 8**



### Basin Characteristics

Parameter Code	Parameter Description	Value	Unit
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Parameter Code	Parameter Description	Value	Unit
CARBON	Percentage of area of carbonate rock	0	percent
DRNAREA	Area that drains to a point on a stream	0.56	square miles
FOREST	Percentage of area covered by forest	1.8149	percent
PRECIP	Mean Annual Precipitation	45	inches
URBAN	Percentage of basin with urban development	96.3424	percent

### Peak-Flow Statistics Parameters [Peak Flow Region 4 SIR 2019 5094]

Parameter Code	Parameter Name	Value	Units	Min Limit	Max Limit
DRNAREA	Drainage Area	0.56	square miles	1.2	512
CARBON	Percent Carbonate	0	percent	0	68.5

### Peak-Flow Statistics Disclaimers [Peak Flow Region 4 SIR 2019 5094]

One or more of the parameters is outside the suggested range. Estimates were extrapolated with unknown errors.

### Peak-Flow Statistics Flow Report [Peak Flow Region 4 SIR 2019 5094]

Statistic	Value	Unit
50-percent AEP flood	153	ft <sup>3</sup> /s
20-percent AEP flood	275	ft <sup>3</sup> /s
10-percent AEP flood	380	ft <sup>3</sup> /s
4-percent AEP flood	536	ft <sup>3</sup> /s

<b>Statistic</b>	<b>Value</b>	<b>Unit</b>
2-percent AEP flood	668	ft <sup>3</sup> /s
1-percent AEP flood	813	ft <sup>3</sup> /s
0.5-percent AEP flood	971	ft <sup>3</sup> /s
0.2-percent AEP flood	1210	ft <sup>3</sup> /s

*Peak-Flow Statistics Citations*

**Roland, M.A., and Stuckey, M.H.,2019, Development of regression equations for the estimation of flood flows at ungaged streams in Pennsylvania: U.S. Geological Survey Scientific Investigations Report 2019–5094, 36 p. ([https:// doi.org/10.3133 /sir20195094](https://doi.org/10.3133/sir20195094))**

### Base Flow Statistics Parameters [Statewide Mean and Base Flow]

<b>Parameter Code</b>	<b>Parameter Name</b>	<b>Value</b>	<b>Units</b>	<b>Min Limit</b>	<b>Max Limit</b>
DRNAREA	Drainage Area	0.56	square miles	2.26	1720
PRECIP	Mean Annual Precipitation	45	inches	33.1	50.4
CARBON	Percent Carbonate	0	percent	0	99
FOREST	Percent Forest	1.8149	percent	5.1	100
URBAN	Percent Urban	96.3424	percent	0	89

### Base Flow Statistics Disclaimers [Statewide Mean and Base Flow]

One or more of the parameters is outside the suggested range. Estimates were extrapolated with unknown errors.

### Base Flow Statistics Flow Report [Statewide Mean and Base Flow]

<b>Statistic</b>	<b>Value</b>	<b>Unit</b>
Base Flow 10 Year Recurrence Interval	0.259	ft <sup>3</sup> /s
Base Flow 25 Year Recurrence Interval	0.23	ft <sup>3</sup> /s
Base Flow 50 Year Recurrence Interval	0.215	ft <sup>3</sup> /s

*Base Flow Statistics Citations*

**Stuckey, M.H.,2006, Low-flow, base-flow, and mean-flow regression equations for Pennsylvania streams: U.S. Geological Survey Scientific Investigations Report 2006-5130, 84 p. (<http://pubs.usgs.gov/sir/2006/5130/>)**

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Application Version: 4.8.1

StreamStats Services Version: 1.2.22

NSS Services Version: 2.1.2

# Meadowbrook Avenue

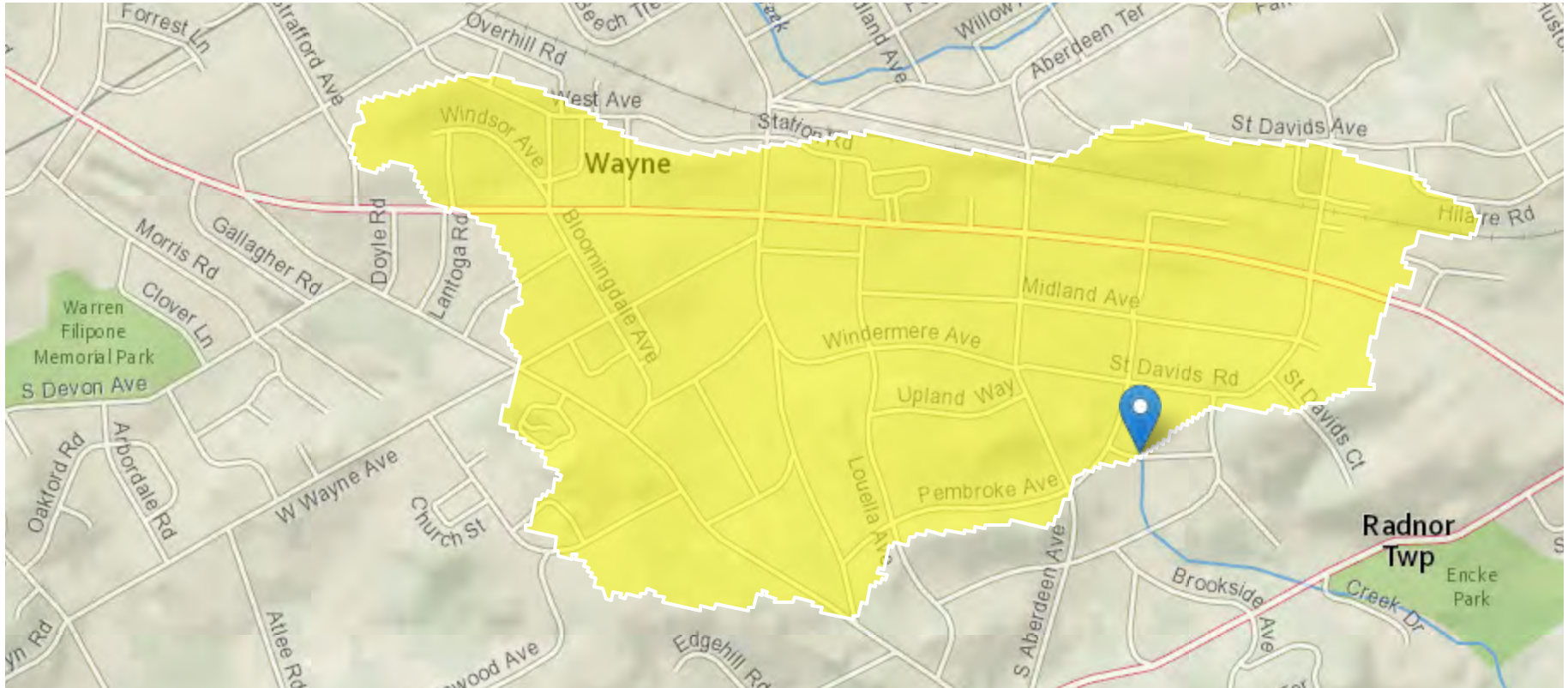
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**Workspace ID:** PA20220408134617690000

**Clicked Point (Latitude, Longitude):** 40.03948, -75.37846

**Time:** 2022-04-08 09:46:37 -0400

**SECTION 9**



## Basin Characteristics

Parameter Code	Parameter Description	Value	Unit
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Parameter Code	Parameter Description	Value	Unit
CARBON	Percentage of area of carbonate rock	0	percent
DRNAREA	Area that drains to a point on a stream	0.61	square miles
FOREST	Percentage of area covered by forest	1.643	percent
PRECIP	Mean Annual Precipitation	45	inches
URBAN	Percentage of basin with urban development	96.6889	percent

### Peak-Flow Statistics Parameters [Peak Flow Region 4 SIR 2019 5094]

Parameter Code	Parameter Name	Value	Units	Min Limit	Max Limit
DRNAREA	Drainage Area	0.61	square miles	1.2	512
CARBON	Percent Carbonate	0	percent	0	68.5

### Peak-Flow Statistics Disclaimers [Peak Flow Region 4 SIR 2019 5094]

One or more of the parameters is outside the suggested range. Estimates were extrapolated with unknown errors.

### Peak-Flow Statistics Flow Report [Peak Flow Region 4 SIR 2019 5094]

Statistic	Value	Unit
50-percent AEP flood	162	ft <sup>3</sup> /s
20-percent AEP flood	292	ft <sup>3</sup> /s
10-percent AEP flood	402	ft <sup>3</sup> /s
4-percent AEP flood	566	ft <sup>3</sup> /s

<b>Statistic</b>	<b>Value</b>	<b>Unit</b>
2-percent AEP flood	705	ft <sup>3</sup> /s
1-percent AEP flood	858	ft <sup>3</sup> /s
0.5-percent AEP flood	1020	ft <sup>3</sup> /s
0.2-percent AEP flood	1270	ft <sup>3</sup> /s

*Peak-Flow Statistics Citations*

**Roland, M.A., and Stuckey, M.H., 2019, Development of regression equations for the estimation of flood flows at ungaged streams in Pennsylvania: U.S. Geological Survey Scientific Investigations Report 2019–5094, 36 p. ([https:// doi.org/10.3133 /sir20195094](https://doi.org/10.3133/sir20195094))**

### Base Flow Statistics Parameters [Statewide Mean and Base Flow]

<b>Parameter Code</b>	<b>Parameter Name</b>	<b>Value</b>	<b>Units</b>	<b>Min Limit</b>	<b>Max Limit</b>
DRNAREA	Drainage Area	0.61	square miles	2.26	1720
PRECIP	Mean Annual Precipitation	45	inches	33.1	50.4
CARBON	Percent Carbonate	0	percent	0	99
FOREST	Percent Forest	1.643	percent	5.1	100
URBAN	Percent Urban	96.6889	percent	0	89

### Base Flow Statistics Disclaimers [Statewide Mean and Base Flow]

One or more of the parameters is outside the suggested range. Estimates were extrapolated with unknown errors.

### Base Flow Statistics Flow Report [Statewide Mean and Base Flow]



<b>Statistic</b>	<b>Value</b>	<b>Unit</b>
Base Flow 10 Year Recurrence Interval	0.282	ft <sup>3</sup> /s
Base Flow 25 Year Recurrence Interval	0.251	ft <sup>3</sup> /s
Base Flow 50 Year Recurrence Interval	0.234	ft <sup>3</sup> /s

*Base Flow Statistics Citations*

**Stuckey, M.H., 2006, Low-flow, base-flow, and mean-flow regression equations for Pennsylvania streams: U.S. Geological Survey Scientific Investigations Report 2006-5130, 84 p. (<http://pubs.usgs.gov/sir/2006/5130/>)**

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Application Version: 4.8.1

StreamStats Services Version: 1.2.22

NSS Services Version: 2.1.2

## StreamStats Report

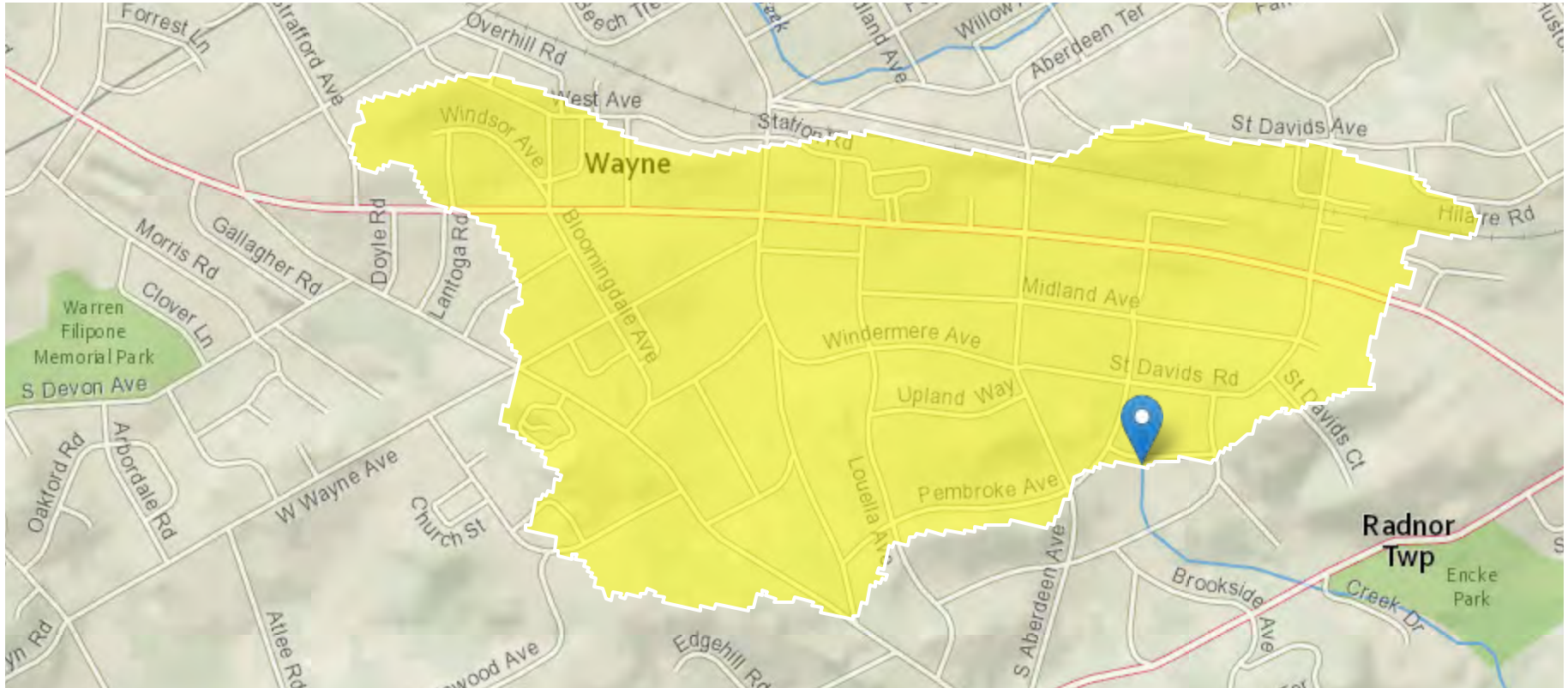
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**Workspace ID:** PA20220421122557678000

**Clicked Point (Latitude, Longitude):** 40.03928, -75.37838

**Time:** 2022-04-21 08:26:17 -0400

**SECTION 10**



### Basin Characteristics

Parameter Code	Parameter Description	Value	Unit
----------------	-----------------------	-------	------

Parameter Code	Parameter Description	Value	Unit
CARBON	Percentage of area of carbonate rock	0	percent
DRNAREA	Area that drains to a point on a stream	0.62	square miles
FOREST	Percentage of area covered by forest	1.6241	percent
PRECIP	Mean Annual Precipitation	45	inches
URBAN	Percentage of basin with urban development	96.7268	percent

### Peak-Flow Statistics Parameters [Peak Flow Region 4 SIR 2019 5094]

Parameter Code	Parameter Name	Value	Units	Min Limit	Max Limit
DRNAREA	Drainage Area	0.62	square miles	1.2	512
CARBON	Percent Carbonate	0	percent	0	68.5

### Peak-Flow Statistics Disclaimers [Peak Flow Region 4 SIR 2019 5094]

One or more of the parameters is outside the suggested range. Estimates were extrapolated with unknown errors.

### Peak-Flow Statistics Flow Report [Peak Flow Region 4 SIR 2019 5094]

Statistic	Value	Unit
50-percent AEP flood	164	ft <sup>3</sup> /s
20-percent AEP flood	295	ft <sup>3</sup> /s
10-percent AEP flood	406	ft <sup>3</sup> /s
4-percent AEP flood	572	ft <sup>3</sup> /s

<b>Statistic</b>	<b>Value</b>	<b>Unit</b>
2-percent AEP flood	712	ft <sup>3</sup> /s
1-percent AEP flood	867	ft <sup>3</sup> /s
0.5-percent AEP flood	1030	ft <sup>3</sup> /s
0.2-percent AEP flood	1290	ft <sup>3</sup> /s

*Peak-Flow Statistics Citations*

**Roland, M.A., and Stuckey, M.H., 2019, Development of regression equations for the estimation of flood flows at ungaged streams in Pennsylvania: U.S. Geological Survey Scientific Investigations Report 2019–5094, 36 p. ([https:// doi.org/10.3133 /sir20195094](https://doi.org/10.3133/sir20195094))**

### Base Flow Statistics Parameters [Statewide Mean and Base Flow]

<b>Parameter Code</b>	<b>Parameter Name</b>	<b>Value</b>	<b>Units</b>	<b>Min Limit</b>	<b>Max Limit</b>
DRNAREA	Drainage Area	0.62	square miles	2.26	1720
PRECIP	Mean Annual Precipitation	45	inches	33.1	50.4
CARBON	Percent Carbonate	0	percent	0	99
FOREST	Percent Forest	1.6241	percent	5.1	100
URBAN	Percent Urban	96.7268	percent	0	89

### Base Flow Statistics Disclaimers [Statewide Mean and Base Flow]

One or more of the parameters is outside the suggested range. Estimates were extrapolated with unknown errors.

### Base Flow Statistics Flow Report [Statewide Mean and Base Flow]

<b>Statistic</b>	<b>Value</b>	<b>Unit</b>
Base Flow 10 Year Recurrence Interval	0.286	ft <sup>3</sup> /s
Base Flow 25 Year Recurrence Interval	0.255	ft <sup>3</sup> /s
Base Flow 50 Year Recurrence Interval	0.237	ft <sup>3</sup> /s

*Base Flow Statistics Citations*

**Stuckey, M.H., 2006, Low-flow, base-flow, and mean-flow regression equations for Pennsylvania streams: U.S. Geological Survey Scientific Investigations Report 2006-5130, 84 p. (<http://pubs.usgs.gov/sir/2006/5130/>)**

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Application Version: 4.8.1

StreamStats Services Version: 1.2.22

NSS Services Version: 2.1.2

## StreamStats Report

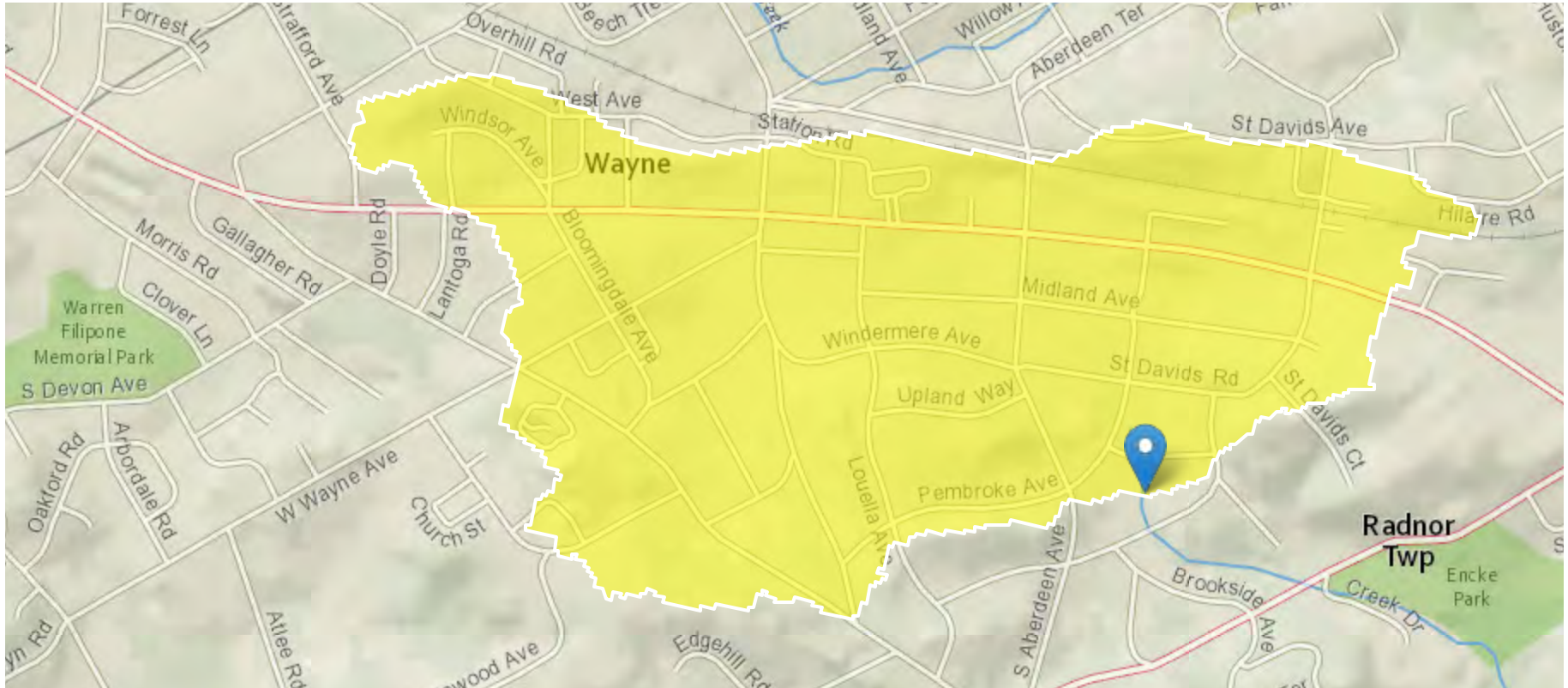
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**Workspace ID:** PA20220421131051758000

**Clicked Point (Latitude, Longitude):** 40.03867, -75.37827

**Time:** 2022-04-21 09:11:19 -0400

**SECTION 11**



### Basin Characteristics

Parameter Code	Parameter Description	Value	Unit
----------------	-----------------------	-------	------

Parameter Code	Parameter Description	Value	Unit
CARBON	Percentage of area of carbonate rock	0	percent
DRNAREA	Area that drains to a point on a stream	0.63	square miles
FOREST	Percentage of area covered by forest	1.6062	percent
PRECIP	Mean Annual Precipitation	45	inches
URBAN	Percentage of basin with urban development	96.7631	percent

### Peak-Flow Statistics Parameters [Peak Flow Region 4 SIR 2019 5094]

Parameter Code	Parameter Name	Value	Units	Min Limit	Max Limit
DRNAREA	Drainage Area	0.63	square miles	1.2	512
CARBON	Percent Carbonate	0	percent	0	68.5

### Peak-Flow Statistics Disclaimers [Peak Flow Region 4 SIR 2019 5094]

One or more of the parameters is outside the suggested range. Estimates were extrapolated with unknown errors.

### Peak-Flow Statistics Flow Report [Peak Flow Region 4 SIR 2019 5094]

Statistic	Value	Unit
50-percent AEP flood	166	ft <sup>3</sup> /s
20-percent AEP flood	298	ft <sup>3</sup> /s
10-percent AEP flood	411	ft <sup>3</sup> /s
4-percent AEP flood	578	ft <sup>3</sup> /s

<b>Statistic</b>	<b>Value</b>	<b>Unit</b>
2-percent AEP flood	720	ft <sup>3</sup> /s
1-percent AEP flood	875	ft <sup>3</sup> /s
0.5-percent AEP flood	1050	ft <sup>3</sup> /s
0.2-percent AEP flood	1300	ft <sup>3</sup> /s

*Peak-Flow Statistics Citations*

**Roland, M.A., and Stuckey, M.H., 2019, Development of regression equations for the estimation of flood flows at ungaged streams in Pennsylvania: U.S. Geological Survey Scientific Investigations Report 2019–5094, 36 p. ([https:// doi.org/10.3133 /sir20195094](https://doi.org/10.3133/sir20195094))**

### Base Flow Statistics Parameters [Statewide Mean and Base Flow]

<b>Parameter Code</b>	<b>Parameter Name</b>	<b>Value</b>	<b>Units</b>	<b>Min Limit</b>	<b>Max Limit</b>
DRNAREA	Drainage Area	0.63	square miles	2.26	1720
PRECIP	Mean Annual Precipitation	45	inches	33.1	50.4
CARBON	Percent Carbonate	0	percent	0	99
FOREST	Percent Forest	1.6062	percent	5.1	100
URBAN	Percent Urban	96.7631	percent	0	89

### Base Flow Statistics Disclaimers [Statewide Mean and Base Flow]

One or more of the parameters is outside the suggested range. Estimates were extrapolated with unknown errors.

### Base Flow Statistics Flow Report [Statewide Mean and Base Flow]



<b>Statistic</b>	<b>Value</b>	<b>Unit</b>
Base Flow 10 Year Recurrence Interval	0.291	ft <sup>3</sup> /s
Base Flow 25 Year Recurrence Interval	0.259	ft <sup>3</sup> /s
Base Flow 50 Year Recurrence Interval	0.241	ft <sup>3</sup> /s

*Base Flow Statistics Citations*

**Stuckey, M.H.,2006, Low-flow, base-flow, and mean-flow regression equations for Pennsylvania streams: U.S. Geological Survey Scientific Investigations Report 2006-5130, 84 p. (<http://pubs.usgs.gov/sir/2006/5130/>)**

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Application Version: 4.8.1

StreamStats Services Version: 1.2.22

NSS Services Version: 2.1.2

## StreamStats Report

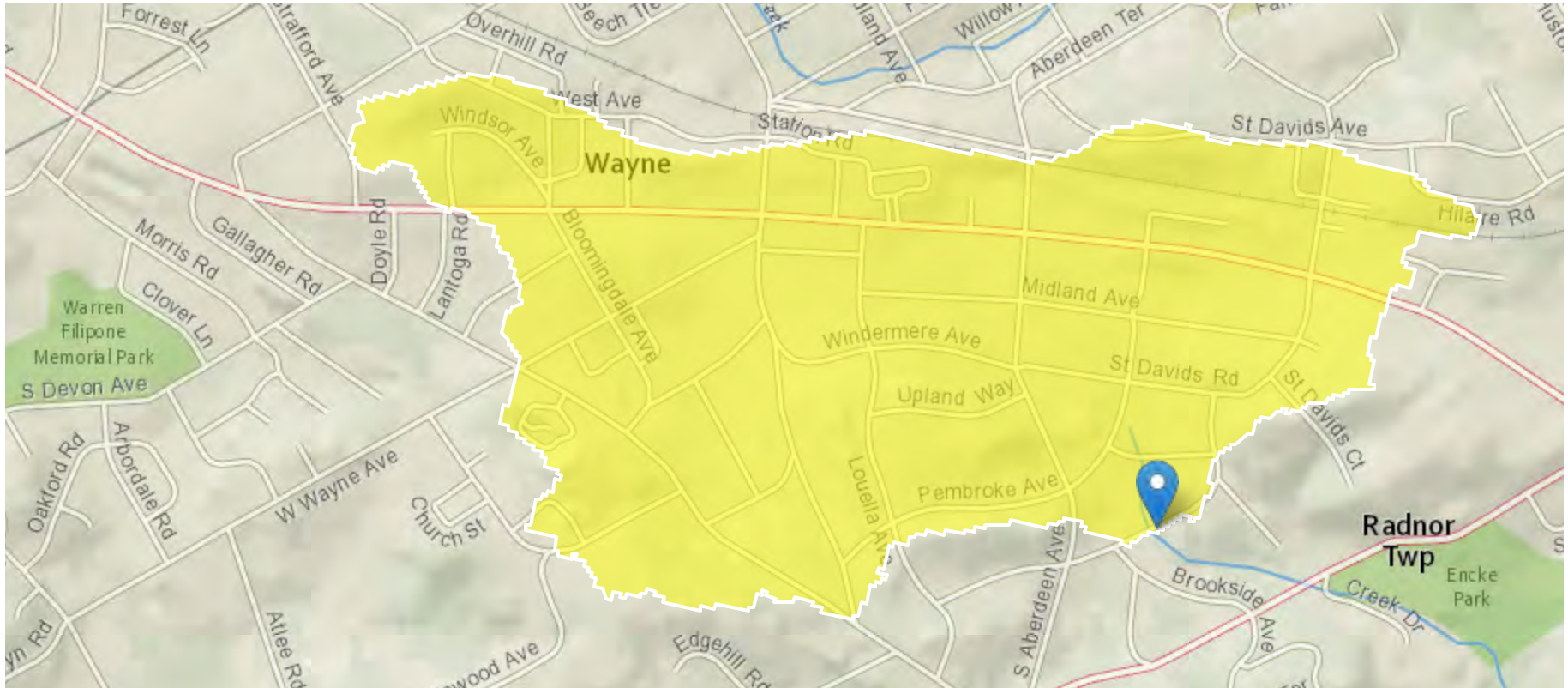
**Region ID:** PA

**Workspace ID:** PA20220421131528718000

**Clicked Point (Latitude, Longitude):** 40.03801, -75.37810

**Time:** 2022-04-21 09:15:58 -0400

**SECTION 12**



### Basin Characteristics

Parameter Code	Parameter Description	Value	Unit
----------------	-----------------------	-------	------

Parameter Code	Parameter Description	Value	Unit
CARBON	Percentage of area of carbonate rock	0	percent
DRNAREA	Area that drains to a point on a stream	0.64	square miles
FOREST	Percentage of area covered by forest	1.5837	percent
PRECIP	Mean Annual Precipitation	45	inches
URBAN	Percentage of basin with urban development	96.8083	percent

### Peak-Flow Statistics Parameters [Peak Flow Region 4 SIR 2019 5094]

Parameter Code	Parameter Name	Value	Units	Min Limit	Max Limit
DRNAREA	Drainage Area	0.64	square miles	1.2	512
CARBON	Percent Carbonate	0	percent	0	68.5

### Peak-Flow Statistics Disclaimers [Peak Flow Region 4 SIR 2019 5094]

One or more of the parameters is outside the suggested range. Estimates were extrapolated with unknown errors.

### Peak-Flow Statistics Flow Report [Peak Flow Region 4 SIR 2019 5094]

Statistic	Value	Unit
50-percent AEP flood	168	ft <sup>3</sup> /s
20-percent AEP flood	301	ft <sup>3</sup> /s
10-percent AEP flood	415	ft <sup>3</sup> /s
4-percent AEP flood	584	ft <sup>3</sup> /s

<b>Statistic</b>	<b>Value</b>	<b>Unit</b>
2-percent AEP flood	727	ft <sup>3</sup> /s
1-percent AEP flood	884	ft <sup>3</sup> /s
0.5-percent AEP flood	1060	ft <sup>3</sup> /s
0.2-percent AEP flood	1310	ft <sup>3</sup> /s

*Peak-Flow Statistics Citations*

**Roland, M.A., and Stuckey, M.H., 2019, Development of regression equations for the estimation of flood flows at ungaged streams in Pennsylvania: U.S. Geological Survey Scientific Investigations Report 2019–5094, 36 p. ([https:// doi.org/10.3133 /sir20195094](https://doi.org/10.3133/sir20195094))**

### Base Flow Statistics Parameters [Statewide Mean and Base Flow]

<b>Parameter Code</b>	<b>Parameter Name</b>	<b>Value</b>	<b>Units</b>	<b>Min Limit</b>	<b>Max Limit</b>
DRNAREA	Drainage Area	0.64	square miles	2.26	1720
PRECIP	Mean Annual Precipitation	45	inches	33.1	50.4
CARBON	Percent Carbonate	0	percent	0	99
FOREST	Percent Forest	1.5837	percent	5.1	100
URBAN	Percent Urban	96.8083	percent	0	89

### Base Flow Statistics Disclaimers [Statewide Mean and Base Flow]

One or more of the parameters is outside the suggested range. Estimates were extrapolated with unknown errors.

### Base Flow Statistics Flow Report [Statewide Mean and Base Flow]

<b>Statistic</b>	<b>Value</b>	<b>Unit</b>
Base Flow 10 Year Recurrence Interval	0.296	ft <sup>3</sup> /s
Base Flow 25 Year Recurrence Interval	0.263	ft <sup>3</sup> /s
Base Flow 50 Year Recurrence Interval	0.245	ft <sup>3</sup> /s

*Base Flow Statistics Citations*

**Stuckey, M.H.,2006, Low-flow, base-flow, and mean-flow regression equations for Pennsylvania streams: U.S. Geological Survey Scientific Investigations Report 2006-5130, 84 p. (<http://pubs.usgs.gov/sir/2006/5130/>)**

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Application Version: 4.8.1

StreamStats Services Version: 1.2.22

NSS Services Version: 2.1.2

## StreamStats Report

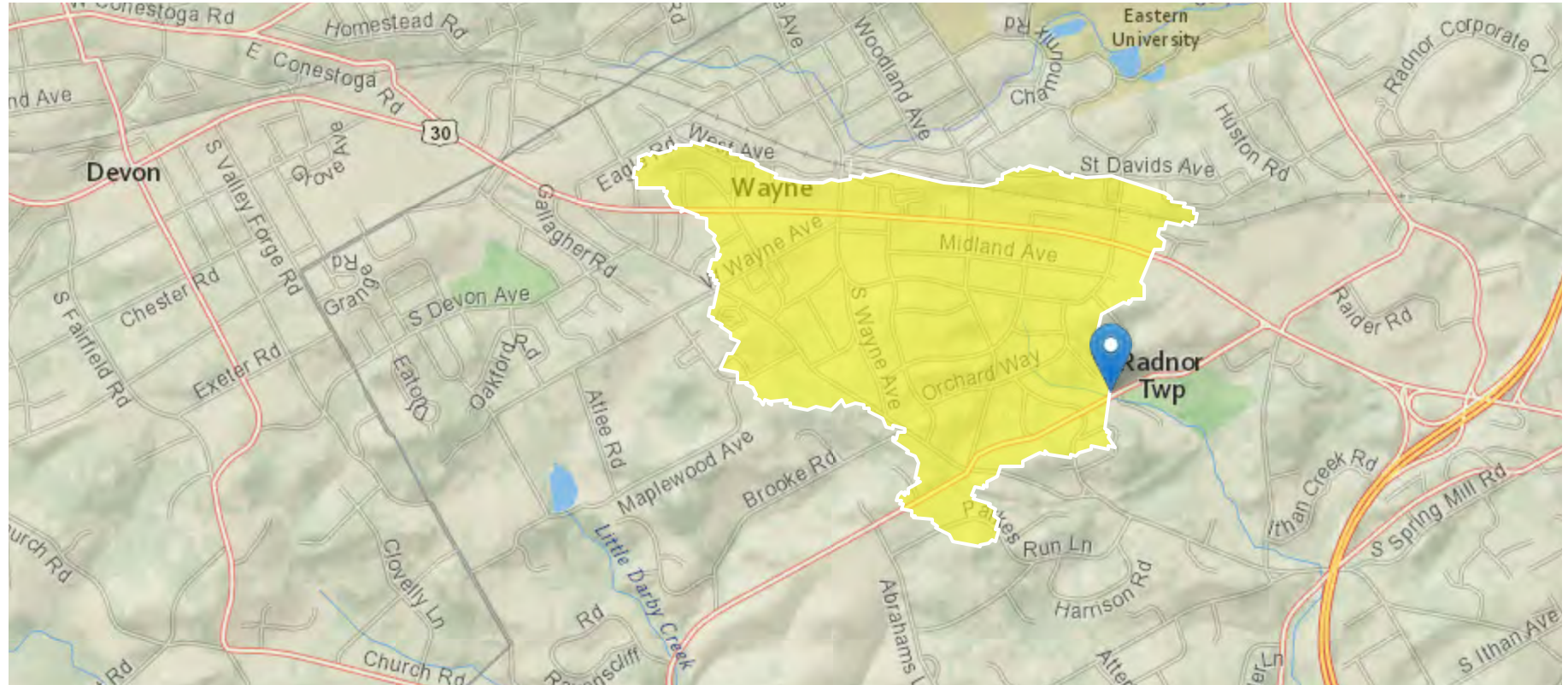
Region ID: PA

Workspace ID: PA20220421131929315000

Clicked Point (Latitude, Longitude): 40.03716, -75.37434

Time: 2022-04-21 09:19:58 -0400

**SECTION 13,14,15**



### Basin Characteristics

Parameter Code	Parameter Description	Value	Unit
----------------	-----------------------	-------	------

Parameter Code	Parameter Description	Value	Unit
CARBON	Percentage of area of carbonate rock	0	percent
DRNAREA	Area that drains to a point on a stream	0.83	square miles
FOREST	Percentage of area covered by forest	1.2205	percent
PRECIP	Mean Annual Precipitation	45	inches
URBAN	Percentage of basin with urban development	97.4841	percent

### Peak-Flow Statistics Parameters [Peak Flow Region 4 SIR 2019 5094]

Parameter Code	Parameter Name	Value	Units	Min Limit	Max Limit
DRNAREA	Drainage Area	0.83	square miles	1.2	512
CARBON	Percent Carbonate	0	percent	0	68.5

### Peak-Flow Statistics Disclaimers [Peak Flow Region 4 SIR 2019 5094]

One or more of the parameters is outside the suggested range. Estimates were extrapolated with unknown errors.

### Peak-Flow Statistics Flow Report [Peak Flow Region 4 SIR 2019 5094]

Statistic	Value	Unit
50-percent AEP flood	201	ft <sup>3</sup> /s
20-percent AEP flood	359	ft <sup>3</sup> /s
10-percent AEP flood	493	ft <sup>3</sup> /s
4-percent AEP flood	691	ft <sup>3</sup> /s

<b>Statistic</b>	<b>Value</b>	<b>Unit</b>
2-percent AEP flood	858	ft <sup>3</sup> /s
1-percent AEP flood	1040	ft <sup>3</sup> /s
0.5-percent AEP flood	1240	ft <sup>3</sup> /s
0.2-percent AEP flood	1540	ft <sup>3</sup> /s

*Peak-Flow Statistics Citations*

**Roland, M.A., and Stuckey, M.H., 2019, Development of regression equations for the estimation of flood flows at ungaged streams in Pennsylvania: U.S. Geological Survey Scientific Investigations Report 2019–5094, 36 p. ([https:// doi.org/10.3133 /sir20195094](https://doi.org/10.3133/sir20195094))**

### Base Flow Statistics Parameters [Statewide Mean and Base Flow]

<b>Parameter Code</b>	<b>Parameter Name</b>	<b>Value</b>	<b>Units</b>	<b>Min Limit</b>	<b>Max Limit</b>
DRNAREA	Drainage Area	0.83	square miles	2.26	1720
PRECIP	Mean Annual Precipitation	45	inches	33.1	50.4
CARBON	Percent Carbonate	0	percent	0	99
FOREST	Percent Forest	1.2205	percent	5.1	100
URBAN	Percent Urban	97.4841	percent	0	89

### Base Flow Statistics Disclaimers [Statewide Mean and Base Flow]

One or more of the parameters is outside the suggested range. Estimates were extrapolated with unknown errors.

### Base Flow Statistics Flow Report [Statewide Mean and Base Flow]



<b>Statistic</b>	<b>Value</b>	<b>Unit</b>
Base Flow 10 Year Recurrence Interval	0.382	ft <sup>3</sup> /s
Base Flow 25 Year Recurrence Interval	0.34	ft <sup>3</sup> /s
Base Flow 50 Year Recurrence Interval	0.317	ft <sup>3</sup> /s

*Base Flow Statistics Citations*

**Stuckey, M.H.,2006, Low-flow, base-flow, and mean-flow regression equations for Pennsylvania streams: U.S. Geological Survey Scientific Investigations Report 2006-5130, 84 p. (<http://pubs.usgs.gov/sir/2006/5130/>)**

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Application Version: 4.8.1

StreamStats Services Version: 1.2.22

NSS Services Version: 2.1.2

## **APPENDIX E: RAINFALL DATA**



**NOAA Atlas 14, Volume 2, Version 3**  
**Location name: Wayne, Pennsylvania, USA\***  
**Latitude: 40.0409°, Longitude: -75.3788°**  
**Elevation: 351.26 ft\*\***



\* source: ESRI Maps  
 \*\* source: USGS

**POINT PRECIPITATION FREQUENCY ESTIMATES**

G.M. Bonnin, D. Martin, B. Lin, T. Parzybok, M.Yekta, and D. Riley

NOAA, National Weather Service, Silver Spring, Maryland

[PF\\_tabular](#) | [PF\\_graphical](#) | [Maps\\_&\\_aerials](#)

**PF tabular**

<b>PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches/hour)<sup>1</sup></b>										
<b>Duration</b>	<b>Average recurrence interval (years)</b>									
	<b>1</b>	<b>2</b>	<b>5</b>	<b>10</b>	<b>25</b>	<b>50</b>	<b>100</b>	<b>200</b>	<b>500</b>	<b>1000</b>
<b>5-min</b>	<b>4.18</b> (3.84-4.55)	<b>4.97</b> (4.57-5.41)	<b>5.83</b> (5.34-6.34)	<b>6.43</b> (5.89-7.00)	<b>7.14</b> (6.50-7.76)	<b>7.62</b> (6.90-8.29)	<b>8.09</b> (7.30-8.82)	<b>8.50</b> (7.62-9.29)	<b>8.95</b> (7.97-9.83)	<b>9.30</b> (8.21-10.2)
<b>10-min</b>	<b>3.34</b> (3.07-3.63)	<b>3.98</b> (3.66-4.33)	<b>4.67</b> (4.28-5.08)	<b>5.14</b> (4.71-5.59)	<b>5.69</b> (5.18-6.19)	<b>6.07</b> (5.50-6.60)	<b>6.43</b> (5.80-7.00)	<b>6.73</b> (6.04-7.36)	<b>7.09</b> (6.30-7.78)	<b>7.32</b> (6.46-8.07)
<b>15-min</b>	<b>2.78</b> (2.56-3.02)	<b>3.33</b> (3.07-3.63)	<b>3.94</b> (3.61-4.28)	<b>4.33</b> (3.97-4.72)	<b>4.80</b> (4.38-5.23)	<b>5.12</b> (4.64-5.57)	<b>5.42</b> (4.88-5.90)	<b>5.66</b> (5.08-6.19)	<b>5.94</b> (5.28-6.52)	<b>6.13</b> (5.40-6.76)
<b>30-min</b>	<b>1.91</b> (1.75-2.07)	<b>2.30</b> (2.12-2.51)	<b>2.80</b> (2.56-3.04)	<b>3.14</b> (2.88-3.42)	<b>3.56</b> (3.24-3.87)	<b>3.86</b> (3.49-4.20)	<b>4.15</b> (3.74-4.52)	<b>4.41</b> (3.96-4.82)	<b>4.73</b> (4.20-5.19)	<b>4.96</b> (4.38-5.47)
<b>60-min</b>	<b>1.19</b> (1.09-1.29)	<b>1.44</b> (1.33-1.57)	<b>1.79</b> (1.64-1.95)	<b>2.04</b> (1.87-2.22)	<b>2.37</b> (2.16-2.58)	<b>2.61</b> (2.37-2.84)	<b>2.86</b> (2.58-3.11)	<b>3.09</b> (2.77-3.38)	<b>3.39</b> (3.02-3.72)	<b>3.62</b> (3.20-3.99)
<b>2-hr</b>	<b>0.712</b> (0.650-0.780)	<b>0.864</b> (0.791-0.946)	<b>1.08</b> (0.984-1.18)	<b>1.24</b> (1.13-1.36)	<b>1.45</b> (1.31-1.59)	<b>1.62</b> (1.46-1.77)	<b>1.79</b> (1.60-1.96)	<b>1.96</b> (1.74-2.15)	<b>2.18</b> (1.91-2.40)	<b>2.36</b> (2.04-2.60)
<b>3-hr</b>	<b>0.518</b> (0.474-0.568)	<b>0.628</b> (0.574-0.689)	<b>0.785</b> (0.716-0.860)	<b>0.905</b> (0.823-0.991)	<b>1.06</b> (0.962-1.17)	<b>1.19</b> (1.07-1.30)	<b>1.32</b> (1.18-1.44)	<b>1.45</b> (1.28-1.59)	<b>1.62</b> (1.41-1.79)	<b>1.75</b> (1.51-1.94)
<b>6-hr</b>	<b>0.323</b> (0.296-0.356)	<b>0.391</b> (0.358-0.430)	<b>0.487</b> (0.444-0.535)	<b>0.564</b> (0.513-0.619)	<b>0.672</b> (0.606-0.736)	<b>0.759</b> (0.679-0.831)	<b>0.851</b> (0.754-0.932)	<b>0.946</b> (0.830-1.04)	<b>1.08</b> (0.931-1.19)	<b>1.19</b> (1.01-1.32)
<b>12-hr</b>	<b>0.195</b> (0.179-0.216)	<b>0.236</b> (0.216-0.261)	<b>0.296</b> (0.269-0.327)	<b>0.345</b> (0.313-0.381)	<b>0.417</b> (0.374-0.459)	<b>0.477</b> (0.424-0.525)	<b>0.543</b> (0.476-0.598)	<b>0.613</b> (0.531-0.677)	<b>0.715</b> (0.606-0.793)	<b>0.801</b> (0.666-0.891)
<b>24-hr</b>	<b>0.113</b> (0.104-0.124)	<b>0.136</b> (0.125-0.149)	<b>0.171</b> (0.157-0.187)	<b>0.200</b> (0.183-0.218)	<b>0.242</b> (0.220-0.264)	<b>0.277</b> (0.251-0.302)	<b>0.315</b> (0.284-0.343)	<b>0.356</b> (0.319-0.387)	<b>0.416</b> (0.368-0.452)	<b>0.466</b> (0.408-0.506)
<b>2-day</b>	<b>0.065</b> (0.060-0.071)	<b>0.079</b> (0.072-0.086)	<b>0.099</b> (0.091-0.108)	<b>0.116</b> (0.105-0.126)	<b>0.139</b> (0.126-0.152)	<b>0.158</b> (0.143-0.173)	<b>0.179</b> (0.161-0.195)	<b>0.201</b> (0.180-0.219)	<b>0.233</b> (0.206-0.253)	<b>0.258</b> (0.228-0.282)
<b>3-day</b>	<b>0.046</b> (0.042-0.050)	<b>0.055</b> (0.051-0.061)	<b>0.069</b> (0.064-0.076)	<b>0.081</b> (0.074-0.088)	<b>0.097</b> (0.088-0.106)	<b>0.110</b> (0.100-0.120)	<b>0.125</b> (0.112-0.136)	<b>0.140</b> (0.125-0.152)	<b>0.161</b> (0.143-0.176)	<b>0.179</b> (0.158-0.195)

**Note: Our recommendations for proposed improvements to the stream / culverts are for the 100-yr storm intensity (2.86 inches per hour for the 1 hour storm) which exceeds the 10-year 1hour rainfall intensity of 2.04 which was previously noted by Meliora to be most attributable to localized flooding.**

<b>4-day</b>	<b>0.036</b> (0.033-0.040)	<b>0.044</b> (0.040-0.048)	<b>0.055</b> (0.050-0.060)	<b>0.063</b> (0.058-0.069)	<b>0.076</b> (0.069-0.083)	<b>0.086</b> (0.078-0.094)	<b>0.097</b> (0.088-0.106)	<b>0.109</b> (0.098-0.119)	<b>0.126</b> (0.112-0.137)	<b>0.139</b> (0.123-0.152)
<b>7-day</b>	<b>0.024</b> (0.022-0.026)	<b>0.029</b> (0.027-0.032)	<b>0.036</b> (0.033-0.039)	<b>0.041</b> (0.038-0.045)	<b>0.050</b> (0.045-0.054)	<b>0.056</b> (0.051-0.061)	<b>0.063</b> (0.058-0.069)	<b>0.071</b> (0.064-0.077)	<b>0.081</b> (0.073-0.089)	<b>0.090</b> (0.080-0.098)
<b>10-day</b>	<b>0.019</b> (0.018-0.021)	<b>0.023</b> (0.021-0.025)	<b>0.028</b> (0.026-0.030)	<b>0.032</b> (0.030-0.035)	<b>0.038</b> (0.035-0.041)	<b>0.042</b> (0.039-0.046)	<b>0.047</b> (0.043-0.051)	<b>0.052</b> (0.047-0.056)	<b>0.059</b> (0.053-0.064)	<b>0.065</b> (0.058-0.070)
<b>20-day</b>	<b>0.013</b> (0.012-0.014)	<b>0.015</b> (0.014-0.017)	<b>0.018</b> (0.017-0.020)	<b>0.021</b> (0.019-0.022)	<b>0.024</b> (0.022-0.026)	<b>0.026</b> (0.025-0.028)	<b>0.029</b> (0.027-0.031)	<b>0.031</b> (0.029-0.034)	<b>0.035</b> (0.032-0.037)	<b>0.037</b> (0.034-0.040)
<b>30-day</b>	<b>0.011</b> (0.010-0.011)	<b>0.013</b> (0.012-0.013)	<b>0.015</b> (0.014-0.016)	<b>0.016</b> (0.016-0.017)	<b>0.019</b> (0.018-0.020)	<b>0.020</b> (0.019-0.021)	<b>0.022</b> (0.021-0.023)	<b>0.023</b> (0.022-0.025)	<b>0.026</b> (0.024-0.027)	<b>0.027</b> (0.025-0.029)
<b>45-day</b>	<b>0.009</b> (0.009-0.010)	<b>0.011</b> (0.010-0.011)	<b>0.012</b> (0.012-0.013)	<b>0.014</b> (0.013-0.014)	<b>0.015</b> (0.014-0.016)	<b>0.016</b> (0.015-0.017)	<b>0.017</b> (0.016-0.018)	<b>0.018</b> (0.017-0.019)	<b>0.020</b> (0.018-0.021)	<b>0.021</b> (0.019-0.022)
<b>60-day</b>	<b>0.008</b> (0.008-0.009)	<b>0.010</b> (0.009-0.010)	<b>0.011</b> (0.010-0.012)	<b>0.012</b> (0.011-0.013)	<b>0.013</b> (0.013-0.014)	<b>0.014</b> (0.013-0.015)	<b>0.015</b> (0.014-0.016)	<b>0.016</b> (0.015-0.017)	<b>0.017</b> (0.016-0.018)	<b>0.018</b> (0.017-0.018)

<sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

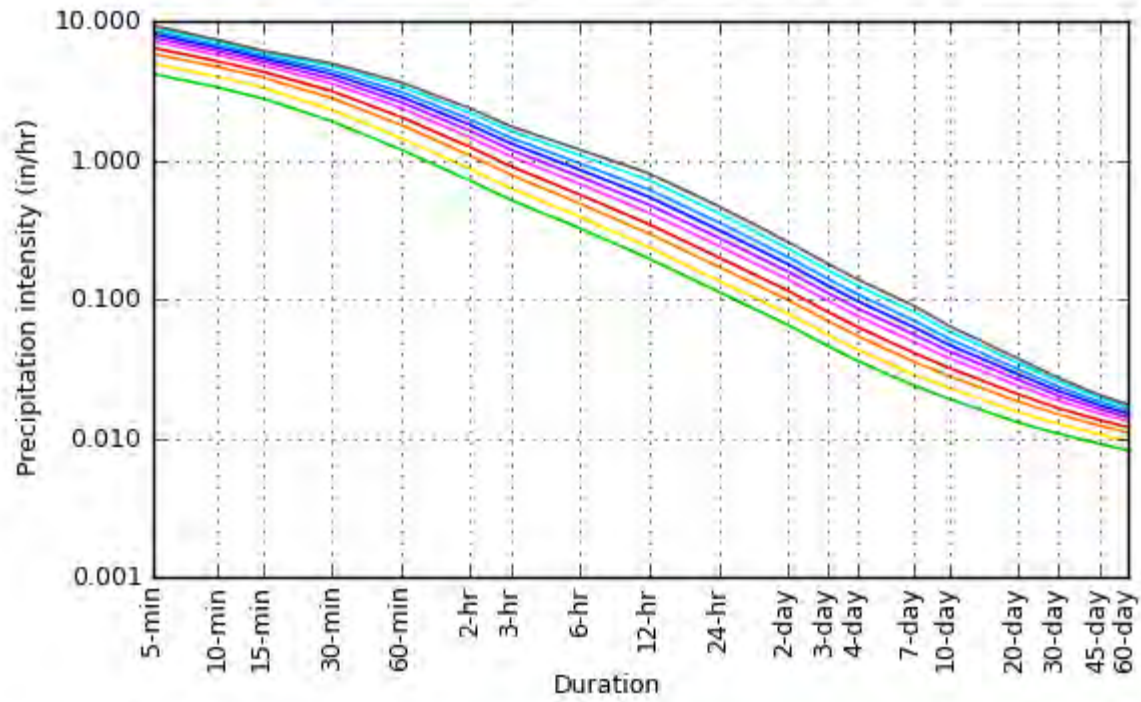
Please refer to NOAA Atlas 14 document for more information.

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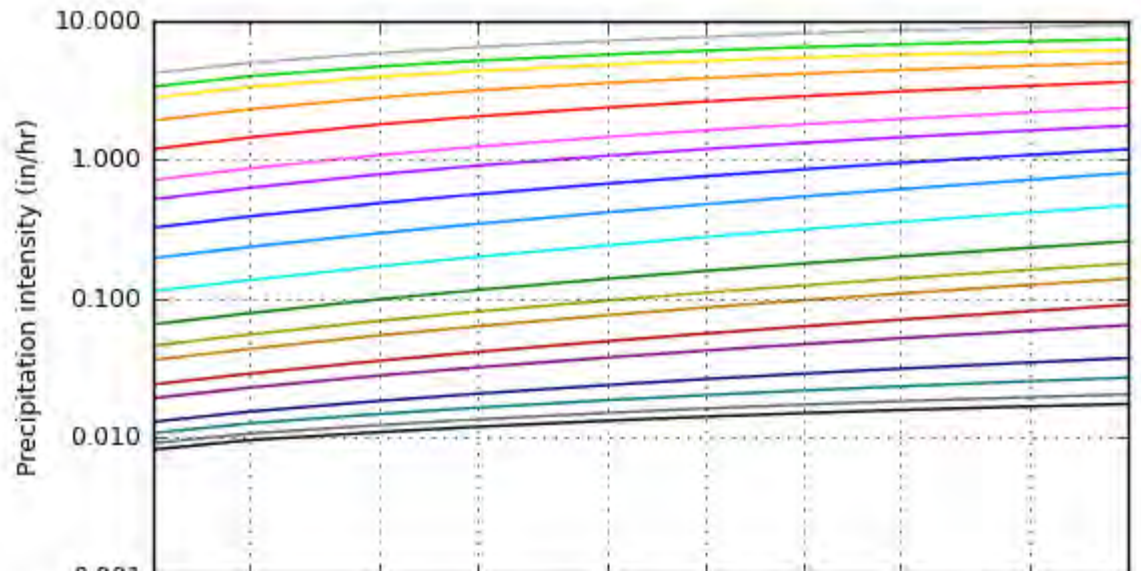
## PF graphical

### PDS-based intensity-duration-frequency (IDF) curves

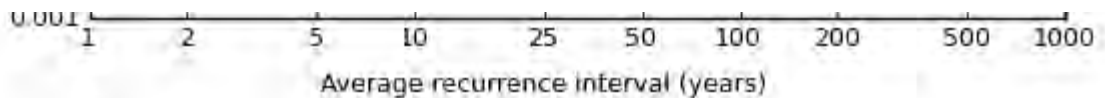
Latitude: 40.0409°, Longitude: -75.3788°



Average recurrence interval (years)
1
2
5
10
25
50
100
200
500
1000



Duration
5-min
10-min
15-min
30-min
60-min
2-hr
3-hr
6-hr
12-hr
24-hr
2-day
3-day
4-day
7-day
10-day
20-day
30-day
45-day
60-day



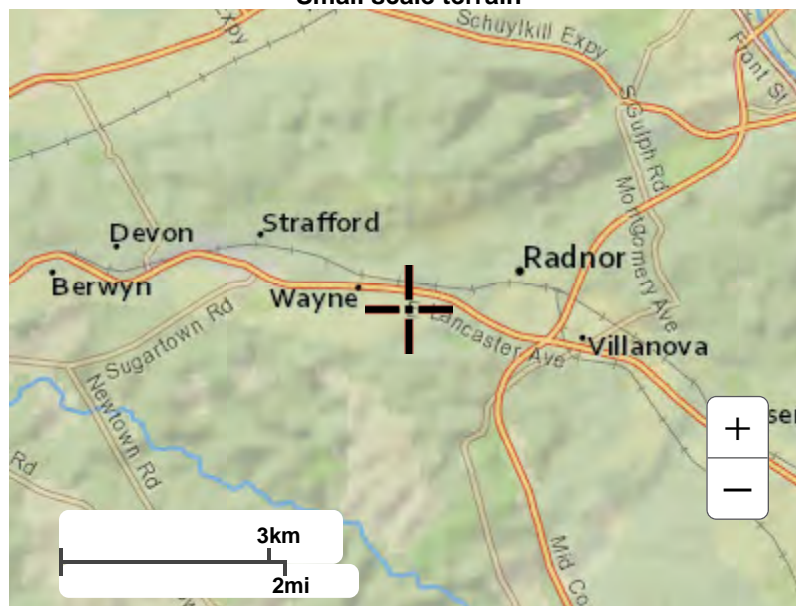
NOAA Atlas 14, Volume 2, Version 3

Created (GMT): Thu Apr 21 19:32:01 2022

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## Maps & aerials

### Small scale terrain



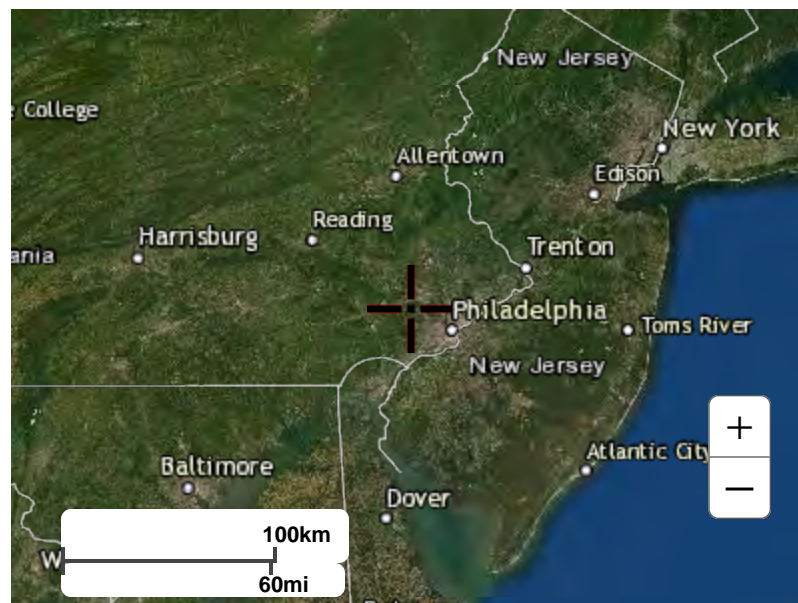
### Large scale terrain



Large scale map



Large scale aerial



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[US Department of Commerce](#)  
[National Oceanic and Atmospheric Administration](#)  
[National Weather Service](#)  
[National Water Center](#)  
1325 East West Highway  
Silver Spring, MD 20910  
Questions?: [HDSC.Questions@noaa.gov](mailto:HDSC.Questions@noaa.gov)

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**APPENDIX F: STORM SEWER BYPASS PLANS**



Carroll Engineering Corporation  
 CORPORATE OFFICE  
 949 EASTON ROAD  
 WARRINGTON, PA 18976  
 PHONE: 215.343.5700  
 FAX: 215.343.0875

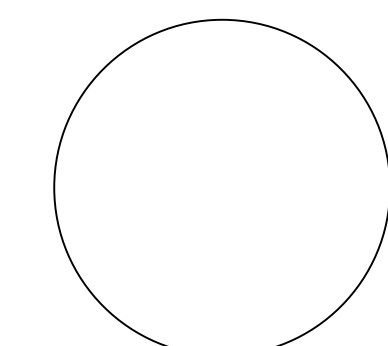
630 Freedom Business Ctr., 3rd Fl. 105 Rader Boulevard, Suite 206  
 King of Prussia, PA 19386 Hillsborough, NJ 08044  
 Phone: 610.572.7093 Phone: 908.874.7500  
 Fax: 908.874.5122

433 Lancaster Avenue, Suite 200  
 Malvern, PA 19355  
 Phone: 610.489.5100

www.carrollengineering.com



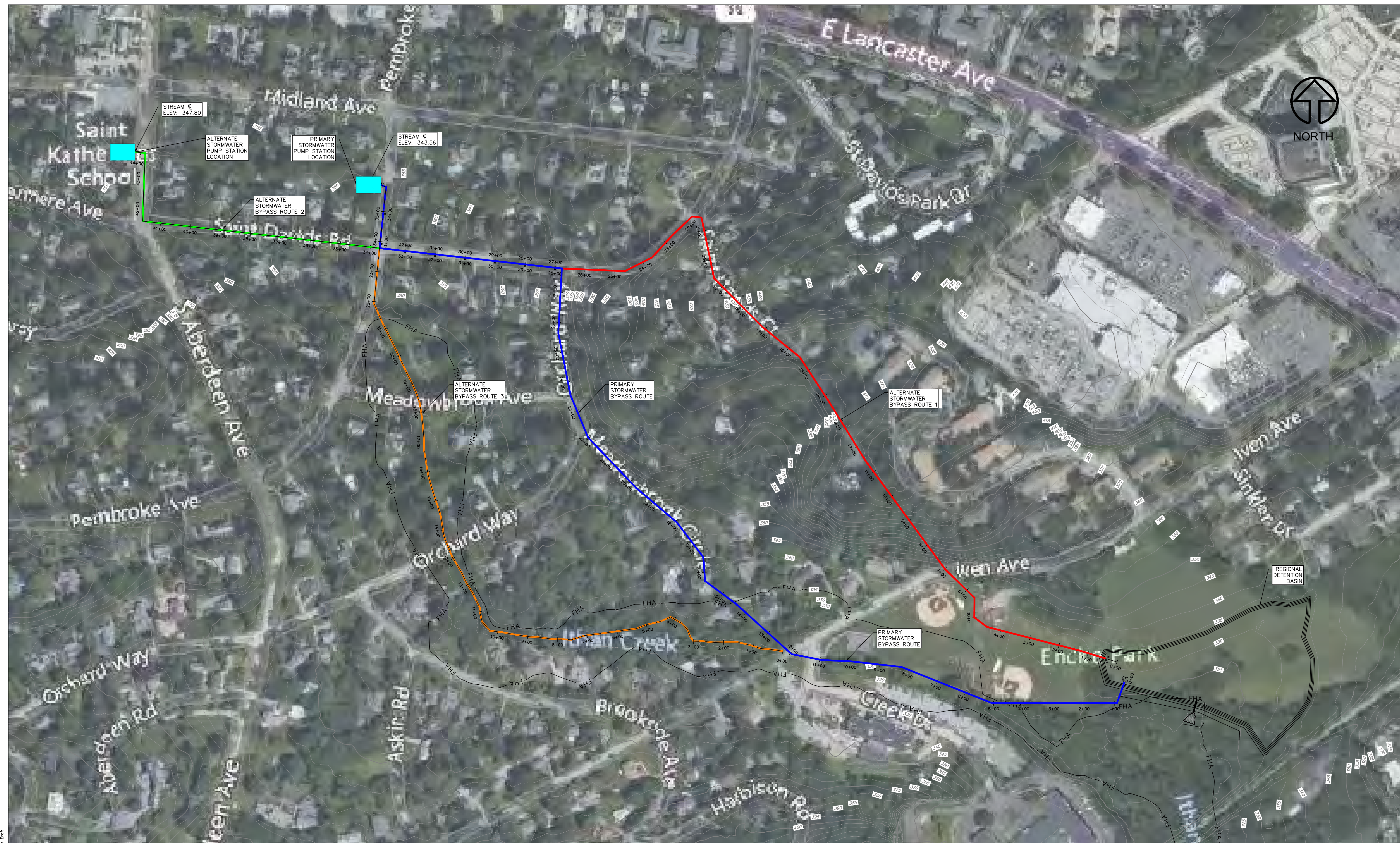
NORTH



STORM SEWER BYPASS  
 CONCEPTUAL PLAN

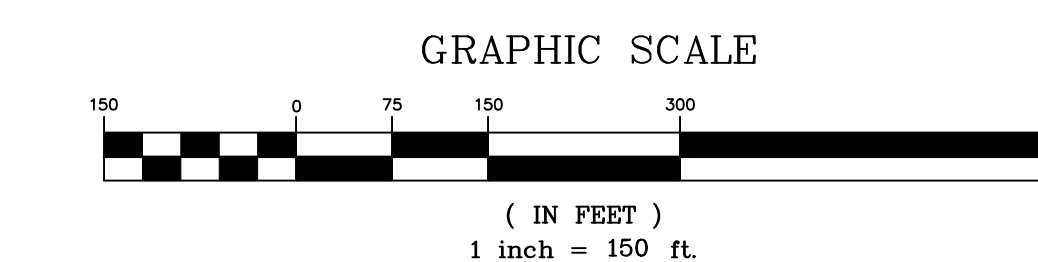
SOUTH WAYNE DRAINAGE IMPROVEMENTS  
 FEASIBILITY STUDY

SITUATED IN  
 RADNOR TOWNSHIP, DELAWARE COUNTY  
 PREPARED FOR  
 RADNOR TOWNSHIP  
 301 IVEN AVE  
 WAYNE, PA 19087



STORMWATER BYPASS SUMMARY TABLE			
	PIPE DIA. (IN)	TOTAL LENGTH	
PRIMARY BYPASS	84	3601 LF	
ALTERNATE BYPASS 1 (SAINT DAVIDS)	84	3506 LF	
ALTERNATE BYPASS 2 (SAINT KATHERINE'S PS LOCATION)	84	4422 LF	
ALTERNATE BYPASS 3 (PARALLEL TO ITHAN CREEK)	84	3818 LF	

PROPOSED SWM FACILITY STORAGE				
STAGE	ELEVATION	CONTOUR AREA (SF)	INCREMENTAL STORAGE (CF)	TOTAL STORAGE (CF)
0	325.00	165,848	-	-
1	326.00	169,699	167,774	167,774
3	328.00	177,501	347,200	514,974
5	330.00	185,434	362,935	877,909
7	332.00	193,497	378,931	1,256,840



NO.	DATE	DESCRIPTION	INITIALS

DATE 4-22-2022  
 CADD FILE 2119900004  
 JOB NO 21-1990  
 DSG BY CAP  
 DWN BY MEW  
 CKD BY WNM  
 SCALE 1"=150'  
 DRAWER NUMBER -  
 SHEET 1 OF 4 SHEETS  
 DRAWING NUMBER C-101



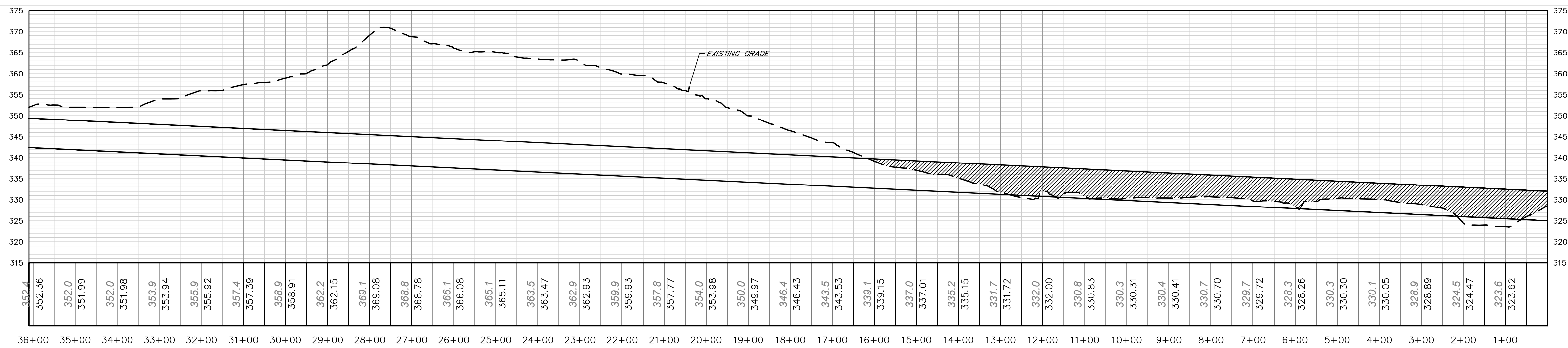
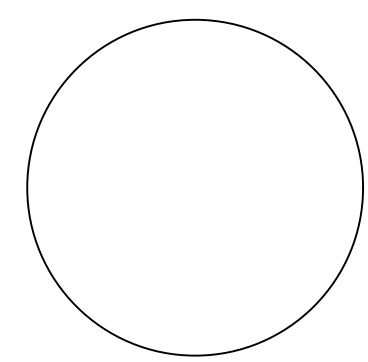
Carroll Engineering Corporation

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949 EASTON ROAD  
WARRINGTON, PA 18976  
PHONE: 215.343.5700  
FAX: 215.343.0875

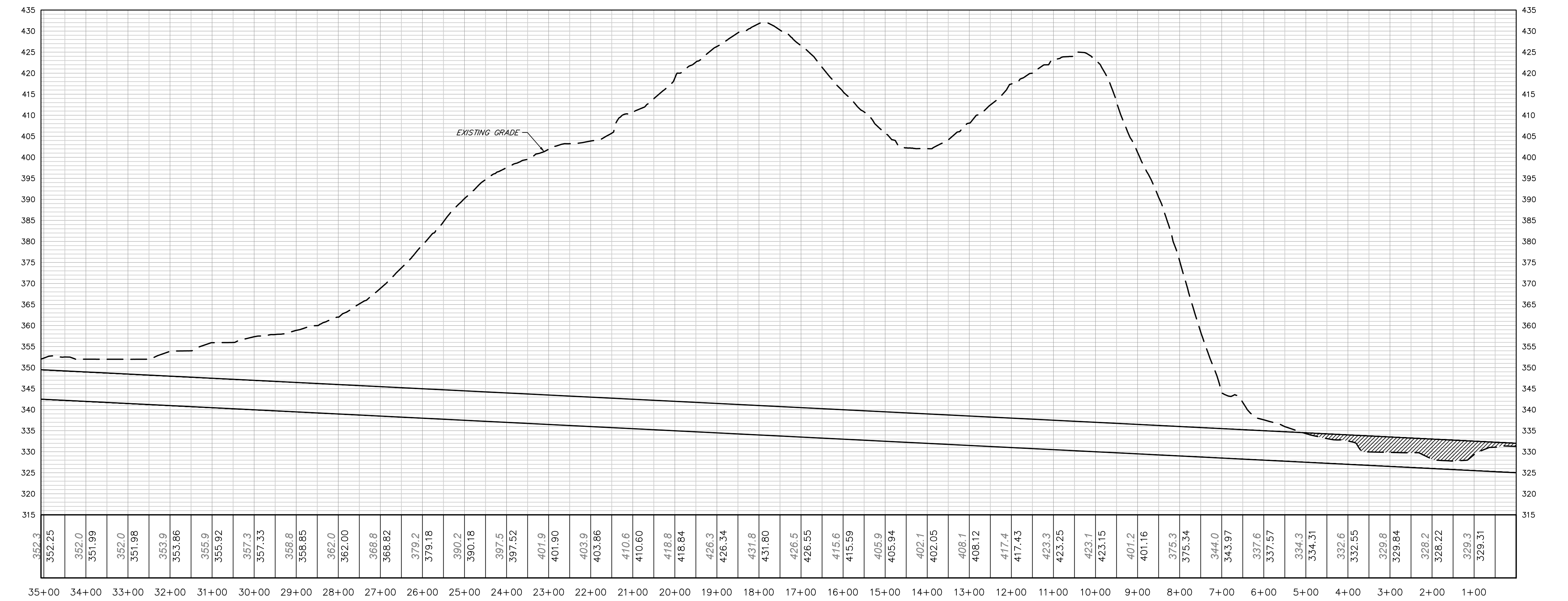
630 Freedom Business Ctr., 3rd Fl. 105 Raider Boulevard, Suite 206  
King of Prussia, PA 19386 Hillsborough, NJ 08044  
Phone: 610.572.7093 Fax: 908.874.7500

433 Lancaster Avenue, Suite 200  
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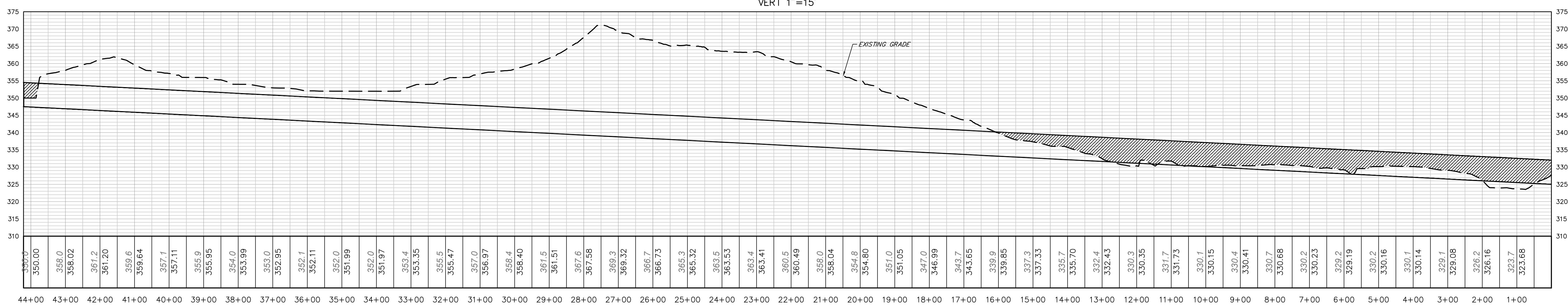
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ITHAN CREEK BYPASS PROFILE  
SCALE: HORIZ 1"=150'  
VERT 1"=15'



ITHAN CREEK BYPASS ALTERNATE 1 PROFILE  
SCALE: HORIZ 1"=150'  
VERT 1"=15'



ITHAN CREEK BYPASS ALTERNATE 2 PROFILE  
SCALE: HORIZ 1"=150'  
VERT 1"=15'

STORM SEWER BYPASS  
GRAVITY PIPE PROFILES  
SOUTH WAYNE DRAINAGE IMPROVEMENTS  
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301 IVEN AVE  
WAYNE, PA 19087

NO.	DATE	DESCRIPTION	INITIALS

DATE 4-22-2022  
CADD FILE 2119900004  
JOB NO 21-1990  
DSG BY CAP  
DWN BY MEW  
CKD BY WNM  
SCALE 1"=150'  
DRAWER NUMBER -

SHEET 2 OF 4 SHEETS

DRAWING NUMBER  
C-102



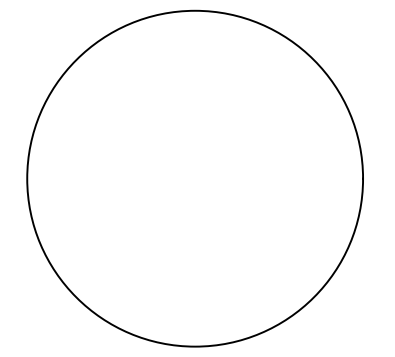
Carroll Engineering Corporation

CORPORATE OFFICE  
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FAX: 215.343.0875

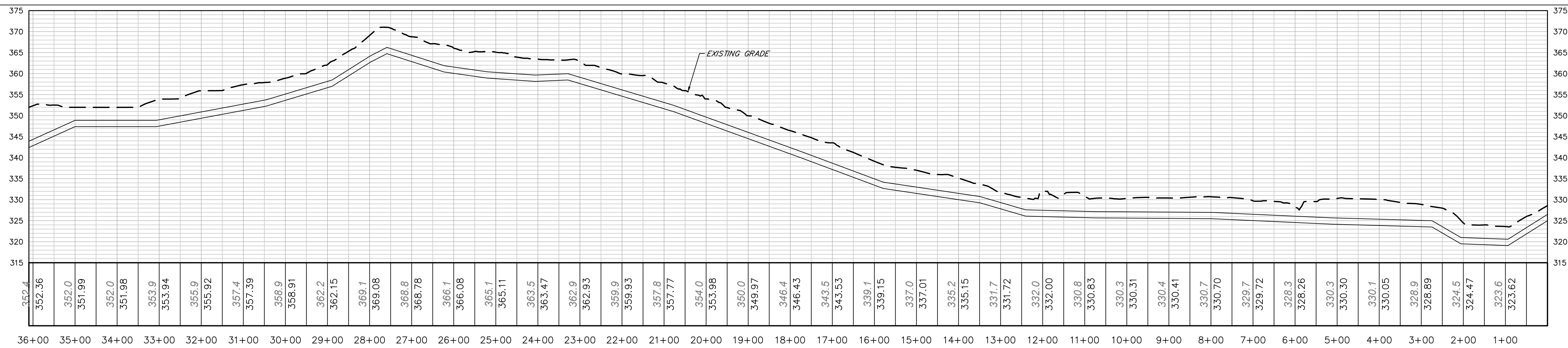
630 Freedom Business Ctr., 3rd Fl. 105 Rader Boulevard, Suite 206  
King of Prussia, PA 19386 Hillsborough, NJ 08044  
Phone: 610.572.7093 Phone: 908.874.7500  
Fax: 908.874.5122

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Malvern, PA 19355  
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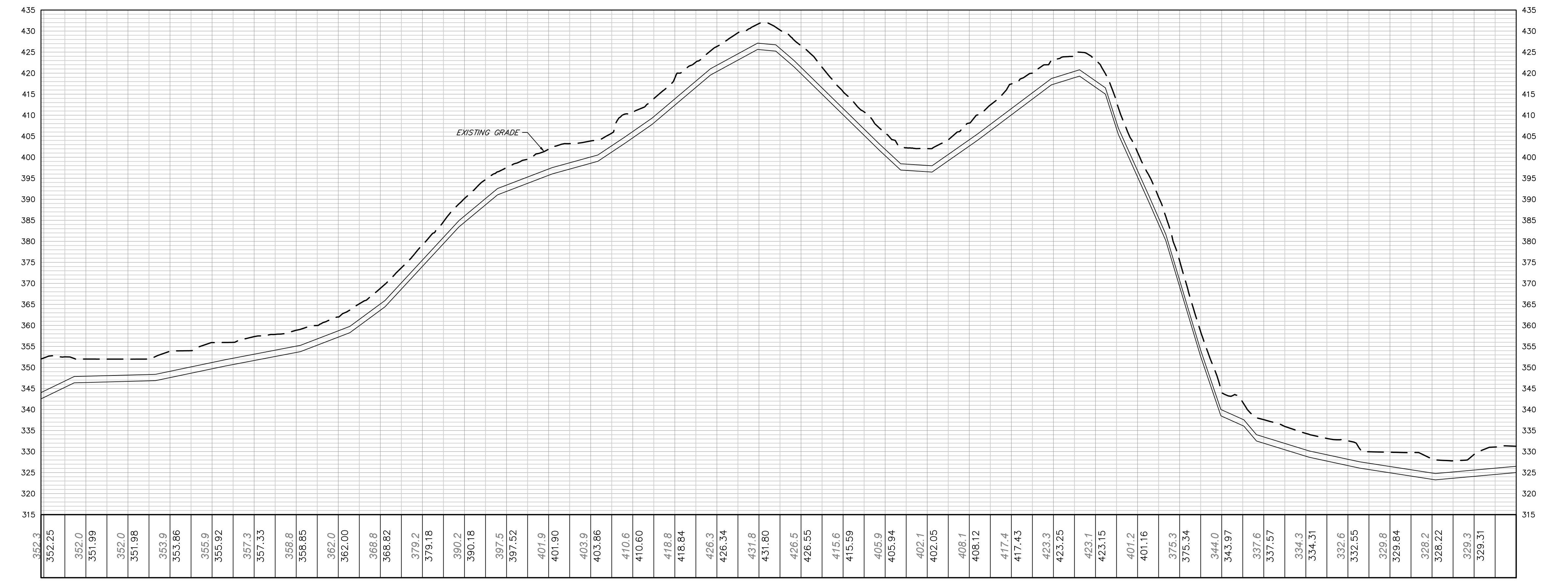
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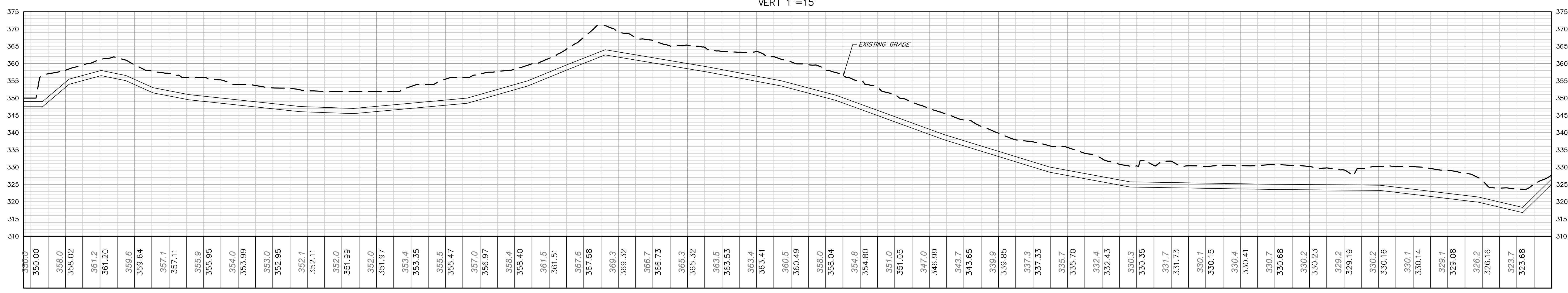
STORM SEWER BYPASS  
PRESSURE PIPE PROFILES  
SOUTH WAYNE DRAINAGE IMPROVEMENTS  
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ITHAN CREEK BYPASS PROFILE  
SCALE: HORIZ 1"=150'  
VERT 1"=15'



ITHAN CREEK BYPASS ALTERNATE 1 PROFILE  
SCALE: HORIZ 1"=150'  
VERT 1"=15'



ITHAN CREEK BYPASS ALTERNATE 2 PROFILE  
SCALE: HORIZ 1"=150'  
VERT 1"=15'

PL:\211990\CAD\211990000.dwg, Apr. 22, 2022, 4:10pm, mwalsh, Eriat

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NO.	DATE	DESCRIPTION

DATE	4-22-2022
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JOB NO	21-1990
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DWN BY	MEW
CKD BY	WNM
SCALE	1"=150'
DRAWER NUMBER	-

SHEET 3 OF 4 SHEETS

DRAWING NUMBER  
**C-103**

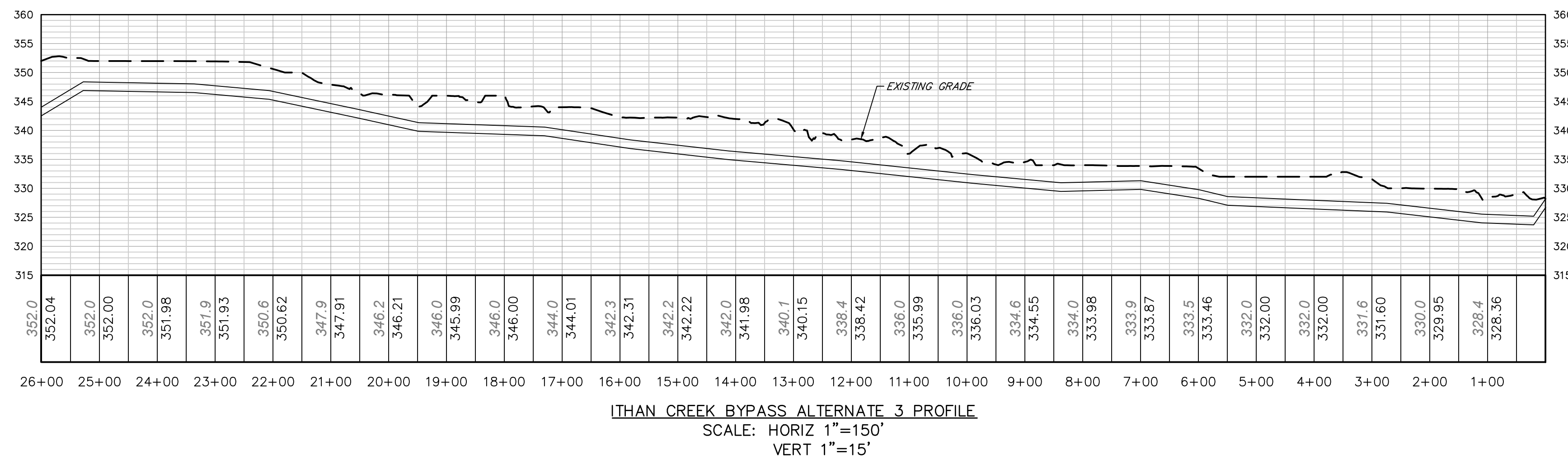
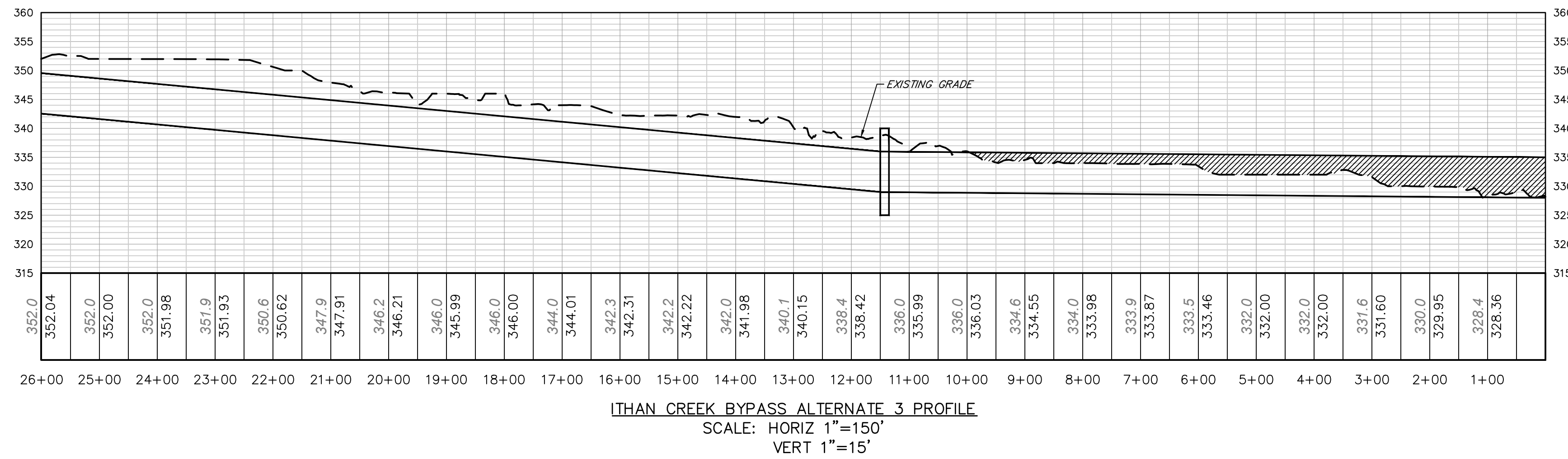
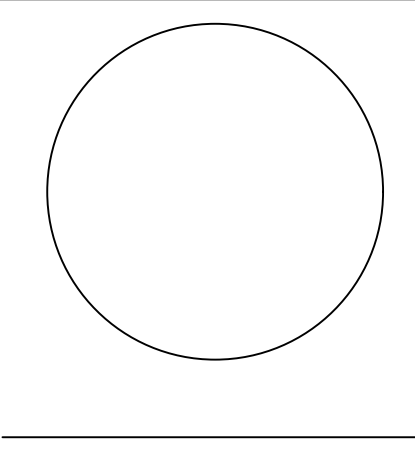


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STORM SEWER BYPASS  
 ALTERNATE 3 PROFILES  
 SOUTH WAYNE DRAINAGE IMPROVEMENTS  
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DATE 4-22-2022  
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 JOB NO 21-1990  
 DSG BY CAP  
 DWN BY MEW  
 CKD BY WNM  
 SCALE 1"=150'  
 DRAWER NUMBER -  
 SHEET 4 OF 4 SHEETS

DRAWING NUMBER  
**C-104**